

# LOW-RISE RESIDENTIAL ALTERNATIVE CALCULATION METHOD APPROVAL MANUAL

NOVEMBER 1998

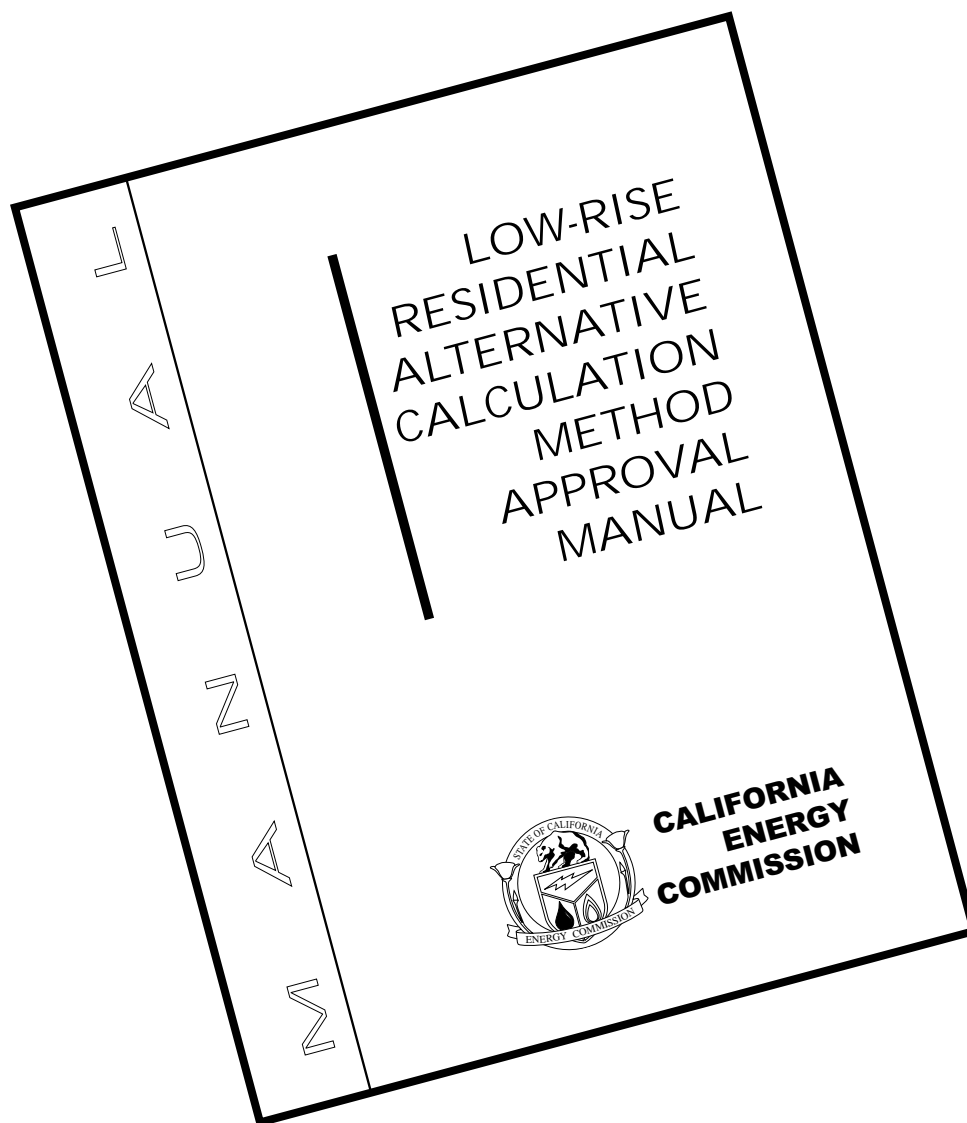


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**Appendices****A. CERTIFICATION AND APPROVAL FORMS****B. MINIMUM CAPABILITIES TEST SPECIFICATIONS****C. CUSTOM BUDGET TEST SPECIFICATIONS****D. OPTIONAL CAPABILITIES TEST SPECIFICATIONS****E. CONSTRUCTIONS FOR AUTOMATIC FORM 3 GENERATOR TEST****F. STANDARD PROCEDURE FOR DETERMINING THE SEASONAL ENERGY EFFICIENCIES OF RESIDENTIAL AIR DISTRIBUTION SYSTEMS.****G. APPLICATION PACKAGE FOR CERTIFICATION OF SOLAR WATER HEATING ENERGY PERFORMANCE CALCULATION METHODS FOR RESIDENTIAL BUILDINGS****H. GLOSSARY****I. INTERIOR MASS CAPACITY (IMC)****J. HVAC DISTRIBUTION (DUCT) SYSTEM EFFICIENCY TABLES**



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## 1. Overview

This Manual explains the requirements for approval of residential *Alternative Calculation Methods* (ACMs). Residential ACMs are used to demonstrate compliance with the performance approach to the efficiency standards for Low-Rise Residential Buildings as defined in the building energy efficiency standards of the State Building Code.

The approval procedure is one of self-testing and self-certification by the vendor of an ACM. The vendor conducts the specified tests, evaluates the results and certifies in writing that the ACM passes the tests. The California Energy Commission (Commission) will perform spot checks and may require additional tests to verify that the proposed ACM is suitable for compliance purposes. The vendor is required to develop a compliance supplement (program user manual) explaining how to use the program for showing compliance with the standards. The compliance supplement will also be checked by the Commission for accuracy and ease of use.

When energy analysis techniques are compared, there may be two basic sources of discrepancies: differences in user interpretation when entering the building specifications, and differences in the ACM's algorithms for estimating energy use. The approval tests in this manual are designed to minimize differences in interpretation by providing explicit detailed descriptions of the test buildings that must be analyzed.

This Manual is written as if all ACMs are computer programs. While this is generally true, there is nothing to prohibit other kinds of energy analysis methods from seeking ACM approval. The basic requirements for accuracy and reliability still apply.

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### 1.1 Summary of ACM Changes

The ACM Approval Manual is updated with each major revision of the low-rise residential Standards. This manual is to be used with the 1998 Standards to be implemented July 1, 1999. The major changes between this manual and the 1992 manual are summarized below.

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#### 1.1.1 Modeling Assumptions

Several changes have been made to the way energy use is calculated in the public domain program, as summarized below.

- Fenestration Shading
- Thermal Mass Defaults
- Basement Walls
- Thermal Distribution Efficiency
  - (including a variety of duct efficiency measures such as leakage reduction, ACCA Manual D design specifications, reduced duct surface area)
- Infiltration/Ventilation Modeling



(including continuous infiltration reduction, window opening for Indoor Air Quality [IAQ] and shielding class)

- Solar Gain Reductions
- Water Heating Calculations

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### **1.1.2 Standard Design Definition**

The definition of the standard design (the custom budget building) has been updated to correspond with the performance levels required by the 1998 Standards.

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## **1.2 ACM Requirements**

This chapter presents the general requirements for residential ACMs.

Appropriate inputs for all modeling capabilities are discussed in Chapter 2.

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### **1.2.1 Minimum Modeling Capabilities**

Minimum modeling capabilities must be included in all ACMs. If a candidate ACM does not have all of these capabilities, then it cannot be approved for compliance. The minimum modeling capabilities are summarized below:

- Conduction gains and losses through opaque and fenestration surfaces.
- Infiltration gains and losses
- Solar gains through glazing including the effects of internal shading devices, external shading devices and fixed overhangs.
- Natural ventilation cooling and natural ventilation for Indoor Air Quality (IAQ).
- Mechanical Ventilation for IAQ.
- Thermal mass effects to dampen temperature swings.
- Space conditioning equipment efficiency and distribution systems.
- Water heating equipment efficiency and distribution systems.
- Radiant Barriers

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### **1.2.2 Optional Modeling Capabilities**

Candidate ACMs may have more capabilities than the minimum required. ACMs can be approved for use with none, a few, or all of the optional capabilities. The following optional capabilities are recognized for residential ACMs:

- Raised floors with automatically operated crawl space vents.



- Zonal control or multi-zone modeling of the sleeping and living areas of the house.
- Attached sunspaces for collection and possible storage of heat for transfer to the main house.
- Exterior mass walls.
- Side Fin Shading.
- Combined hydronic space and water heating.
- Building additions.
- Solar water heating.
- Form 3 report generator.
- Gas-Fired Heat Pumps

Many of the optional modeling capabilities have been previously approved by the Commission through the exceptional methods process. The approval tests for optional modeling capabilities are included in Chapter 6. To determine how to apply for the Exceptional Method Application (EMA) to provide optional modeling capability refer to Section 0, Page 7 of this Manual.

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### ***1.3 Application Checklist***

The following is a checklist of all the items that must be included in an application package for ACMs. Some materials are required only for general purpose ACMs and are so indicated.

- *ACM Vendor Certification Statement.* A statement from the ACM vendor certifying the ACM, and, its reliability and accuracy when used for compliance purposes (see Appendix A, Page A-1).
- *Computer Run Summary Sheets.* Hard copy summary sheets of all the required computer runs (see Appendix A, Pages A-2 to A-12).
- *Computer Runs.* Copies of the computer runs specified in Chapters 5 and 6 of this Manual, including complete input and output files, on diskettes or in IBM-compatible computer readable form acceptable to the Commission to enable spot checks.
- *Compliance Supplement.* A copy of the Compliance Supplement discussed in Chapter 8. The Compliance Supplement and the ACM User's Manual may be combined into the same document.
- *Copy of the ACM.* A magnetic media copy of the ACM (in IBM-PC compatible, or other format agreed to by the Commission staff) for verification of analyses and random verification of compliance analyses. Weather data must be included.



- *Weather Data Documentation.* For those general purpose ACMs not using the standard Commission, full year, hourly weather data, a copy of the summarized weather data must be submitted. Documentation must be included on the method used to develop the summary weather data.
- *Application Fee.* An application fee of \$1,000.00 (one thousand dollars) is required to cover costs of evaluating the application.

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## 1.4 Types of Approval

This Manual addresses three types of ACM approval: full approval, streamlined approval of new program features, and amendments to full approvals.

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### 1.4.1 Full Approval

Full approval is required when a candidate ACM has never been previously approved by the Commission, and/or when the ACM vendor makes changes to the executable program code or algorithms, or any other change that in any way affects the results. The Commission may also require that all ACMs be approved again when the standards are updated on the three year cycle or whenever substantial revisions are made to the approval process, for instance, if new analysis capabilities come into widespread use, and the Commission declares them to be minimum capabilities for all ACMs.

When re-approval is necessary, the Commission will notify all ACM vendors of the timetable for renewal. There will also be a revised ACM Approval Manual published, with complete instructions for re-approval.

Full approval is required for all ACM changes, unless they qualify for the streamlined approval process or for an addendum, as discussed below.

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### 1.4.2 Streamlined Approval

Certain types of changes may be made to approved residential ACMs through a streamlined procedure. Examples of changes that qualify for streamlined approval are modifications to the user interface or implementation on a different operating system as long as there are no changes to the executable program code that would in anyway affect the results.

If an ACM modification qualifies for streamlined approval, then the following procedure is followed:

- The ACM vendor prepares an addendum to the compliance supplement, when appropriate, describing the change to the ACM.
- The ACM vendor notifies the Commission by letter of the change. The letter must describe in detail the nature of the change and why it is being made. The notification letter shall be included in the Compliance Supplement.
- Provide the Commission with an updated copy of the ACM and include any new reports created by the ACM (or modifications in the standard reports).
- The Commission responds in 45 days. The Commission response may take several forms. The Commission may request additional information, refuse to approve the



change or require that the ACM vendor make specific changes to either the Compliance Supplement addendum or the ACM.

- With Commission approval, the vendor may issue new copies of the ACM with the Compliance Supplement addendum and notify ACM users and building officials.

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### **1.4.3 Amendments**

An ACM approval must be amended when optional modeling capabilities are added. The vendor must provide the additional computer runs required for the optional modeling capability. It is not necessary to include computer runs previously submitted.

An amendment to an approved ACM must be accompanied by a cover letter explaining the type of amendment requested, and copies of other documents as necessary. All items on the application checklist should be submitted, when applicable. The timetable for approval of amendments is the same as for full approval.

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### **1.4.4 When Approval is not Required**

Changes which do not affect compliance with the Energy Efficiency Standards for Residential Buildings do not require full or streamlined approval. However, the ACM vendor must notify the Commission and provide the Commission with an updated copy of the program and user manual. Reapproval is required for any ACM program change that affects the energy use calculations for compliance, the modeling capabilities for compliance, the format and/or content of compliance forms, or any other change which would affect a building's compliance with the Standards. Any questions regarding applicable approval procedures should be directed to the Commission.

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## **1.5 Challenges**

Building officials, program users, program vendors or other interested parties may challenge any residential ACM approval. If any interested party believes that a compliance program, an algorithm, or method of calculation used in a compliance program, a particular capability or other aspect of a program provides inaccurate results, the party may challenge the program. (See Section 0, 1.6 Decertification of ACMs, for a description of the process for a challenge.)

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## **1.6 Decertification of ACMs**

The Commission may *decertify* (rescind approval of) an alternative calculation method through various means:

- All ACMs are decertified when the standards undergo substantial changes which usually occur every three years.
- Any ACM can be decertified by a letter from the ACM vendor requesting that a particular version (or versions) of the ACM be decertified. The decertification request must briefly describe the nature of the program errors or "bugs" which justify the need for decertification.
- Any "initiating party" may commence a procedure to decertify an ACM according to the steps outlined below. The intent is to include a means whereby serious program



errors, flawed numeric results, improper forms and/or incorrect program documentation not discovered in the certification process can be verified, and use of the particular ACM version discontinued. In this process, there is ample opportunity for the Commission, the ACM vendor and all interested parties to evaluate any alleged errors in the ACM program.

Following is a description of the process for challenging an ACM or initiating a decertification procedure:

1. Any party may initiate a review of an ACM's approval by sending a written communication to the Commission's Executive Director. (The Commission may be the initiating party for this type of review by noticing the availability of the same information listed here.)

The initiating party shall:

- (a) State the name of the ACM and the program version number(s) which contain the alleged errors;
  - (b) Identify concisely the nature of the alleged errors in the ACM which require review;
  - (c) Explain why the alleged errors are serious enough in their effect on analyzing buildings for compliance to justify a decertification procedure; and,
  - (d) Include appropriate data on IBM PC compatible floppy diskettes and/or information sufficient to evaluate the alleged errors.
2. The Executive Director shall make a copy or copies of the initial written communication available to the ACM vendor and interested parties within 30 days.
  3. Within 75 days of receipt of the written communication, the Executive Director may request any additional information needed to evaluate the alleged ACM errors from the party who initiated the decertification review process. If the additional information is incomplete, this procedure will be delayed until the initiating party submits complete information.
  4. Within 75 days of receipt of the initial written communication, the Executive Director may convene a workshop to gather additional information from the initiating party, the ACM vendor and interested parties. All parties will have 15 days after the workshop to submit additional information regarding the alleged program errors.
  5. Within 90 days after the Executive Director receives the application or within 30 days after receipt of complete additional information requested of the initiating party, whichever is later, the Executive Director shall either:
    - (a) Determine that the ACM need not be decertified; or,
    - (b) Submit to the Commission a written recommendation that the ACM be decertified.
  6. The initial written communication, all other relevant written materials and the Executive Director's recommendation shall be placed on the consent calendar and considered at the next business meeting after submission of the recommendation. The matter may be removed from the consent calendar at the request of any person.
  7. If the Commission approves the ACM decertification, it shall take effect 60 days later. During the first 30 days of the 60 day period, the Executive Director shall send



out a Notice to Building Officials and Interested Parties announcing the decertification.

All initiating parties have the burden of proof to establish that the review of alleged ACM errors should be granted. The decertification process may be terminated at any time by mutual written consent of the initiating party and the Executive Director.

As a practical matter, the ACM vendor may use the 180- to 210-day period outlined here to update the ACM program, get it reapproved by the Commission, and release a revised version that does not contain the bugs initially brought to the attention of the Commission. Sometimes the ACM vendor may wish to be the initiating party to ensure that a faulty program version is taken off the market.

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### ***1.7 Alternative ACM Tests***

This Manual provides tests to verify that ACMs are accurate. These tests are provided in Chapters 5 and 6 of the Manual. An ACM vendor may propose alternate tests when the vendor believes that one or more of the standard tests are not appropriate for the ACM. Alternate tests will be evaluated by the Commission and will be accepted if they are considered reasonable. If accepted, the alternate test(s) will be added to this manual as an addendum and the alternate test(s) will be available for use by all ACMs. The alternate test will coexist with the standard test presented in this Manual until the Manual is revised. When a new version of this Manual is produced, the alternative test may be substituted for the current test or may continue to coexist with the original test.

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### ***1.8 Approval of New Exceptional Methods***

The Commission may approve new exceptional methods. Exceptional methods are special modeling capabilities or calculation methods necessary to recognize building features that cannot be adequately modeled with existing ACMs. When an Exceptional Method is approved, a new optional capabilities test may be approved as part of the process. Exceptional Methods do not necessarily produce *optional capabilities* for ACMs. For instance, radiant heating systems are recognized by an adjusted equipment efficiency that may be used directly in ACMs or other compliance methods. To be approved for the new optional capability, vendors must amend their ACM approval.

Even if an ACM already incorporates the Exceptional Method, the vendor must receive approval to use the Exceptional Method in the compliance process. The ACM vendor must demonstrate that the ACM automatically uses the correct fixed and restricted inputs for the Exceptional Method and that the standard reports identify the building feature(s) recognized by the Exceptional Method. Additionally, the ACM compliance supplement must be updated, referencing the use of the new Exceptional Method.

To receive a copy of the Exceptional Method contact the Residential Office at (916) 654-4064.







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## 2. Standard Reports

For consistency and ease of enforcement, the manner in which building features are reported by ACMs must be standardized. This section of the ACM Approval manual describes the required standard reports. All residential ACMs must automatically produce compliance reports in the Commission-prescribed format specified in the following sections of this Manual. These *Standard Reports* are required to enable building officials to evaluate the results from ACMs without having to learn each computer program. Included in every compliance package will be reports CF-1R and C-2R, which are described in detail below.

Both the CF-1R and the C-2R must have two highly visible sections, one for special features and modeling assumptions and a second for features requiring verification by approved home energy rating system (HERS) providers. These two sections serve as “punchlists” for special consideration during compliance verification by the local building department. Items listed in the *Special Features and Modeling Assumptions* section indicate the use for compliance of unusual features or assumptions, and call for special care by the local building department. Items listed in the HERS Required Verification section are for features that rely on diagnostic testing or independent verification by HERS raters under the supervision of Commission-approved HERS providers to insure proper field installation in addition to local building department inspection.

Only user inputs are described and included in the standard reports. The fixed and restricted inputs are not included since ACMs must be designed so that the fixed and restricted inputs and default values in the absence of specific user input are automatically used when the program is used for compliance.

For compliance forms, the structure of the Standard Reports described in the subsequent sections should be followed as closely as possible. The reports are divided into tabular *listings* that have a title, column headings and data entries. The data entries shown in the listings that appear in this manual are *typical* values and are included only to illustrate the report format; they are not default values and cannot be assumed to be in compliance with the standards. The specification of the category or type of data expected in each field is provided in the list of definitions associated with each column heading. The type of data entries will be one of the following:

- *text*: A variable-length text field input by the user.
- *recommended descriptor*: An abbreviation or short name from lists or tables of permissible types provided within this manual (e.g., *LgStoGas*). Only types found in these lists or tables may be used. Different descriptors may be used by the ACM as long as they are reasonable descriptors for the list entry item and are not misleading. In some cases where the descriptor is a short complete word, the descriptors are prescribed and must be used. Even for prescribed descriptors some discretion is allowed. For example, for tables with long rows *Y* may be used for the prescribed descriptor *Yes*. User-defined descriptors may NOT be used but rather must be



automatically assigned by the ACM based upon user input. For example, *UWALL01* may be assigned by the ACM to the first user-defined wall type.

- *filename.ext*: The name of the input or output file
- dimensions or units of measure, such as "hr-ft<sup>2</sup>-/F /Btu", ft<sup>2</sup>, etc.
- *Num*: A cardinal or ordinal number.

Modifications will be approved by the Commission when they are necessary because of conceptual differences between ACMs or because of special modeling features. The categories of information represented in the tables and the standard headings must not be changed. Additional columns or additional tables may be added when necessary and column headings may be abbreviated, and reports may be reformatted with different character spacing, line spacing, row heights or column widths to permit better readability or paper conservation. ACMs may also provide additional customized information at the bottom of the standard reports, separated from the standard report by a line.

Some of the tables in the Standard Reports are not applicable for all buildings. When a table is not applicable for a particular building, it should be omitted. When one of the standard tables is included, all the columns should be included (although column width may be reduced), even if some of the information in the columns is not applicable to the proposed design.

The Standard Reports are designed to accommodate the optional modeling capabilities included in this manual. Approval of additional optional modeling capabilities may require modification of the standard report format.

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## **2.1 Certificate of Compliance (CF-1R)**

The Certificate of Compliance (report CF-1R) is the first standard report that must be produced. The Certificate of Compliance is required by the Administrative Requirements (Title 24, Section 10).



**Heading.** The following heading shall appear on the first page.

CERTIFICATE OF COMPLIANCE: RESIDENTIAL		Page 1 of 2    CF-1R
Project Title	Filename:	Date:
Project Address	Run Title:	<runcode>
Documentation Author		<initiation time>
Telephone		Building Permit #
Compliance Method		Plan Check / Date
Location/Climate Zone		Field Check/ Date

The Filename , Run Title, Runcode, and Initiation Time need not appear in the header as shown above but must appear as part of the header information for all pages of the Certificate of Compliance.

Subsequent pages shall have the following heading.

CERTIFICATE OF COMPLIANCE: RESIDENTIAL		Page 2 of 2    CF-1R
Project Title	Filename:	Date:
	Run Title:	<runcode/initiation time>

- *Project Title, Date, Project Address, Documentation Author and Telephone, and Climate Zone (text):* Display user inputs for these fields.
- *Filename (filename.ext):* The filename of the input file used to generate the compliance form.
- *Compliance Method (text):* The Alternative Calculation Method program name and version number (e.g., CALRES2 v2.01)
- *<Runcode/Initiation Time> (alphanumeric text):* A unique runcode designation generated automatically by the ACM to identify the specific run. This number and the initiation time changes with each run initiated by the user even though the filename and Run Title may remain the same. The initiation time is the time (including the hour and minute) that the compliance run was initiated by the user.
- *Run Title (text):* Optional user input item. Use for commentary or description of unique characteristics of a particular run.

**General Information.** This listing in the Certificate of Compliance follows the first page heading on both the CF-1R and the CF2-R and provides basic information about the building. The items and information listed on the Certificate of Compliance are identical to some of the items and information found in the Computer Method Summary (C-2R). A description of these data elements is given later in this chapter.



## GENERAL INFORMATION

Conditioned Floor Area:	1384 ft <sup>2</sup>
Average Ceiling Height	10.2 ft.
Building Type:	Single Family Detached
Building Front Orientation:	15 deg (North)
Glazing Area as % of Floor Area	14.4%
Average Fenestration U-Value	0.52
Average Fenestration SHGC	0.60
Number of Stories	2
Number of Dwelling Units:	1
Floor Construction Type:	Raised Floor

**Building Insulation.** This listing summarizes the insulation levels and conditions for the opaque surfaces of the building and slab perimeters. A separate row is to be provided for each unique condition. If a radiant barrier is used for a roof, the ACM is required to report this feature. The ACM may either add a column, titled "Radiant Barrier" and place the word "Yes" in the corresponding row, or the words "Radiant Barrier" are to be automatically placed in the Location/Comments field in the row associated with the roof surface having the radiant barrier."

Metal-framed walls are reported in the frame type column. The use of metal-framed walls must be reported in the *Special Features and Modeling Assumptions* listing since metal framing reduces the effective R-value of cavity insulation by short circuiting heat flow.

## BUILDING INSULATION

Component Type	Frame Type	Cavity Insulation R-value	Sheathing Insul. R-value	Total R-value	Assembly U-value	Location/Comments
Wall	Wd2x4@16"oc	R-11	R-4	15.38	0.065	typical
Wall	Mtl2x4@16"oc	R-13	R-7	12.20	0.082	at garage
Mass Wall	n/a	R-5	R-0	6.29	0.159	Foundation
Roof	Wd2x6@24"oc	R-38	R-0	38.5	0.026	Attic w/Radiant Barrier
Roof	Wd2x10@24"oc	R-30	R-0	29.41	0.034	Vaulted Ceiling
Door	n/a	R-0	R-0	3.03	0.33	
Floor	Wd2x12@24"oc	R-19	R-0	27.03	0.037	crawl space
Floor	Wd2x10@16"oc	R-19	R-0	20.83	0.048	over garage
Slab Perimeter	n/a	R-7	n/a			F2 = 0.76 uninsulated

- **Component Type.** Possible types are wall, mass wall, door, ceiling or roof, floor over crawl space, exposed floor, slab perimeter, etc.



- **Frame Type.** Framing information shall include framing material [wood (*Wd*) or metal (*Mtl*) alternatively steel (*Stl*) or aluminum (*Alu*)], the nominal size of framing members [e.g. 2x4 for nominal 2" x 4"], and their nominal spacing [*@16"oc* for "at 16 inches on center"]. Metal framing is presumed to be steel framing unless otherwise coded.
- **Cavity Insul R-value.** The R-value of the cavity insulation alone, not including framing effects, dry wall, air films, etc. If no insulation is proposed, the response may be "none".
- **Total R-value.** The number one divided by the *Assembly U-Value* (the inverse of the *Assembly U-Value* or  $1/U_{\text{assembly}}$ ) rounded to two digits to the right of the decimal point.
- **Sheathing Insul. R-value:** The sum total R-value of continuous insulation layers which are not penetrated by framing members. These are for layers used specifically for insulation (R-2 or greater) and do not include interior or exterior finish materials such as drywall or exterior siding layers unless they have significant thermal resistance. For slabs-on-grade, report the R-value of slab edge insulation.
- **Assembly U-value.** The U-value for the assembly, including framing effects. Calculated U-values are rounded to three digits to the right of the decimal point. (U-values are calculated using standard engineering principles as documented in the Glossary, Appendix G of the *Residential Manual*<sup>1</sup> under *R-Value*)
- **Location/Comments.** A verbal description of where the component is located or other relevant information.

**Floors.** This listing summarizes floor types and surface areas. The ACM shall use this information to determine the thermal mass for the Standard Design and the default thermal mass for the Proposed Design. This listing must include all conditioned floor area and may include listings of unconditioned floor types and areas.

FLOOR TYPES AND AREAS

Construction Type	Area (ft <sup>2</sup> )	Conditioned?	Location/Description
Slab	1086	Yes	1st Floor
Slab	226	No	Garage
NonSlab	675	Yes	2nd Floor

- **Construction Type:** The construction type of the floor. Construction type is either *Slab* or *NonSlab Floor*. A *Slab* floor includes slab-on-grade floors and raised slab floors with conditioned space above and unconditioned space below. Raised slab floors with conditioned space above and below are considered *NonSlab* floors for this categorization. Floors with unconditioned space above may be either *Slab* or *NonSlab*.

<sup>1</sup>1998 Residential Manual, California Energy Commission Publication P400-98-002.



- *Area (ft<sup>2</sup>).* The area of the mass element in square feet.
- *Conditioned?:* The conditioning status of the air immediately above the floor. *Yes* indicates that the air is conditioned and *No* indicates that the air above this part of the floor is unconditioned. An ACM may exclude this column if it is clear to the user that all entries for floor area are for conditioned floor area only. If the ACM excludes this output column, the ACM must assign all user entered floor areas as conditioned floor areas and spaces with unconditioned floor areas such as sunspaces shall not be modeled.
- *Location/Description.* A verbal description of the location of the floor.

**Fenestration Surfaces.** The term "fenestration" is used to refer to an assembly of components consisting of frame and glass or glazing materials. According to the standards, fenestration includes "any transparent or translucent material plus frame, mullions, and dividers, in the envelope of a building." Fenestration surfaces include windows, skylights and glazing in doors or other transparent or translucent surfaces. This listing reports information about each fenestration surface. One row is to be included in the listing for each unique fenestration condition. When compliance is for all orientations, the building facade orientations shall be reported for the case with the "front" facing north or the orientation shall be reported as "Any", and the *Special Features and Modeling Assumptions* listings must also indicate that compliance is for all orientations.

FENESTRATION SURFACES

Fenestration #/Type/Orien	Orien-tation	Area (ft <sup>2</sup> )	Fenes.tration U-value	Fenestration SHGC	Interior Shading Att.	Exterior Shading Att.	Over-hang /Fins
1 Wdw Front	N	10	0.65	0.70			None
2 Wdw Front	NW	40	0.65	0.60	Roller-shade		None
3 Wdw Front	N	8	1.23	1.23	Blindsna	na	None
4 Wdw Left	W	110	0.65	0.65		Shade-screen	None
5 Wdw Back	S	50	0.65	0.65			Ovhg
6 Wdw Back	S	8	1.23	1.23			None
7 Wdw Right	E	85	0.65	0.65			None
8 Sky Back	S	8	1.23	1.23			None
9 Sky Horz	na	22	1.23	1.23			None

- *Fenestration Surface: Num/Type/Loc (#/text/prescribed descriptor).* *Num* is a unique number assigned by the user to each fenestration item in the fenestration surfaces list (see Computer Method Summary; C-2R). The type is Wdw (window) Dr (door) or Sky (skylight). *Loc* is the location of the surface with respect to the front of the building (Front, Back, Left, Right or na).
- *Orientation* (prescribed descriptor) is reported here as the nearest 22.5° compass point in parenthesis (N, NNE, NE, ENE etc.). *Orientation* may also be reported to the nearest degree (0°-360°) When compliance is for all orientations, orientation may



be listed as *All* or only the *Loc* need be reported or *Orientation* may be reported with Front facing North.

- *Area (ft<sup>2</sup>)*. The rough frame area of the fenestration in square feet.
- *U-value*. The rated U-value of the fenestration product, in Btu/h-ft<sup>2</sup>-°F, including air films. Calculated fenestration U-values are rounded and reported to 2 digits to the right of the decimal.
- *Fenestration SHGC*: The Solar Heat Gain Coefficient (SHGC) for this fenestration system typically the glazing plus the frame. This value corresponds to the rated value reported on a Commission-approved label, a Commission default value reported on a manufacturer's label, or a Commission default value for a carpenter's window.
- *Interior Shading Att.:* A verbal description of the interior shading attachment if an attachment other than the default drapery is proposed. Interior shades recognized by the standards include default draperies, blinds (all colors and styles), and opaque roller shades. Translucent roller shades have higher SHGCs than opaque roller shades hence they are modeled as default draperies. The Solar Heat Gain Coefficients (SHGCs) for these attachments shall be taken from the attachments listed in Table 2-1 below.

The allowed solar heat gain coefficient of the attachments shown in Table 2-1 are based on the shading performance of those products in combination with 1/8" single pane clear glass and metal framing. "*Standard*" (Default Interior Shade - Draperies) or " " (a blank field) must automatically appear in this field when no special interior shading device is included in the building plans.

Table 2-1 Allowed Interior Shading Devices and Recommended Descriptors

Recommended Descriptor	Interior Shading Attachment Reference	Solar Heat Gain Coefficient before 1/1/2002	Solar Heat Gain Coefficient after 1/1/2002
<i>Standard</i>	Draperies or No Special Interior Shading - Default Interior Shade	0.68	0.68 <sup>1</sup>
<i>Blind</i>	Venetian Blind, Vertical Blind or MiniBlind	0.47	0.47
<i>OpRollShd</i>	Opaque Roller Shades	0.47	0.68
<i>None</i> <sup>2</sup>	No Interior Shading - Only for Skylights (Fenestration tilt <60 degrees)	1.00	1.00

Note (general): No other interior shading devices or attachments are given credit for compliance with the building efficiency standards.

Note 1: Default drapery shading shall be assumed whenever no other interior shading is specified for a window. Output shall note that although *Standard* is specified, a drapery is modeled but is not required to



be installed and present at final inspection . Output shall note for any interior shading device other than drapery that it must be installed and present at final inspection.

Note 2: *None* is the default for fenestration tilted less than 60 degrees from horizontal (skylights) and is only allowed for fenestration tilted less than 60 degrees from horizontal (skylights)., i.e. *None* is not an interior shading option for ordinary vertical windows.

- **Exterior Shading Att.:** A verbal description of the exterior shading attachment, when applicable. Only a limited number of shading attachments may be used for shading credit in the performance approach. The exterior shading attachments and their allowed SHGCs are listed in Table 2-2 below:
- “Standard” (Default Bug Screen) or “ ” must automatically appear when no special exterior shading device is included in the building plans. The standard design assumes that Standard or default partial bugscreen coverage credit is used for all windows. The proposed design assumes that Standard is used for all windows unless other exterior shading attachments are specified. Standard credit has been reduced to account for the fact that bugscreens will only cover a portion of all windows in a house or residence. A user claiming credit for any ordinary bugscreens must use Standard as the input for the exterior shading device modeled.

Table 2-2 Allowed Exterior Shading Devices and Recommended Descriptors

Recommended Descriptor	Exterior Shading Device Reference	Solar Heat Gain Coefficient
<i>Standard</i>	Bugscreens or No Shading - Default Bug Screens are modeled.	0.76
<i>WvnScrn</i>	Woven SunScreen (SC<0.35)	0.30
<i>LvrScrn</i>	Louvered Sunscreen	0.27
<i>LSASnScrn</i>	LSA Sunscreen	0.13
<i>RIDownAwng</i>	Roll-down Awning	0.13
<i>RIDownBlnds</i>	Roll -down Blinds or Slats	0.13
<i>None</i> <sup>1</sup>	For skylights only - No exterior shading	1.00

Note 1: *None* is the default for fenestration tilted less than 60 degrees from horizontal (skylights) and is only allowed for fenestration tilted less than 60 degrees from horizontal (skylights)., i.e. *None* is not an exterior shading option for ordinary vertical windows.

- **Overhangs/Fins:** An indication of whether or not the fenestration is shaded by overhangs or fins [*Ovhg, Fins, Both, None*]

**Thermal Mass.** This listing summarizes thermal mass elements in the proposed design. Note that ACMs must require the input of conditioned slab floor area and the conditioned



nonslab floor area prior to the entry of special thermal mass features. These two areas determine the thermal mass for the Standard Design and the default thermal mass for the Proposed Design. The specific thermal mass for the proposed design is ONLY modeled if the thermal mass for the proposed design exceeds a specific threshold, otherwise the default thermal mass is modeled for both the Proposed and Standard Designs (See Sections 3.6 and 3.7 for more details). This *Thermal Mass* listing **must not** be reported unless the Proposed Design's thermal mass exceeds the mass credit threshold. When the thermal mass in the *Proposed Design* is greater than the threshold mass it must be reported in this format and it **must automatically** be reported in the *Special Features and Modeling Assumptions* listing and independently verified by the local enforcement agency.

## THERMAL MASS

Type/Covering	Area (ft <sup>2</sup> )	Thickness	Location/Description
Slab Exposed	120	3.5 in	Kitchen entry
Slab Covered	250	3.5 in	Kitchen dining
Nonslab	980	0	All Other
Tile	34	0.5 in	Bath

- *Type/Covering.* The type of mass and the surface condition (exposed or covered). The types described in the *Residential Manual* Glossary may be used.
- *Area (ft<sup>2</sup>).* The area of the mass element in square feet.
- *Thickness.* The mass thickness in inches.
- *Location/Description.* A verbal description of the location of the mass or other special features.

**Infiltration/Ventilation.** This listing is only produced when the applicant has used reduced infiltration measures or mechanical ventilation measures to improve the overall energy efficiency of the Proposed Design while maintaining adequate air quality. The use of reduced infiltration requires diagnostic blowerdoor testing by a certified HERS rater to verify the modeled reduced leakage area and to ensure minimum infiltration/ventilation rates are achieved. Relevant information regarding infiltration and ventilation must be reported in the *HERS Required Verification* listings on the CF-1R and the C-2R. The listings must indicate that diagnostic blower door testing must be performed as specified in ASTM E 779-87 (Reapproved 1992), *Standard Test Method for Determining Air Leakage Rate by Fan Pressurization*. This listings must also report the target CFM50<sub>H</sub> required for the blowerdoor test to achieve the modeled SLA and the minimum CFM50<sub>H</sub> (corresponding to an SLA of 1.5) allowed to avoid backdraft problems. This minimum allowed value is considered by the Commission to be “unusually tight” per the requirements of the Uniform Mechanical Code.

When the target CFM50<sub>H</sub> of the *Proposed Design* is below the value corresponding to an SLA of 3.0, mechanical ventilation with a minimum capacity of 0.047 CFM per square foot of conditioned floor area is required. This requirement for mechanical ventilation and



minimum capacity must be reported in the *HERS Required Verification* and the *Special Features and Modeling Assumptions* listings of the CF-1R and C-2R. Also, the *HERS Required Verification* listings must state that when the measured CFM50<sub>H</sub> is less than the minimum allowed value, corrective action must be taken to either intentionally increase the infiltration or provide for mechanical supply ventilation adequate to maintain the residence at a pressure greater than -5 pascals relative to the outside average air pressure with other continuous ventilation fans operating. Mechanical ventilation may also be used in conjunction with reduced infiltration to achieve even greater energy savings. When mechanical ventilation is part of the Proposed Design the exhaust and supply fan wattages must be reported in this listing and the *HERS Required Verification* listings. Whenever mechanical ventilation is modeled by the user or required by modeling an SLA of 3.0 or less, the mechanical ventilation capacity selected by the user must be greater than or equal to 0.047 cfm per square foot of conditioned floor area to be modeled by an approved ACM. If the user enters a volumetric capacity that is less than 0.047 cfm/ft<sup>2</sup>, the ACM must indicate an input error to the user and block compliance output.

When reduced infiltration or mechanical ventilation is modeled, the *Special Features and Modeling Assumptions* listings must include a statement that the homeowner's manual provided by the builder to the homeowner must include instructions that describe how to use the operable windows or mechanical ventilation to provide for proper ventilation.

INFILTRATION/VENTILATION DETAILS (*Example Listing*)

Blower Door Leakage Target (CFM50 <sub>H</sub> /SLA)	Blower Door Leakage Minimum (CFM50 <sub>H</sub> /SLA)	Vent. Fan CFM (Supply/Exhaust)	Mechanical Vent Fans (Watts) [Supply/Exhaust]
1250/2.9	586/1.5	200/300	50/75

- *Blower Door Leakage Target (CFM50<sub>H</sub> /SLA):* The measured blower door leakage in cfm at 50 pascals of pressurization and its equivalent Specific Leakage Area (SLA) value.
- *Blower Door Leakage Minimum (CFM50<sub>H</sub> /SLA):* The backdraft limit for the blower door leakage test which corresponds to a Specific Leakage Area (SLA) of 1.5 which is considered to be “unusually tight” and must satisfy the Uniform Mechanical Code requirements for “unusually tight” construction. The ACM must report in the *HERS Required Verification* listings that the Commission considers this minimum CFM and the corresponding SLA of 1.5 or less to be “unusually tight” per the Uniform Mechanical Code. In the sample listing given above a 1600 square foot house and the SLA lower limit of 1.5 is used to get the *Blower Door Leakage Minimum* shown.
- *Vent. (Ventilation) Fans (CFM):[Supply/Exhaust]* The total volumetric capacity of supply fans and exhaust fans listed separately, separated by a slash (or reported in separate columns). The balanced portion of mechanical ventilation is the smaller of these two numbers while the unbalanced portion is the difference between these two numbers. These values are reported in cubic feet per minute.



- *Mechanical Vent. (Ventilation) Fans (Watts) [Supply/Exhaust]:* The total power consumption of the supply ventilation fans and the total power consumption of the exhaust ventilation fans in watts.

**HVAC Systems.** This listing provides data on the heating and cooling systems in the building. These data are identical to those in the Computer Method Summary (Report C-2R) under "HVAC Systems" described on Page 38

#### HVAC SYSTEMS

System Name	System Type	Minimum Equipment Efficiency	Distribution Type and Location	Duct R-value
Zone=Living				
LowerHeat	GasFurnace	0.78 AFUE	DuctsCrawl	4.2
LowerAC	AirCond-Split	10.0 SEER	DuctsCrawl	4.2
Zone=Sleep				
UpperHeat	Electric	1.00 COP	Baseboard	
UpperAC	AirCond-Split	10.0 SEER	DuctsAttic	4.2

- *System Name (text):* A unique name for the HVAC system
- *System Equipment (recommended descriptor):* The type of HVAC equipment. This is specified separately from the distribution type.

Permissible equipment types: Listed in Tables 2-3 and 2.4.

In the case of *CombHydro* heating, the name of the water heating system should be identified in the previous column. When the proposed house is not air conditioned, the entry should be *NoCooling*. If more than one type of equipment is specified, each must be listed on separate rows.



Table 2-3 HVAC Heating Equipment Descriptors

Recommended Descriptor	Heating Equipment Reference
<i>CntrlFurnace</i>	Gas- or oil-fired central furnaces or heating equipment considered equivalent to a gas-fired central furnace, such as wood stoves that qualify for the wood heat exceptional method. Gas fan-type central furnaces have a minimum AFUE=78%. Distribution can be gravity flow or use any of the ducted systems. [Efficiency Metric: AFUE]
<i>Heater</i>	Non-central gas- or oil-fired space heaters, such as wall heaters floor heaters or unit heater. Equipment has varying efficiency requirements. Distribution is ductless and may be gravity flow or fan-forced.[Efficiency Metric: AFUE]
<i>Boiler</i>	Gas or oil boilers. Distribution systems can be <i>Radiant</i> , <i>Baseboard</i> or any of the ducted systems. <i>Boiler</i> may be specified for dedicated hydronic systems. Systems in which the boiler provides space heating and fires an indirect gas water heater ( <i>IndGas</i> ) may be listed as <i>Boiler/CombHydro Boiler</i> and must be listed under “Equipment Type” in the HVAC Systems listing. [Efficiency Metric: AFUE]
<i>SplitHeatPump</i>	Heating side of central split system heat pump heating systems. Distribution system must be one of the ducted systems. [Efficiency Metric: HSPF]
<i>PkgHeatPump</i>	Heating side of central packaged heat pump systems. Central packaged heat pumps are heat pumps in which the blower, coils and compressor are contained in a single package, powered by single phase electric current, air cooled, rated below 65,000 Btuh. Distribution system must be one of the ducted systems. [Efficiency Metric: HSPF]
<i>LrgPkgHeatPump</i>	Heating side of large packaged units rated at or above 65,000 Btu/hr (heating mode). Distribution system must be one of the ducted systems These include water source and ground source heat pumps. [Efficiency Metric: COP]
<i>RoomHeatPump</i>	Heating side of non-central room air conditioning systems. These include small ductless split system heat pump units and packaged terminal (commonly called “through-the-wall”) units. Distribution system must be <i>DuctIndoor</i> . [Efficiency Metric: COP]
<i>Electric</i>	All electric heating systems other than space conditioning heat pumps. Included are electric resistance heaters, electric boilers and storage water heat pumps (air-water) ( <i>StoHP</i> ). Distribution system can be <i>Radiant</i> , <i>Baseboard</i> or any of the ducted systems. [Efficiency Metric: HSPF]
<i>CombHydro</i>	Water heating system can be storage gas ( <i>StoGas</i> , <i>LgStoGas</i> ), storage electric ( <i>StoElec</i> ) or heat pump water heaters ( <i>StoHP</i> ). Distribution systems can be <i>Radiant</i> , <i>Baseboard</i> , or any of the ducted systems and can be used with any of the terminal units ( <i>FanCoil</i> , <i>RadiantFlr</i> , <i>Baseboard</i> , and <i>FanConv</i> ).



Table 2-4 HVAC Cooling Equipment Descriptors

Recommended Descriptor	Cooling Equipment Reference
<i>NoCooling</i>	Entered when the proposed building is not air conditioned or when cooling is optional (to be installed at some future date). Both the <i>Standard Design</i> equivalent building and the proposed design use the same default system (refer to sections 3 and 4). [Efficiency Metric: SEER]
<i>SplitAirCond</i>	Split air conditioning systems. Distribution system must be one of the ducted systems. [Efficiency Metric: SEER]
<i>PkgAirCond</i>	Central packaged air conditioning systems less than 65,000 Btuh cooling capacity. Distribution system must be one of the ducted systems. [Efficiency Metric: SEER]
<i>LrgPkgAirCond</i>	Large packaged air conditioning systems rated at or above 65,000 Btu/hr (cooling capacity). Distribution system must be one of the ducted systems. [Efficiency Metric: EER]
<i>RoomAirCond</i>	Non-central room air conditioning cooling systems. These include small ductless split-system air conditioning units and packaged terminal (commonly called "through-the-wall") air conditioning units. Distribution system must be <i>DuctIndoor</i> . [Efficiency Metric: EER]
<i>SplitHeatPump</i>	Cooling side of split heat pump systems. Distribution system must be one of the ducted systems. [Efficiency Metric: SEER<65,000 Btu/hr EER>65,000 Btu/hr]
<i>PkgHeatPump</i>	Cooling side of central single-packaged heat pump systems with a cooling capacity less than 65,000 Btuh. Distribution system must be one of the ducted systems. [Efficiency Metric: SEER]
<i>LrgPkgHeatPump</i>	Cooling side of large packaged heat pump systems rated at or above 65,000 Btu/hr (cooling capacity). Distribution system must be one of the ducted systems. [Efficiency Metric: EER]
<i>RoomHeatPump</i>	Cooling side of non-central, room heat pump systems. These include small ductless split-system air conditioning units and packaged terminal (commonly called "through-the-wall") units. Distribution system must be <i>DuctIndoor</i> . [Efficiency Metric: EER]
<i>EvapDirect</i>	Direct evaporative cooling systems. The SEER is set to 11.0. The default distribution system location is <i>DuctAttic</i> ; evaporative cooler duct insulation requirements are the same as those for air conditioner ducts. [Efficiency Metric: SEER]
<i>EvapIndirDirect</i>	Indirect-direct evaporative cooling systems. The SEER is set to 13.0. The default distribution system location is <i>DuctAttic</i> ; evaporative cooler duct insulation requirements are the same as those for air conditioner ducts. [Efficiency Metric: SEER]



- *Minimum Equipment Efficiency/Method (fraction/recommended descriptor):* The minimum equipment efficiency needed for compliance along with the applicable method.

Permissible Methods: *AFUE* for furnaces and boilers, *HSPF* for electric heating equipment, *SEER* for heat pumps (cooling) and central air conditioners, and *RE* for water heaters.

If equipment type is *Electric*, an HSPF of 3.413 should be entered, except for radiant systems which may use an HSPF of 3.55.

- *Distribution Type and Location (recommended descriptor):*

Permissible entries: Listed in Table 2-5



Table 2-5 HVAC Distribution Type and Location Descriptors

Recommended Descriptors	HVAC Distribution Type and Location Reference
Ducted Systems	Fan-powered, ducted distribution systems that can be used with most heating or cooling systems. When ducted systems are used with furnaces, boilers, or combined hydronic/water heating systems the electricity used by the fan shall be calculated using the methods described later in this manual. R-value must be specified in "Duct R-value" column when a ducted system is specified
<i>DuctsAttic</i>	Ducts located overhead in the unconditioned attic space
<i>DuctsCrawl</i>	Ducts located underfloor in the unconditioned crawl space
<i>DuctsGarage</i>	Ducts located in an unconditioned garage space.
<i>DuctsBasemtl</i>	Ducts located in an unconditioned basement space
<i>DuctsInEx12</i>	Ducts located within the conditioned floor space except for less than 12 lineal feet of duct, typically an HVAC unit in the garage mounted on return box with all other ducts in conditioned space.
<i>DuctsInAll</i>	HVAC unit or systems with all HVAC ducts located within the conditioned floor space, such as gas-fired wall furnaces. This category is used also for systems such as wall furnaces having a fan.
<i>DuctsOutdoor</i>	Ducts located in exposed locations outdoors.
<i>Ductless Systems</i>	Ductless radiant or warm/cold air systems using fan-forced or natural air convection and hydronic systems relying upon circulation pumps and fan-forced or natural air convection, and
<i>Furnaces</i>	Heating equipment such as wall and floor furnaces
<i>Radiant</i>	Radiant electric panels or fanless systems used with a boiler, electric or heat pump water heater, or combined hydronic heating equipment.
<i>Baseboard</i>	Electric baseboards or hydronic baseboard finned-tube natural convection systems

- *Diagnostic Duct Leakage.* If diagnostic duct leakage is specified by the user, the requirement for diagnostic testing shall be reported in the *HERS Required Verification* listings on the CF-1R and C-2R.
- *Duct R-value(hr-ft<sup>2</sup>-/F/Btu).* The installed R-value for duct insulation. The minimum value is 4.2, which is required by the mandatory measures section.

When the modeled duct R-value is larger than 4.2, the ACM must report the modeled R-value in this listing and must specify this higher duct R-value in the *Special Features and Modeling Assumptions* listings.

The modeled R-value cannot be less than 4.2 °F-ft<sup>2</sup>-hr/Btu unless an existing building and an existing HVAC distribution system is being modeled as part of an



existing plus addition analysis. When duct R-value is less than 4.2 the *Special Features and Modeling Assumptions* listings must indicate that an existing building with an existing HVAC distribution system is being modeled as part of an existing plus addition analysis.

**HVAC Distribution Systems Misc.** This listing details important information associated with the use of special HVAC distribution efficiency. The use of any of these features is considered to be special and must also be individually listed on the *HERS Required Verification* listing and individually verified.

HVAC DISTRIBUTION EFFICIENCY DETAILS (Example Listing)

System Name	Measured Duct Leakage Target (% of fan cfm / leakage cfm) <sup>1,2</sup>	Measured Duct Surface Area (ft <sup>2</sup> )	ACCA Manual D Design	Fan CFM
Primary	6%/75.6	150	Yes	1200
Bath	n/a	None	No	n/a

*Note 1: % of fan cfm is used when the HVAC system is installed at the time of testing and is based on a supply fan capacity of 400 cfm per ton of air conditioning capacity or 21.7 cfm per 1,000 Btus/hour of furnace capacity. When the HVAC is not installed or its capacity is not known the alternate leakage target reported is calculated from 6% of 0.70 cfm per square foot of conditioned floor area for Climate Zones 8 to 15 and 0.50 cfm per square foot of conditioned floor area for the remaining Climate Zones. For an 1800 square foot house in Climate Zone 13 (example shown above) the maximum duct leakage when system capacity is unknown is 75.6 cfm at 25 pascals.*

*Note 2: The HERS Required Verification listings must include the information specified in Note 1 or the results of those calculations as the method of reporting the appropriate target values for the reduced duct leakage test.*

- *System Name (text):* Descriptive name corresponding to a system name defined in the HVAC System listing.
- *Measured Duct Leakage Target (% of fan cfm/leakage cfm):* Reduced duct leakage has been modeled to determine seasonal duct efficiency. This credit requires site diagnostic testing by a certified HERS rater supervised by a Commission-approved HERS provider tested in accordance with the procedures in Appendix F. The test results must be less than 6% of fan cfm (derived from installed system capacity when present or from the default assumptions for duct efficiency calculations when the HVAC heating or cooling equipment is not installed) and reported by the HERS rater on a CF-6R form and verified by the local enforcement agency. The target duct leakage must be listed in the *HERS Required Verification* section.
- *ACCA Manual D Design (prescribed descriptor: Yes or No):* Indicates whether modeling credit for ACCA Manual D duct design has been used. When duct



efficiency credit for ACCA Manual D design is claimed, the *HERS Required Verification and the Special Features and Modeling Assumptions* listings must specify that the ACCA Manual D design, layout, and calculations be submitted to the local enforcement agency and a certified HERS rater. The certified HERS rater shall verify the existence of ACCA Manual D layout and calculations and verify that the field installation is consistent with this design.

- *Measured Duct Surface Area (ft<sup>2</sup>):* This item is applicable only if the entry for *ACCA Manual D Design* is “Yes” and documents the modeling of reduced duct surface area when a value other than na (not applicable) is reported. The *HERS Required Verification* listing must indicate that this total value and its subcomponent areas by location must be verified by a certified HERS rater. Moreover reduced duct sizes must still preserve adequate air flow to receive duct efficiency credit. Consequently credit for reduced duct surface area also requires that the HERS rater measure and report HVAC supply fan flow to verify that the manufacturer’s specified fan flow, consistent with the ACCA manual D design, has not been impaired by reduced duct sizes. The *HERS Required Verification* listing must also indicate this requirement.

When *Measured Duct Surface Area* is specified the *HERS Verification Listings* must report the supply duct surface area in each of four locations: *Attic/Outside, Crawlspace, Basement, Garage*. This listing must also report whether or not the basement where the ducts are located is conditioned or not.

**Water Heating Systems.** This listing provides information on the water heating systems used in the building and is identical to information in the listings of the Computer Method Summary (C-2R) described on Page 42. Information concerning auxiliary energy systems, the performance and features of instantaneous gas, large storage gas and indirect gas water heaters, and combined hydronic equipment, if installed, must be included in the *Special Features and Modeling Assumptions* listing if energy credit is taken for such systems. When combined hydronic systems, solar water heating, or wood stove boilers are used, ACM's must augment the Water Heating Systems listing with the inclusion of two additional listings, Water Heating Systems Misc and Water Heater/Boiler Details. The use of these optional capability features must be reported in the *Special Features and Modeling Assumptions* listing with cross references to the Water Heating Systems Misc and Water Heater/Boiler Details listings, and the content of these listings verified as *Special Features*.



## WATER HEATING SYSTEMS

System Name	Distribution Type	Water Heater Name	Water Heater Type	Number of Heaters (#)	Energy Factor	Tank Volume (gal)
Upper Floors	Recirc/Timer	State100	StorGas	3	.52	100
Lower Floors	Recirc/Timer	State50	StorGas	4	.62	50
Kitchens	POU	Loch006	InstElec	18	.98	na.

- *System Name (text)*: Unique descriptive name for the water heating system. The name must be linked to entries in the Water Heating Systems Misc and Water Heater System Assignments listings.
- *Distribution Type (recommended descriptor)*: The type of distribution system used to transport hot water from the water heater to the point of use. Qualifying requirements for these distribution systems are included in Section 6.6 of the *Residential Manual*.

Permissible types: Listed in Table 2-7

Table 2-6 Water Heating Distribution System Descriptors

Recommended Descriptor	Distribution System Reference
<i>Std</i>	Standard (non-recirculating) potable water heating system with tank storage remote from points of consumptive use
<i>POU</i>	Point-of-use potable water heating system, within 8' of fixtures
<i>HWR</i> (optional)	Standard system with hot water recovery capability
<i>Std/PIns</i>	Standard system with pipe insulation entire length of piping run
<i>ParallelPiping</i>	Individual pipes from the water heater to each point of use
<i>Recirc</i>	Recirculation system, continuous operation w/o control
<i>Recirc/Timer</i>	Recirculation system, timer controlled
<i>Recirc/Dmd</i>	Recirculation system, demand controlled
<i>Recirc/Temp</i>	Recirculation system, temperature controlled
<i>Recirc/Timer/Temp</i>	Recirculation system, timer + temperature controlled
<i>R/D&amp;HWR</i>	combination <i>Recirc/Dmd</i> + <i>HWR</i>
<i>R/D&amp;PIns</i>	combination <i>Recirc/Dmd</i> + <i>PIns</i>

- *Water Heater Name (text)*: User-defined descriptive name that is specified in the Water Heater Systems and Water Heater/Boiler Details listings.



- **Water Heater Type (recommended descriptor):** The type or category of water heater used. Permissible types: Listed in Table 2-8

Table 2-7 Water Heater Type Descriptors

Recommended Descriptor	Water Heater Reference
<i>StoGas</i>	gas <sup>2</sup> - or oil-fired storage tank $\approx$ 2 gal, input $\leq$ 75,000 Btu/hr
<i>LgStoGas</i>	gas- or oil-fired storage tank, input > 75,000 Btu/hr
<i>StoElec</i>	electric-resistance-heated storage tank $\approx$ 2 gal
<i>InstGas</i>	instantaneous gas-fired, storage < 2 gal
<i>InstElec</i>	instantaneous electric-resistance-heated, storage < 2 gal
<i>StoHP</i>	electric heat pump with storage tank
<i>IndGas</i>	storage tank indirectly heated by gas- or oil-fired source
<i>Boiler</i>	boiler dedicated solely to hydronic space heating

- **Num of Heaters (#):** The quantity of water heaters of this type in the system.
- **Energy Factor (fraction):** Applicable to all water heater types subject to National Appliance Energy Conservation Act (NAECA) regulations. Does not apply to *LgStoGas* types; for these types enter "na". If the energy factor is not published, then the water heater is not covered by NAECA and the Water Heater/Boiler Details listing must be completed.
- **Tank volume (gal):** The listed storage volume of the water heater.

**Note:** When water heaters with an Energy Factor (EF) of less than 0.58 are installed, the *Special Features and Modeling Assumptions* must list the EF of the water heater and the R-value of externally-applied insulation wrap in hr-ft<sup>2</sup>-/F/Btu as well as the mandatory R-value requirement for external insulation for these water heaters.

**Water Heating Systems Misc.** This listing details credits associated with the use of solar water heating, wood stove boilers and provides information about combined hydronic pump energy for electric combined hydronic systems. A credit may be taken for either a solar water heating system or a wood stove boiler, but not both.

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<sup>2</sup>Gas may be natural gas or propane.



## WATER HEATING SYSTEMS MISC

(Example Listing)

System Name	Solar Savings Fraction	Solar System Type	Wood Stove Boiler?	Wood Stove Boiler Pump?	Combined Hydronic Pump Power (Watts)
Hydronic	0.00	<i>None</i>	Yes	Yes	60.00
DHW	0.64	<i>Passive</i>	No	No	

- *System Name (text)*: Descriptive name corresponding to a system name defined in the Water Heating Systems listing.
- *Solar Savings Fraction (fraction)*: Fraction of the annual heating load for the system met by solar energy, if the water heating system uses a solar system to provide auxiliary heating. The Solar Savings Fraction may be determined using *f-Chart* or other methods approved by the Commission.
- *Solar System Type (prescribed descriptor)*: Defines the general type of solar system.  
Permissible types: *Active* (pump/blower assisted solar collection/circulation), *Passive* (natural collection/circulation), and *None*
- *Wood-Stove Boiler (prescribed descriptor)*: Indicates whether a wood-stove boiler is used.  
Permissible entries: *Yes* and *No*.
- *Wood-Stove Boiler Pump (prescribed descriptor)*: Indicates whether a wood-stove boiler pump is used to circulate water between the wood stove and the storage tank.  
Permissible entries: *Yes* and *No*.
- *Combined Hydronic Pump (Watts)*: Required only for electric combined hydronic (*Elec/*, *StoElec/* and *InstElec/CombHydro*) systems. Not required for storage gas/oil or heat pump combined hydronic systems (*StoGas/*, *LgStoGas/*, and *StoHP/CombHydro*).

**Water Heater/Boiler Details.** This listing provides information about the energy characteristics of the water heaters or boilers used in combined hydronic (*CombHydro*) systems and for non-NAECA water heaters; it will not be applicable to the remainder. In such cases, "na" may be reported.



## WATER HEATER/BOILER DETAILS

(Example Listing)

Water Heater Name	Recovery Efficiency (fraction)	AFUE (fraction)	Rated Input (kBtu/hr)	Standby Loss (fraction)	Tank R-value (hr-ft <sup>2</sup> -/F/Btu)	Pilot Energy (Btu/hr)
CombHydState 100	0.78	na	60.00	na	na	na
BigRmWH	0.79	na	75.00	0.04	15.30	na

- *Water Heater Name (text):* Name of water heater specified in the Water Heating Systems listing. In the case of a hydronic system heater, the name should be descriptive of this function to distinguish it from any domestic water system heaters.
- *Recovery Efficiency (fraction):* Recovery efficiency is the performance measure for instantaneous gas water heaters (*InstGas*), large storage gas/oil water heaters (*LgStoGas*) and indirect gas/oil water heaters (*IndGas*). It is also required for storage gas/oil water heaters (*StoGas*) used in combined hydronic systems (*CombHydro*). The value is taken from the Commission's appliance databases<sup>3</sup> or from the manufacturer's literature. If the value is omitted for NAECA regulated water heaters, then the default value will be assumed. When boilers are used to fire an indirect gas/oil water heater (*IndGas*), the value of the AFUE (see below) is used for the recovery efficiency.
- *AFUE (fraction):* Annual Fuel Utilization Efficiency, the heating efficiency of the water heater based upon approved test methodologies. Values of AFUE are listed in the Commission's directories cited above.
- *Rated Input (kBtu/hr):* The energy input rating from the above directories or from the manufacturer's literature. Entries are required for large storage gas/oil water heaters (*LgStoGas*), indirect gas/oil water heaters (*IndGas*), and when storage gas water heaters (*StoGas/LgStoGas*) or heat pump water heaters (*StoHP*) are used in combined hydronic space heating systems (*CombHydro*).

<sup>3</sup> The complete appliance databases can be downloaded from the Energy Commission's Internet FTP site (<ftp://sna.com/pub/users/eff-tech/appliances>). This requires database software (spreadsheet programs cannot handle some of the larger files). To use the data, a user must download the database file (or files), download a brand file and a manufacturer file and then decompress these files. Then download a description file that provides details on what is contained in each of the data fields. With these files, and using database software, the data can be sorted and manipulated. Directories approved by the Commission may also be used. Currently the Commission has approved the Gas Appliance Manufacturers Association (GAMA) *Consumers' Directory of Certified Efficiency Ratings for Residential Heating and Water Heating Equipment* directory to be used to verify certification on *some* residential appliances. The GAMA directory (Sections I and II) can be used for gas furnaces, boilers and water heaters.



- *Standby Loss (fraction)*: The fractional storage tank energy loss per hour during non-recovery periods (standby) taken from the Commission's directories cited above. Applicable only to large storage gas water heaters (*LgStoGas*).
- *Tank R-value (hr-ft<sup>2</sup>-F/Btu)*: The total thermal resistance of the internally-insulated tank and any external insulation wrap. Applicable to large storage gas/oil (*LgStoGas*) and indirect gas/oil (*IndGas*) water heaters only.
- *Pilot light (Btu/hr)*: The pilot light energy consumption rating from one of the Commission's directories, cited above. Applicable only to instantaneous gas (*InstGas*) and indirect gas/oil (*IndGas*) water heaters.

**Special Features and Modeling Assumptions.** This listing must **stand out and command the attention** of anyone reviewing this form to emphasize the importance of verifying these Special Features and the aspects of these features that were modeled to achieve compliance or the energy use results reported. This listing in the Certificate of Compliance must include any special features of the building that affect the building's compliance with the standards and which are not described elsewhere on the Certificate of Compliance. For example, water heating features, or auxiliary credits must be listed under "*Special Features and Modeling Assumptions*" as well as being listed under a special listing of their own. The use of certain non-default values must also be included in this list. These special default values are indicated in the subsequent text. This listing should also include any variations in building features necessary to achieve compliance in multiple orientations.

SPECIAL FEATURES AND MODELING ASSUMPTIONS: (Example Listing)      Plan      Field

This house has Zonal control with multiple zones, interzone surfaces, and interzone ventilation.		
This building uses metal-framed walls that must meet mandatory insulation requirements. In this case R-7 sheathing has been used in addition to the R-13 cavity insulation. for these walls.		
This house has an attached sunspace with interzone surfaces ,custom solar heat gain distribution and sunspace thermal mass elements		
This house is modeled with reduced infiltration and/or mechanical ventilation. Consequently the homeowner's manual provided by the builder to the homeowner must include operating instructions for the homeowner on how to use operable windows and/or mechanical ventilation to achieve adequate ventilation.		

**HERS Required Verification.** Specific features that require diagnostic testing to assure proper installation require field testing and verification by a certified home energy rater (HERS rater) under the supervision of a CEC- approved HERS provider, and must be listed in this section. This listing must **stand out and command the attention** of anyone reviewing this form to emphasize the importance of HERS verification of these features and the aspects of these features that were modeled to achieve compliance. or the energy use results reported.

All items in the *HERS Required Verification* listings must also report that the installer and HERS rater must both provide the appropriate CF-6R documentation for proper installation, testing, and test results for the features that require verification by a HERS



rater. The installer must document and sign the CF-6R to verify compliance with design and installation specifications. The HERS rater must document and sign the CF-6R to confirm the use of proper testing procedures and protocol, to report test results, and to report field verification of installation consistent with the design specifications needed to achieve these special compliance efficiency credits.

The ACM must ask the user if there are vented combustion appliances inside the conditioned space that draw air for combustion from the conditioned space prior to any entry for reduced infiltration or mechanical ventilation. Cooking appliances, refrigerators and domestic clothes dryers are excluded from this requirement. If appliances other than cooking appliances, refrigerators and domestic clothes dryers are present and use conditioned air for combustion, the ACM must instruct the user that reduced infiltration must not be modeled when these devices are part of the Proposed Design and block data entries and ACM modeling of reduced infiltration and mechanical ventilation. When the user indicates that such devices are present or when the user models reduced infiltration or mechanical ventilation, the ACM must report in the *Special Features and Modeling Assumptions* listings that reduced infiltration and/or mechanical ventilation are prohibited from being modeled when vented combustion appliances, not excluded above, are inside conditioned space.

When a *Proposed Design* is modeled with a reduced target infiltration (CFM50<sub>H</sub>) that corresponds to an SLA less than 3.0, mechanical ventilation is required and must be reported in the *HERS Required Verification* listings.

HERS REQUIRED VERIFICATIONS : (Example Listing)	Plan	Field
This house is using reduced duct leakage to comply and must have diagnostic site testing of duct leakage performed by a certified HERS rater under the supervision of a CEC-approved HERS provider. The results of the diagnostic testing must be reported on a CF-6R form and list the target and measured CFM duct leakage at 25 pascals.		
This house has tight construction with reduced infiltration and a target blower door test range between 586 and 1250 CFM at 50 pascals. The blower door test must be performed using the ASTM <i>Standard Test Method for Determining Air Leakage Rate by Fan Pressurization</i> , ASTM E 779-87 (Reapproved 1992).		
WARNING: If this house tests below 586 CFM at 50 pascals, the house must either be provided with a ventilation opening that will increase the tested infiltration to at least 586 CFM at 50 pascals (SLA = 1.5) OR mechanical supply ventilation must be provided that can maintain the house at a pressure of at least -5 pascals relative the outside average air pressure while other continuous ventilation fans are operating. Note also that the Commission considers an SLA≤1.5 to be "unusually tight" per the Uniform Mechanical Code.		
WARNING - Houses modeled with reduced infiltration are prohibited from having vented combustion appliances other than cooking appliances, refrigerators and domestic clothes dryers that use indoor air for combustion inside conditioned space.		

**Compliance Statement and Signatures.** Signature requirements and other details on the compliance statement are included in Section 1.3 of the *Residential Manual*.



COMPLIANCE STATEMENT

This certificate of compliance lists the building features and performance specifications needed to comply with the Energy Standards in Title 24, Parts 1 and 6, of the California Code of Regulations, and the Administrative regulations to implement them. This certificate has been signed by the individual with overall design responsibility. When this certificate of compliance is submitted for a single building plan to be built in multiple orientations, any shading feature that is varied is indicated in the *Special Features and Modeling Assumptions* section.

<b>Designer or Owner (per Business &amp; Professions Code)</b>  Name _____ Title/Firm _____ Address _____ City & Zip Code _____ Telephone _____ License Number _____ Signature/Date _____	<b>Documentation Author</b>  Name _____ Title/Firm _____ Address _____ City & Zip Code _____ Telephone _____ Signature/Date _____
<b>Enforcement Agency</b>  Name _____ Title _____ Agency _____ City _____ Telephone _____ Signature/Date _____	



## 2.2 Computer Method Summary (C-2R)

The second standard report, that must be automatically produced, gives more detail about the program inputs. The Computer Method Summary must always accompany the Certificate of Compliance when the computer performance approach is used.

The Computer Method Summary shall include all information provided by the program user.

Information on the Computer Method Summary is provided below to illustrate the use of all the standard tables.

**Report Heading.** The following heading shall appear on the first page of each Computer Method Summary.

COMPUTER METHOD SUMMARY		Page 1 of 4	C-2R
Project Title	Filename:	Date:	
Project Address		<runcode>	
Documentation Author		<initiation time>	
Telephone		Building Permit #	
Compliance Method		Plan Check / Date	
Climate Zone		Field Check/ Date	

The following heading shall appear on subsequent pages.

COMPUTER METHOD SUMMARY		Page 2 of 4	C-2R
Project Title	Filename:	Date:	
	<runcode/initiation time>		

**Energy Use Summary.** This section compares the energy use of the proposed building to the energy budget of the standard design building. All units in this table are source kBtu/ft<sup>2</sup>-year. Energy is shown for space heating, space cooling and hot water. The space heating and cooling energy budgets are determined from the standard design using the custom budget method. The water heating budget is calculated from the water heating budget equation contained in the standards. ACM vendors may add additional columns to this report when appropriate, such as for multi-zone building analyses.



ENERGY USE SUMMARY (kBtu/ft<sup>2</sup>-yr)

	Standard Design Energy Budget	Proposed Design Energy Use
Space Heating	23.45	21.23
Space Cooling	10.34	8.23
Water Heating	15.90	14.67
Total	49.69	44.13

Additional rows may be added to the table when necessary to accommodate energy uses that are to be included in the analysis but cannot be easily assigned to one of the three principal categories. For example, an additional row for miscellaneous electrical energy may be required if electric equipment energy use cannot be assigned separately to heating, cooling or hot water.

**General Information.** This section contains general information about the project.

## GENERAL INFORMATION

Conditioned Floor Area:	1384 ft <sup>2</sup>
Building Type:	Single-family detached
Building Front Orientation:	0 deg (North)
Number of Dwelling Units:	1
Number of Stories:	1
Floor Construction Type:	Slab on grade
Number of Conditioned Zones:	2
Total Conditioned Volume:	11072 cf
Conditioned Slab Floor Area:	1384 ft <sup>2</sup>
Total Conditioned Floor Area:	1384 ft <sup>2</sup>

- *Conditioned Floor Area.* The conditioned floor area of all building zones modeled in the computer run.
- *Building Type.* The type of building. Possible types are single-family detached, single-family attached (which includes duplexes and halfplexes) multi-family (all other attached dwellings including condominiums), addition alone, addition plus existing, or alteration.
- *Building Front Orientation.* The azimuth of the front of the building. This will generally be the side of the building where the front door is located. A typical reported value would be "290° (west)". This would indicate that the front of the building faces north 70° west in surveyors terms. The closest orientation on 45° compass points should be verbally reported in parenthesis, e.g. north, northeast, east, southeast, south, southwest, west or northwest. When compliance is shown for multiple orientations, "all orientations" may be reported. When "all orientations" is



reported, the *Special Features and Modeling Assumptions* listing shall describe shading features that vary with orientation.

- *Number of Dwelling Units.* The total number of dwelling units in the building. This number may be a fraction for cases of addition alone.
- *Number of Stories.* The number of building stories as defined by the *Uniform Building Code*.
- *Floor Construction Type.* The floor construction type determines the basis of the custom budget or the standard design building; choices are slab or nonslab. Rules for determining the type of floor construction are discussed in Chapter 3 of this Manual.
- *Number of Conditioned Zones.* The number of conditioned zones modeled in the computer run.
- *Total Conditioned Volume.* The total volume of conditioned space within the building.
- *Conditioned Slab Floor Area.* The total area of slab floor (on grade or raised) with conditioned space above and the ground or unconditioned space below. This is used to determine the standard design mass requirement for buildings and the default values of the thermal mass requirements for the proposed design.
- *Total Conditioned Floor Area.* The total floor area of conditioned space in the building to be permitted. This area must be no less than the *Conditioned Slab Floor Area* specified above. The conditioned nonslab floor area is the difference between the *Total Conditioned Floor Area* and the *Conditioned Slab Floor Area* and is used to determine the thermal mass for the Standard Design, the default value of thermal mass for the Standard Design, and the threshold thermal mass requirement for thermal mass credit in the Proposed Design. The conditioned nonslab floor area includes any nonslab floors, raised or not, and raised slab floors with conditioned space above and below the floor.

**Building Zone Information.** For most compliance documentation, only one row will be reported in this table. Additional rows are reported when a proposed building is modeled as two zones (zonal control), or when attached, unconditioned spaces are modeled, such as crawl spaces or sunspaces.

BUILDING ZONE INFORMATION

Zone Name	Floor Area (ft <sup>2</sup> )	Volume (ft <sup>3</sup> )	# of Units	Zone Type	Tstat Type	Vent Height (ft)	Vent Area (ft <sup>2</sup> )
House	1384	11072	1	Conditioned	Setback	2.0	32

- *Zone Name.* Each zone is given a name that is used to categorize information in the following tables.



- *Floor Area (ft<sup>2</sup>)*. The floor area of the zone measured to outside wall. The sum of the floor area of all conditioned zones must equal the conditioned floor area reported under "General Information".
- *Volume (ft<sup>3</sup>)*. The volume of the zone. The sum of the volume of all conditioned zones must equal the total volume reported under "General Information".
- *# of Units*. The number of dwelling units in the zone. This number may be a fraction for cases of addition alone or a building in which there are more zones than dwellings.
- *Zone Type*. This description controls some modeling restrictions, such as infiltration, internal and solar gains, etc. Possible conditioned zone entries are Conditioned, Living and Sleeping. Possible unconditioned zone entries include Unconditioned, CVCrawl and Sunspace.
- *Thermostat Type*. Possible conditioned zone entries are Setback, NoSetback, LivingStat, SleepingStat. Additional thermostat types may be allowed for optional modeling capabilities.
- *Vent Height (ft)*. The height difference between the "inlet" ventilation area and the "outlet" ventilation area. The default ventilation height is determined by the number of stories: one story - 2 feet, two or more stories - 8 feet. Different vent heights may be modeled but a non-default vent height is considered a special feature or special modeling assumption that must be reported in the *Special Features and Modeling Assumptions* listing for special verification. The ventilation height for other windows is the average height difference between the centers of the lower operable window openings and the centers of the upper operable window openings.
- *Vent Area (ft<sup>2</sup>)*. This entry is either the default vent area which is assumed by the ACM based on entries in the Fenestration Surfaces table or some other value entered by the user. A Vent Area value greater than 10% of the total rough-out opening area (all windows treated as opening type: "slider") of all fenestration must be reported in the *Special Features and Modeling Assumptions* listing for special verification.

**Opaque Surfaces.** A row shall be reported in this table for each unique opaque surface in the proposed building. Opaque surfaces include walls, roofs, floors and doors.

For buildings that are modeled as multiple thermal zones, the opaque surfaces shall be grouped for each zone and indicated with a header "Zone = <ZoneName>". The zone name used in the header should be the same as the name used in the table titled "Building Zone Information"



## OPAQUE SURFACES

Surface Type	Area (ft <sup>2</sup> )	U-Value	Cavity Insul R-value	Sheath. Insul. R-value	Total R-value	True Azimuth	Tilt	Solar Gains	Form Reference	3 Location/ Comments
Zone=Living										
Wall	105.4	0.088	R-13	na	11.30	0	90	Yes	Wall-1	Typical
Wall	145.4	0.068	R-11	R-4	14.69	180	90	Yes	Wall-1	Typical
Base WallA	100	0.124	na	R-6	8.08	0	90	No	BWall-1	0-2 ft below grade
Base Wall B	160	0.124	na	R-6	8.08	0	90	No	BWall-2	2-6 ft. below grade
Wall	176.8	0.088	R-13	na	11.30	270	90	Yes	Wall-1	Typical
Roof	692	0.031	R-30	na	32.48	0	0	Yes	Roof-1	Typical
Door	40	0.330	na	na	3.03	0	90	Yes	Door-1	Typical
Zone=Sleep										
Wall	145.4	0.088	R-13	na	11.30	0	90	Yes	Wall-1	Typical
Wall	176.8	0.068	R-11	R-4	14.69	90	90	Yes	Wall-1	Typical
Wall	145.4	0.088	R-13	na	11.30	180	90	Yes	Wall-1	Typical
Roof	692	0.031	R-30	na	32.48	0	0	Yes	Roof-1	Typical
Zone=SunSpc										
Wall	72	0.088	R-13	na	11.30	90	90	Yes	Wall-1	Sunspace Wall
Wall	90	0.088	R-13	na	11.30	180	90	Yes	Wall-1	Sunspace Wall
Wall	72	0.088	R-13	na	11.30	270	90	Yes	Wall-1	Sunspace Wall
Roof	135	0.031	R-30	na	32.48	0	0	Yes	Roof-1	Sunspace Roof

- *Surface Type.* Valid types are Wall, BaseWallA (0-1.99 ft below grade), BaseWallB (2.0-5.99 ft below grade) , BaseWallC (more than 6 ft below grade), Roof/Ceiling, and Floor. If floor is over a crawl space (FlrCrawl), then the U-values used in the custom budget run are based on having a crawl space. Otherwise, they are not. Floor types and areas are also used to determine the default thermal mass for the Proposed Design and the thermal mass for the Standard Design.
- *Area (ft<sup>2</sup>).* The area of the surface.
- *Assembly U-value.* The overall U-value of the surface assembly. (U-values are calculated using standard engineering principles as documented in the *Residential Manual*<sup>4</sup>, Appendix G and Appendix H.
- *Cavity Insul R-val.* The rated R-value of the installed insulation in the cavity between framing members. This does not include framing effects or the R-value of drywall, air films, etc. When insulating sheathing is installed over a framed wall, the "Cavity Insul R-val" should report the insulation in the cavity only.

<sup>4</sup> 1998 Residential Manual, California Energy Commission Publication P400-98-002.



- *Sheath Insul R-val.* The sum total rated R-value of all installed layers of insulating sheathing (R-2 or greater). Multiple sheathing layers must report the total of the sum of the R-values for all insulating sheathing layers. Gypsum board and exterior siding layers are not included unless they have an R-value greater than 2.0. Cavity insulation is not reported. The R-values of air films are not included
- *Total R-value.* The total R-value of the opaque surface assembly. This includes framing effects and the R-value of drywall, air films, etc. For below grade walls this value does not include the outside air film nor the R-value of the adjacent soil or gravel. For raised floors over a crawlspace, this value does not include the R-value for the crawlspace.
- *True Azimuth.* The actual azimuth of the surface after adjustments for building rotation. There are various ways of describing the orientation or azimuth of surfaces. For ACMs approved by the CEC, a standard convention must be used. The azimuth is zero degrees for surfaces that face exactly north. From this reference the azimuth is measured in a clockwise direction. East is 90 degrees, south 180 degrees and west 270 degrees.
- *Tilt.* The tilt of the surface. Vertical walls are 90°; flat roofs are 0°; floors are 180°.
- *Solar Gains.* A yes/no response is given to indicate if a surface receives solar gains. Surfaces that do not receive solar gains may include floors over crawl spaces and walls adjacent to garages. Only a yes/no response is required since the surface absorptance is a fixed input.
- *Form 3 Reference.* A reference to attached Form 3's that may accompany the compliance documentation. This name may also be referenced from the thermal mass table to indicate an exterior mass wall.
- *Location/Comments.* User provided text describing where the surface is located or other relevant information.

**Perimeter Losses.** This table provides details about components of the building envelope that are modeled as perimeter losses. Typical perimeter losses are slab edge losses, retaining wall losses, and losses from the base of controlled ventilation crawl spaces. A row is provided in the table for each unique perimeter element. Note that a single F2 factor is reported for slab edge losses for slab floor interiors that are carpeted or exposed based on a fixed assumption of 20% of the edge adjacent to exposed slab. This assumption must be used and separate F2 values for different interior covering conditions may not be reported or modeled by an approved ACM.

For buildings that are modeled as multiple thermal zones, the items shall be grouped for each zone and indicated with a header "Zone = <ZoneName>". The zone name used in the header should be the same as the name used in the table titled "Building Zone Information"



## PERIMETER LOSSES

Perimeter Type	Length (ft)	F2 Factor	Insul R-val	Insul Depth (in)	Location/Comments
Zone=Living					
SlabEdge	76	0.75	R-3	8	Exposed edge
Zone=Sleep					
SlabEdge	76	0.75	R-3	8	Exposed edge
Zone=SunSpc					
SlabEdge	65	0.90	R-0	na	Exposed edge

- *Perimeter Type.* The perimeter type. Possible types are slab edge, crawl space perimeter, etc. Names may be abbreviated.
- *Length (ft).* The perimeter length in feet.
- *F2 Factor.* The perimeter heat loss factor (see Section 4.22).
- *Insul R-Val.* The R-value of the installed insulation. "R-0" or "None" should be reported when no insulation is installed.
- *Insul Depth (in).* The depth that the insulation extends below the top surface of the slab in inches.
- *Location/Comments.* User provided information on the location of the perimeter element or other relevant information.

**Fenestration Surfaces.** This listing must include information about each fenestration surface in the proposed building. Fenestration surfaces include windows, skylights and glazing in doors or other transparent or translucent surfaces. One row is included in the listing for each unique fenestration condition. This listing must also report a note that the SHGC values for fenestration must be taken from an approved label or from the default table in the standards. Default table values for SHGC can only be used when the ACM automatically selects the default based upon other user inputs for the fenestration. ACMs must restrict users to select from a limited list of interior and exterior shading devices and their associated solar heat gain coefficients (SHGCs), namely, those devices and SHGCs listed in Table 2-1 for interior shading devices and those devices and SHGCs in Table 2-2 for exterior shading devices. ACMs shall not allow users to enter custom shading devices nor account for differences in alternative color, density, or light transmission characteristics. Translucent roller shades must be treated as drapes. ACM's are required to calculate, but not report,  $SHGC_{open}$  and  $SHGC_{closed}$  using 1998 Standards calculation procedures and assumptions.

For buildings that are modeled as multiple thermal zones, the fenestration surfaces shall be grouped for each zone and indicated with a header "Zone = <Zone Name>". The zone name used in the header should be the same as the name used in the table titled "Building Zone Information"



## FENESTRATION SURFACES

Fenestration #/Type/Orien	Area (ft <sup>2</sup> )	U-Value	Fenes. SHGC	True Az	Tilt	Exterior Shade Type /SHGC	Interior Shade Type/SHGC
Zone=Living							
1 Wdw Front(N)	70.4	0.65	0.88	0	90		Blinds/ 0.47
2 Wdw Left(E)	70.4	0.65	0.88	90	90	WveScrn/ 0.39	StdDrp/ 0.68
Zone=Sleeping							
3 Wdw Back(S)	70.4	0.65	0.88	180	90		RllrShd/ 0.47
4 Wdw Right(W)	70.4	0.65	0.88	270	90	LvrScrn/ 0.36	StdDrp/ 0.68

- *Fenestration #/Type/Orien.* The # is a unique number for each different fenestration surface entry. The type is Wdw (window) Dr (door) or Sky (skylight). The *Orien* (orientation) is the side of the building (front, left, right or back) followed by the nearest 45° compass point in parenthesis (N, NE, etc.). When compliance is for all orientations, only the side of the building may be reported (front, right, etc.)
- *Area (ft<sup>2</sup>).* The area of the surface in square feet. This should generally be the rough frame opening.
- *U-value.* The rated U-value of the fenestration product, in Btu/h-ft<sup>2</sup>-°F.
- *True Azimuth.* The true (or actual) azimuth of the glazed surface after adjustment for building rotation. The convention for describing the azimuth is standardized as discussed above under opaque surfaces.
- *Tilt.* The tilt of the glazed surface. Most windows will have a 90° tilt. Skylights typically have a tilt equal to the corresponding roof surface.
- *Fenestration SHGC :* The solar heat gain coefficient of the fenestration.
- *Exterior Shade Type/SHGC.* The type of exterior shading device and its solar heat gain coefficient from Table 2-2. "Standard/0.76" or " " must appear when no special exterior shading device is included in the building plans. *Standard (partial bugscreen)* shading shall automatically be given for all window area without other forms of exterior shading devices. This shading assumes that a portion of the window area is covered by bugscreens. Other valid exterior shades include louvered screens (*LvrScrn*), woven sunscreen (*WvnScrn*), and Low Sun Angle Sunscreen (*LSASnScrn*). When used for compliance purposes, ACMs shall not allow or accept input for user-defined exterior shades.
- *Interior Shade Type/SHGC.* The type of interior shading device and its solar heat gain coefficient from Table 2-1. "Standard/0.68" or " ", (no special interior shading or any drapery) must appear when no other interior shading device is included in the building plans and specifications. Output shall indicate that the default devices - in this case draperies - are not required to be installed even if *Standard* appears on an output list. Note that this default category now covers all types of draperies including all colors and weave densities. Two other types of interior shading devices may be



specified: *Blinds* and *RollrShd* (opaque roller shades). **Translucent roller shades** are classified as **default draperies** (*Standard*). No other interior shading devices or attachments are recognized or given credit in the standards.

**Solar Gain Targeting.** This table is only used for special cases, such as sunspaces (an optional modeling capability, and hence a Special Feature). Solar gains that enter conditioned spaces must be targeted to the air, but when glazing surfaces enclose unconditioned spaces, such as sunspaces, the user is allowed to target all but 25% of the solar gains from these surfaces to mass elements located within the unconditioned space. More than one row of targeting data may be included for each glazed surface. Unassigned solar gain is targeted to the air in the unconditioned space. At least 25% of the solar gain from any sunspace fenestration surface must be targeted to high surface area lightweight mass or the air. At most 60% of the solar gain may be targeted to the slab floor of a sunspace, especially in the summer. An ACM must automatically enforce these limits and inform the user of any attempt to exceed these limits.

Note that the use of any optional capability such as sunspace modeling must be reported in the *Special Features and Modeling Assumptions* listings. In addition, solar gain targeting must be separately reported in the *Special Features and Modeling Assumptions* listings so that the local enforcement agency can verify that these inputs are reasonable.

SOLAR GAIN TARGETING

Fenestration #/Type/Orien	Mass Name	Winter Fraction	Summer Fraction
1 Wdw Front(N)	SSS1b	0.30	0.30

- *Fenestration #/Type/Orien.* The fenestration surface which transmits solar gain to an interior unconditioned space thermal mass. This corresponds to an item in the fenestration surfaces table.
- *Mass Name.* The name of the mass element to which solar gains are directed. The mass name corresponds to an item in the thermal mass table.
- *Winter Fraction.* The fraction of solar gains targeted from the glazing surface to the absorbing thermal mass when the building is in a heating mode.
- *Summer Fraction.* The fraction of solar gains targeted from the glazing surface to the absorbing thermal mass when the building is in a cooling mode.

**Overhangs.** Overhangs are a minimum ACM capability and are described in this table.



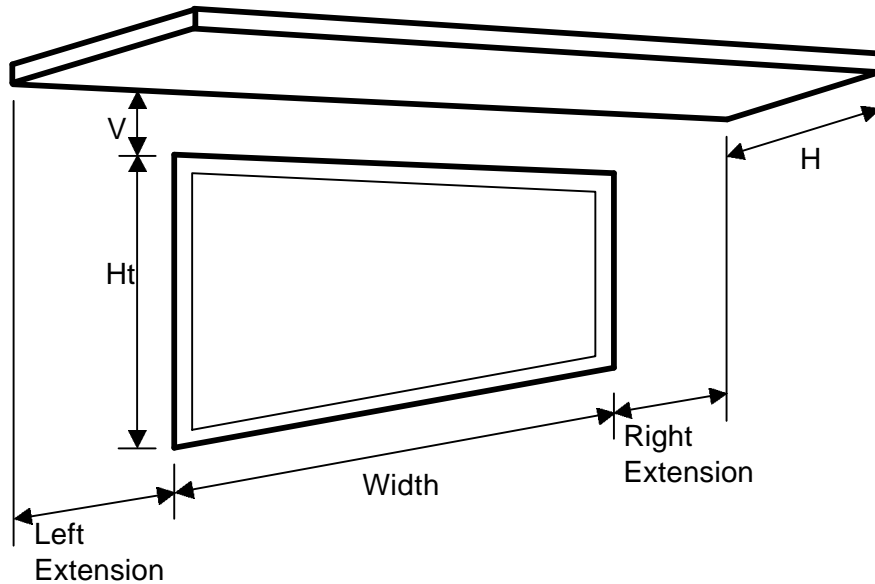


Figure 2-1 - Overhang Dimensions

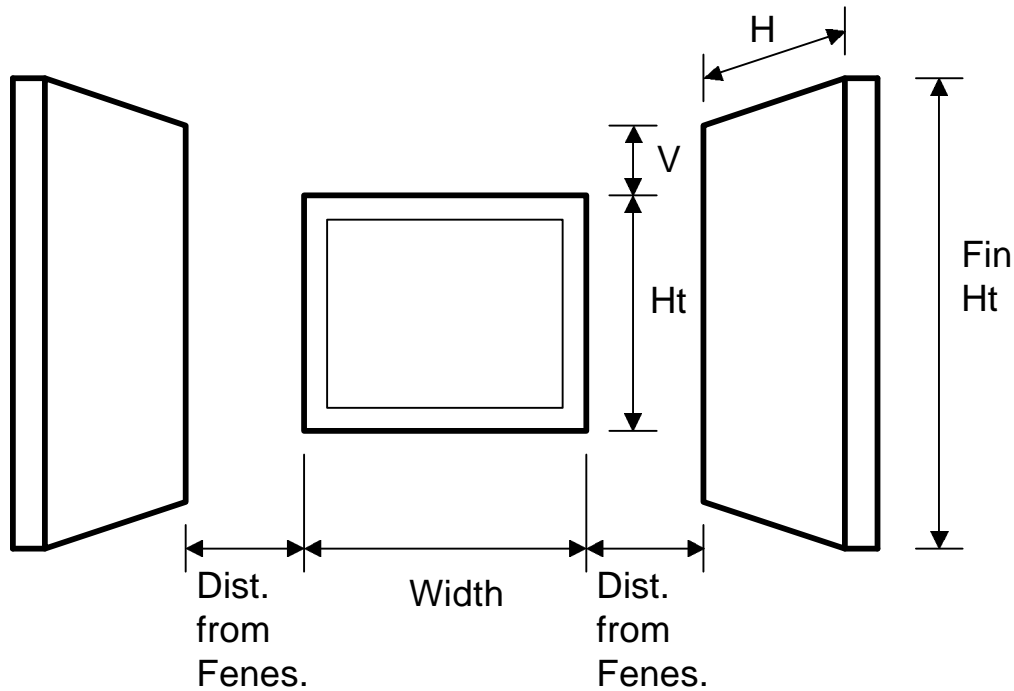
## OVERHANGS

Fenestration			Overhang			
#/Type/Orien	Width	Ht	Length "H"	Ht "V"	Left Extension	Right Extension
3 Wdw Back(S)	4.0	5.0	2.6	1.5	6.0	6.0

- *Fenestration #/Type/Orien.* This corresponds to an item in the fenestration surfaces list.
- *Fenestration Width.* The width of the rough-out frame opening for the fenestration (in feet) measured from the edge of the opening on one side to the edge of the opening on the other side.
- *Fenestration Ht.* The height of the rough-out frame opening for the fenestration (in feet) measured from the bottom of the opening or frame to the top of the opening or frame.
- *Overhang Length "H".* The horizontal distance in feet from the surface of the glazing to the outside edge of the overhang.
- *Overhang Ht "V".* The vertical distance (in feet) from the top of the glazing frame to the bottom edge of the overhang at the distance "H" from the glazing surface. See Figure 2-1.
- *Overhang Left Extension.* The distance in feet from the left edge of the glazing frame to the left edge of the overhang. "Left" and "right" are established from an exterior view of the window.
- *Overhang Right Extension.* The distance in feet from the right edge of the glazing frame to the right edge of the overhang.



**Side Fins.** Side fins are an optional capability. If an ACM does not provide this option, then this table is not used.



Figure

2-2 - Side Fin Dimensions

## SIDE FINS

Fenestration			Left Fin				Right Fin			
#/Type/Orien	Wdth	Ht	Dist from fenes	Lngh "H"	Ht "V"	Fin Ht	Dist from fenes	Lngh "H"	Ht "V"	Fin Ht
3 Wdw Back(S)	4.0	5.0	6.0	2.0	6.0	8.0	6.0	2.0	6.0	8.0

- *Fenestration #/Type/Orien.* This must correspond to an item in the fenestration surfaces list.
- *Fenestration Wdth.* The width of the rough-out opening for the fenestration (in feet) measured from the edge of the opening or frame on one side to the edge of the opening or frame on the other side.
- *Fenestration Ht.* The height of the rough-out opening for the fenestration (in feet) measured from the bottom of the opening or frame to the top of the opening or frame.
- *Left Fin Dist from fenes.* The distance in feet from the nearest glazing frame edge to the fin. "Left" and "right" are established from an exterior view of the window.
- *Left Fin Lngh "H".* The horizontal distance in feet from the surface of the glazing to the outside edge of the fin..



- *Left Fin Ht "V"*. The vertical distance (in feet) from the top of the glazing frame to the top edge of the fin.
- *Left Fin, Fin Ht*. The height of the fin, in feet.
- *Right Fin*. Similar to Left Fin items.

**Inter-Zone Surfaces.** This listing is used only for proposed designs modeled as multiple thermal zones which is considered an exceptional condition and must also be listed in the *Special Features and Modeling Assumptions* listings for the CF-1R and the C-2R. The *Special Features and Modeling Assumptions* listing must direct plan and field checkers to the listings for *Interzone Surfaces* and *Interzone Ventilation*. The *Interzone Surfaces* listing describes the characteristics of the surfaces that separate the zones.

For buildings that are modeled with more than two thermal zones, the inter-zone surfaces shall be grouped so that it is clear which zones are separated by the surfaces. The groupings shall be labeled "Between ZoneName1 and ZoneName2" or some similar convention.

#### INTER-ZONE SURFACES

Surface Type	Area (ft <sup>2</sup> )	U-value	Cavity Insul R-val	Sheath Insul R-valu	Form 3 Reference	Location/Comments
Between Living and Sunspc						
Wall	100	0.09	R-11	na	Wall-2	Insulated partition
Glass	30	1.10	SglGls	na		Sliding glass door
Between Sleeping and Sunspc						
Wall	220	0.09	R-11	R-4	Wall-2	Insulated partition
Glass	10	1.10	SglGls	na		Window
Between Living and Sleeping						
Wall	206	0.293	R-0	na	Wall-3	Gypsum partitions
Door	40	0.33	R-0	na		Hollow core doors

- *Surface Type*. The type of surface separating the zones. Possible types are window, wall, etc.
- *Area (ft<sup>2</sup>)*. The area of the surface in square feet that separates the zones.
- *U-val*. The U-value of the surface.
- *Cavity Insul R-val*. The R-value of insulation installed in cavity of the framed construction assembly. This does not account for framing effects, drywall, air films, etc.
- *Sheath Insul R-val*. The total R-value of all insulation layers (layers R-2 or greater) not penetrated by framing. Excludes low R-value layers such as sheetrock, building paper, and air films.
- *Form 3 Reference*. A reference to attached Form 3's that may accompany the compliance documentation.



- *Location/Comments.* User provided information on the location of the inter-zone surface or other relevant information.

**Inter-Zone Ventilation.** This listing is used for proposed designs that are modeled as multiple building zones. The modeling of multiple building zones is considered an exceptional condition that must be reported in the *Special Features and Modeling Assumptions* listings which must also refer to the information in this listing when this listing is generated by the ACM to echo user inputs for Inter-Zone Ventilation. If inter-zone ventilation is modeled, it must be reported in this listing. It describes natural and/or mechanical ventilation systems that separate the zones.

For buildings that are modeled with more than two thermal zones, the inter-zone ventilation items shall be grouped so that it is clear which zones are linked by the items. The groupings shall be labeled "Between ZoneName1 and ZoneName2" or some similar convention.

#### INTER-ZONE VENTILATION

Vent Type	Inlet Area	Outlet Area	Height Diff.	Fan Watts	Fan Flow (cfm)	Location/Comments
Between Living and Sunspc						
Natural	20	20	3	na	na	

- *Vent Type.* Possible types are natural and fan.
- *Inlet Area.* The area of the air inlet in square feet. This is used only when vent type is "natural".
- *Outlet Area.* The area of the air outlet in square feet. This is used only when vent type is "natural".
- *Height Diff.* The elevation difference between the inlet and the outlet in feet. This is used only when vent type is "natural". Default is two feet.
- *Fan Watts.* The fan power rating in watts. This is used only for sunspaces and only then when vent type is "fan". Fan energy may be reported as a separate line item or added to the source energy for heating.
- *Fan Flow (cfm).* The cubic feet per minute of air flow provided when the fan is operating. This is used only for sunspaces and then only when vent type is "fan".
- *Location/Comments.* User provided text describing where the item is located or other relevant information.

**Thermal Mass for High Mass Design.** This listing can only appear if and when the Proposed Design's thermal mass exceeds the required mass threshold. Exceeding this mass threshold and modeling this mass in the Proposed Design is also considered to be an exceptional condition and must be reported in the *Special Features and Modeling Assumptions* listings on the CF-1R and the C-2R. This listing shall provide detail about the thermal mass elements in the building. One row is provided in the table for each mass element.



Thermal mass elements may be located within a single zone, they may separate zones or they may be located on an exterior wall. Mass elements in each of these categories shall be grouped and labeled accordingly.

THERMAL MASS FOR HIGH MASS DESIGN

Mass Name	Area (ft <sup>2</sup> )	Thickness (inches)	Volumetric Heat Capacity (Btu/ft <sup>3</sup> -°F)	Conductivity (Btu-in)/(hr-ft <sup>2</sup> -°F)	Form 3 Reference	Inside Surface R-value (hr-ft <sup>2</sup> -°F)/Btu	Location/Comments
Zone=Living							
ExpSlb-L	273	3.5	28	.98	na	0	Exposed in living
CarSlb-L	419	3.5	28	.98	na	2	Carpeted in living
Zone=Sleep							
ExpSlb-S	273	3.5	28	.98	na	0	Exposed in sleeping
CarSlb-S	419	3.5	28	.98	na	2	Carpeted in sleeping
Zone=SunSpc							
SSSlb	450	3.5	28	.98	na	0	Sunspace slab
Between Sunspc and Living							
SSWall	100	8.0	28	.98	na	0	Masonry wall

- **Mass Name.** The name of the mass element. This name may be referenced from the optional solar gains targeting section of the fenestration surfaces table.
- **Area (ft<sup>2</sup>).** The area of the mass in square feet.
- **Thickness.** The mass thickness in inches.
- **Heat Capacity.** The volumetric heat capacity of the mass material in Btu/F-cf.
- **Conductivity.** The conductivity of the mass material in Btu-in/hr-ft<sup>2</sup>-°F.
- **Form 3 Reference.** A reference to a wall Form 3. This may be used when a mass element is part of an exterior wall to describe an exterior mass wall or the link between a mass material and an opaque wall surface. The mass area should be the same as the sum of the wall surface areas that reference it.
- **Inside Surface R-value.** The thermal resistance of any material (such as carpet or tapestry) that may exist on the inside surface of the thermal mass excluding air films. For instance, if a mass element is carpeted, a surface R-value of 2 is the fixed input. For mass elements that separate thermal zones, the surface R-value may be reported separately for each side of the mass.
- **Location/Comments.** User provided information on the location of the mass element or other relevant information.

**HVAC Systems.** Information is provided on the type of heating and cooling systems proposed for each zone of the building. Data in the table is organized to accommodate any type of heating or cooling system so some of the information is not applicable for all



system types. When the information is not applicable, "na" is reported. Data in this table should be organized first by heating and cooling system. Note that the thermostat type is reported under "Building Zone Information" described above.

For buildings that are modeled as multiple thermal zones, the items shall be grouped for each zone and indicated with a header "Zone = <ZoneName>". The zone name used in the header should be the same as the name used in the table titled "Building Zone Information"

## HVAC SYSTEMS

Equipment Type	Minimum Equipment Efficiency (or Water Heating System Name) <sup>5</sup>	Distribution Type and Location	Duct R-value
<b>Zone=Living</b>			
Furnace	0.78 AFUE	DuctsCrawl	4.2
AirCond-Split	10.0 SEER	DuctsCrawl	4.2
<b>Zone=Sleep</b>			
CombHydro	Upper Floors	Baseboard	na.
AirCond-Split	10.0 SEER	DuctsAttic	4.2

- *Equipment Type.* The type of heating or cooling equipment. This is specified separate from the distribution type. Required heating equipment and cooling equipment entries are listed in Table 2-7. When the proposed house is not air conditioned, the entry should be NoCooling. If more than one type of equipment is specified, they may be listed on subsequent rows.

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<sup>5</sup> "Water Heating System Name" may be omitted from heading, except when combined hydronic systems are used.



Table 2-8 - HVAC Equipment Types

Heating Equipment	
Furnace	Can be gas, oil or propane; central or wall unit. Distribution systems can be gravity, or any of the ducted systems.
Boiler	Can be gas, oil or propane. Distribution systems can be any of the defined systems. "Boiler" is specified for dedicated hydronic systems.
HtPumpSplit	Distribution system must be one of the ducted systems
HtPumpPckg	Distribution system must be one of the ducted systems
Electric	Includes all electric heating systems other than HtPumpSplit or HtPumpPckg, for instance, electric resistance, electric boilers or hot water heat pumps. Distribution systems can be Radiant, Baseboards or any of the ducted systems
CombHydro	Heating system can be storage gas, storage electric or heat pump water heaters. Distribution systems can be fan, radiant or any of the ducted systems.
Cooling Equipment	
No cooling	Entered when the proposed building is not air conditioned
AirCondSplit	Distribution system must be one of the ducted systems
AirCondPackg	Distribution system must be one of the ducted systems
HtPumpSplit	Distribution system must be one of the ducted systems
HtPumpPackg	Distribution system must be one of the ducted systems

- **Minimum Equipment Efficiency.** The minimum equipment efficiency needed for compliance. The applicable efficiency units should also be reported, for instance AFUE for furnaces and boilers, HSPF for electric heating equipment, and SEER for heat pumps (cooling) and central air conditioners. In the case of combined hydronic heating, the name of the water heating system should be identified. If equipment type is Electric, an HSPF of 3.413 should be entered, except for radiant systems which use a maximum HSPF of 3.55.
- **Distribution Type and Location.** The choices for distribution type and location are shown in Table 2-10 with a brief discussion of each. Any duct location other than all ducts in the attic (*DuctsAttic*) must also be reported in the *Special Features and Modeling Assumptions* listings AND the *HERS Required Verification* listings on the CF-1R and C-2R forms printed by the ACM.



Table 2-9 - Heating and Cooling Distribution Types and Locations

Distribution System Type/Location	
DuctsAttic DuctsCrawl DuctsGarage DuctsBasemt DuctsCVC DuctsInEx12 DuctsInAll	The fan powered ducted distribution systems can be used with any of the heating and cooling systems. When ducted systems are used with furnaces or boilers, then the electricity used by the fan shall be calculated using the methods described later in this manual. If a ducted distribution system is indicated, then the R-value must be indicated in the next column.  "DuctsInEx12" is used for ducted distribution systems where all the main air handler and all but 12 lineal feet or less of ducts and plenums are within conditioned space such as an HVAC unit in a garage adjacent to the conditioned space. For the purpose of determining duct and plenum lengths, the "length" of a plenum return box is the cross diagonal of the box. "DuctsInAll" must have both the HVAC unit and any ducts or plenums located totally within conditioned space. "DuctsInAll" is also used for non ducted fan systems, such as a wall furnace with fan.
DuctLess	This distribution system is most typical for a wall furnace with no fan and floor furnaces, although some central systems might also be constructed without ducts (distributed fan coil units).
Radiant	A ductless system that can be used with a boiler, electric or combined hydronic heating equipment (with no fan).
Baseboard	A ductless system that can be used with a boiler, electric or combined hydronic heating equipment (with no fan).

The default distribution type and location is a ducted, central system with 100% of the ducts in the attic. If a duct design is specified with duct locations on the plans but without specific duct surface areas (sizes and lengths) specified, a *Special Features and Modeling Assumptions* entry which specifies the default duct locations that are specified in Section 3.8.3. To use DuctsCrawl or DuctsBsmt, all supply registers must be in the floor and the *Special Features and Modeling Assumptions* listings must indicate that all supply registers are in the floor.

- *Duct R-value.* The installed R-value for duct insulation. The minimum duct insulation is 4.2 which is required by the mandatory measures section.

**Special Systems - Hydronic Distribution Systems and Terminals.** This listing must be completed for hydronic systems that have more than 10 feet of piping (plan view) located in unconditioned space. As many rows as necessary may be used to describe the piping system. Note that hydronic heating systems (combined or not) must be reported in the *Special Features and Modeling Assumptions* listings. The entry for the *Special Features and Modeling Assumptions* listings must indicate any additional listings that are reported for this feature so that the local enforcement agency can verify the additional information needed to check this special feature.



## SPECIAL SYSTEMS - HYDRONIC DISTRIBUTION SYSTEMS AND TERMINALS

Distribution System Name	Terminal Type	Number (#)	Piping Run Length (ft)	Nominal Pipe Size (in)	Insulation Thickness (in)	Insulation R-value
HydFanCoil	FanCoil	1	15	1.5	1.5	6.0
	Baseboard	1	20	.75	1	4.0
	FanCoil	1	15	.5	1.5	4.0

- *System Name (text)*: Description given to the hydronic system.
- *Terminal Type (prescribed descriptor)*: The type of terminal equipment used in the system.

Permissible types: Listed in Table 2-11.

Table 2-10 Hydronic Terminal Descriptors

Descriptor	Hydronic Terminal Reference
<i>FanCoil</i>	Ducted fan coil used in central systems
<i>Baseboard</i>	Baseboard convector using natural convection
<i>RadiantFlr</i>	Radiant floor

- *Piping Run Length (ft)*. The length (plan view) of distribution pipe located in unconditioned space, in feet, between the primary heating/cooling source and the point of distribution.
- *Nominal Pipe Size*. The nominal (as opposed to true) pipe diameter in inches.
- *Insulation Thickness (in)*. The thickness of the insulation in inches. Enter "none" if the pipe is uninsulated.
- *Insulation R-value (hr-ft<sup>2</sup>-°F/Btu)*. The installed R-value of the pipe insulation. Minimum pipe insulation for hydronic systems is R-4 for 2" or smaller pipe, and R-6 for pipe diameter larger than 2".

**Water Heating Systems.** This listing includes information about water heating systems. A water heating system may serve more than one dwelling unit. A system may also have more than one water heater, but may have only one distribution system. Each water heating system in the building is defined in one or more rows in the following table. Data in this table is associated with data in the Water Heating System Credits Table, the Water Heater Equipment Detail Table, and the Water Heating System Assignments Table. When there are multiple water heater types in a system, the last six columns may be repeated as necessary.



## WATER HEATING SYSTEMS

System Name	Distribution Type	Water Heater Name	Water Heater Type	Number in System	Energy Factor	Tank Size (gal)
Upper Floors	Recirc/Timer	State100	SG	3	.52	100
		State67	SG	3	.55	67
Lower Floors	Recirc/Timer	State50	SG	4	.62	50
Kitchens	POU	Loch006	IE	18	.98	na.

- **System Name.** This is a user defined name for the water heating system that provides a link between the water heating systems table, the Water Heating Systems Credits Table, and the Water Heater System Assignments Table.
- **Distribution Type.** Several specific distribution systems are recognized. The distribution system will be one of the following choices. Qualifying requirements for these distribution systems are included in Section 6.6 of the *Residential Manual*.

Table 2-11 - Water Heating Distribution Types

Standard	RecrcDmd (recirculation with demand control)
PtOfUse (point of use),	RecrcTmp (recirculation with temperature control)
HtWtrRcv (hot water recovery),	R/D&HWR (recirc/demand & hot water recovery)
PipeInsl (pipe insulation)	R/D&PIs (recirc/demand & pipe insulation)
RecrcNC (recirculation with no controls)	RecrcT&T (recirc with timer and temp controls)
RecrcTim (recirculation with timer control)	PrllPipe (parallel piping)

- **Water Heater Name.** This is a user defined name that provides a link between the Water Heater System Table and the Water Heater Equipment Detail Table.
- **Water Heater Type.** The water heater type will be one of the following choices. The large storage gas water heaters are larger than the 75,000 Btu/h maximum input rated by the National Appliance Energy Conservation Act (NAECA). Indirect gas water heaters are essentially a boiler with a separate storage tank. Additional data required for large storage gas and indirect gas types is entered later in the Water Heater Equipment Detail table. "Gas" is used for propane as well as natural gas. If oil water heaters are used, the "gas" choices may be selected.

Table 2-12 - Water Heater Types

SG (storage gas)	IG (instantaneous gas)
SO(storage oil)	IE (instantaneous electric)
SE (storage electric)	LgG (large storage gas)
HP (heat pump water heater)	IndG (indirect gas)

- **Number in System.** The number of identical water heaters that exist in the system.



- **Energy Factor.** The energy factor is the principal performance factor for water heater types subject to NAECA regulations, including storage gas, storage electric, instantaneous electric and heat pump water heaters. If the energy factor is not published, this means that the water heater is not covered by NAECA and the Water Heater Equipment Detail Table must be completed.
- **Tank Size (gal).** The storage tank capacity in gallons. This input is applicable to all storage type water heaters.
- Note: External Insulation Wrap is no longer allowed as a modeling option for approved ACMs.

**Special Water Heating System Credits.** This section includes information about water heating auxiliary energy credits, if used. These features are optional capabilities for ACMs and their use for performance compliance requires listing in the *Special Features and Modeling Assumptions* listings of the CF-1R and the C-2R. The *Special Features and Modeling Assumptions* listing must cross-reference the listing below which must be included as part of the C-2R when any of these applicable optional water heating capabilities are modeled by the ACM.

SPECIAL WATER HEATING SYSTEM CREDITS

System Name	Solar Savings Fraction	Pump Energy (Y/N)	Wood Stove Boiler? (Y/N)	Wood Stove Boiler Pump? (Y/N)
Upper Floors	.60	Y	na.	na.

- **System Name.** This is a name corresponding to a system name defined in the water heating systems table.
- **Solar Savings Fraction.** If the water heating system has a solar system to provide auxiliary heating, the solar savings fraction is entered in this column. The solar savings fraction may be determined using f-Chart or other methods approved by the CEC. A system may have solar auxiliary or a wood stove boiler, but not both.
- **Pump Energy (Y/N).** This is a yes/no response to indicate whether or not pump energy should be considered in the ACM calculation. "No" should be entered if the solar system does not have a recirculation pump or if the energy of the pump was already included in the supporting f-Chart analysis. "Yes" is entered only if the system has a pump and it was not considered in the f-Chart analysis. Active solar systems generally have a pump, while thermosyphon and integral collector storage (ICS) systems generally do not.
- **Wood Stove Boiler (Y/N).** This is a yes/no response on whether or not the system has a wood stove boiler. A credit may be taken for either solar systems or for a wood stove boiler, but not both.
- **Wood Stove Boiler Pump (Y/N).** This is a yes/no response to indicate whether the wood stove boiler has a recirculation pump.



**Special Water Heater/Boiler Details.** This listing describes the equipment that serves the water heating system or systems. It is only necessary to complete this table for combined hydronic systems and for non-NAECA water heaters. The information in the table will not be applicable to every water heater type. The use of these features for performance compliance requires listing in the *Special Features and Modeling Assumptions* listings of the CF-1R and the C-2R. The *Special Features and Modeling Assumptions* listing must cross-reference the listing below which must be included as part of the C-2R when any of these Special Water Heating Equipment characteristics are modeled by the ACM. When the information is not applicable, "na" may be reported.

SPECIAL WATER HEATER /BOILER DETAILS

Water Heater Name	Recovery Efficiency (fraction)	AFUE (fraction)	Rated Input (kBtu/h)	Combined Hydronic Pump (watts)	Standby Loss (fraction)	Tank Total R-value (hr-ft <sup>2</sup> -°F/Btu)	Pilot Light (Btu/h)
Loch006	na.	0.78	na.		na.	na.	na.
State100 Hydro	na.	0.79	40	40	na.	na.	na.
State50	na.	0.80	na.		na.	na.	na.

- *Water Heater Name.* This is a user defined name that provides a link to the water heater system table. In the case of a hydronic system heater, the name should be descriptive of this function to distinguish it from any domestic water system heaters.
- *Recovery Efficiency (fraction).* Recovery efficiency is the performance measure for instantaneous gas water heaters, large storage gas water heaters and indirect gas water heaters. It is also needed for storage gas water heaters used in combined hydronic systems. The value is taken from the CEC Appliance Database<sup>6</sup> or from manufacturers literature. If the value is omitted for NAECA regulated water heaters, then the default value will be assumed.
- *AFUE (fraction).* The Annual Fuel Utilization Efficiency, the heating efficiency of the water heater based upon approved test methodologies. Values of AFUE are listed in the Commission Appliance Database.
- *Rated Input (kBtu/h).* The energy input, in kBtu/h (thousands of Btus per hour), from the CEC Appliance Database or from manufacturers literature. This is needed for large storage gas and indirect gas water heaters and when storage gas water heaters or heat pump water heaters are used for combined hydronic space heating.
- *Combined Hydronic Pump (watts).* This is needed only for electric combined hydronic systems. It is not needed for storage gas or heat pump combined hydronic systems.

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<sup>6</sup> See Footnote 3, Page 2-22.



- *Standby Loss (fraction).* The standby loss percent per hour (taken from the CEC Appliance Database or from manufacturers literature) divided by 100. Applicable to large storage gas water heaters only.
- *Tank Total R-value ( $hr \cdot ft^2 \cdot ^\circ F / Btu$ ).* The total thermal resistance for both the tank and the insulation. This input is applicable to large storage gas and indirect gas water heaters only.
- *Pilot Light (Btu/h).* The pilot light energy, in Btu/h, from the CEC Appliance Database or from manufacturers literature. This column is only applicable for instantaneous gas water heaters and indirect gas water heaters.

Table 2-14 summarizes the applicability of the inputs for the water heater types recognized by the calculation method.

**Table 2-13 - Water Heater Input Summary**

Input Item	NAECA Storage Gas	NAECA Storage Electric	NAEC A Heat Pump	Instant . Gas	Instant. Electric	Large Storage Gas	Indirect Gas
Energy Factor	Yes	Yes	Yes	Yes	Yes		
Pilot Input, Btu				Yes		Yes	Yes
Efficiency, % <sup>7</sup>						Yes	Yes
Standby Loss, %						Yes	
Tank Volume, gal.	Yes	Yes	Yes			Yes	Yes
Tank Insulation, R						Yes	Yes
Ext. Insulation, R						Yes	Yes
If Combined Hydronic System:							
Rated Input, kBtuh	Yes					Yes	Yes
Rated Input, kWl		Yes	Yes				
Recovery Eff, %	Yes		Yes			Yes	Yes
Pump Input, Watts		Yes				Yes	Yes

**Special Water Heating System Assignments.** In multi-unit buildings or buildings with more than one water heating system, it is necessary to assign water heating systems to the dwelling units that they serve. This is necessary in order for the recovery load to be properly calculated for each system. When an ACM models a water heating system that does not have a single separate water heater serving each dwelling unit, it must be reported in the *Special Features and Modeling Assumptions* listings of the CF-1R and the C-2R. The *Special Features and Modeling Assumptions* listing must cross-reference the listing below which must be included as part of the C-2R whenever multiple water heaters serve

<sup>7</sup> May be recovery efficiency, thermal efficiency, or AFUE.



one or more dwelling units or when a single water heater serves more than one dwelling unit and is modeled by the ACM for compliance.

In the example below, the building has three water heating systems labeled "upper-floors", "lower-floors" and "kitchens". The "upper-floors" and "lower-floors" systems are both central gas water heaters with recirculating distribution systems. The kitchens in each dwelling unit have their own point of use instantaneous electric water heaters (all of which may be grouped together as one system).

SPECIAL WATER HEATING SYSTEM ASSIGNMENTS (Example Listing)

Number of Units	CFA per Unit	Name(s) of System(s)
8	1000	Upper Floors Kitchens
10	800	Lower Floors Kitchens

SPECIAL WATER HEATING SYSTEM ASSIGNMENTS (Example Listing)

Number of Units	CFA per Unit	Name(s) of System(s)
1	1800	Main

- *Number of Units.* The number of dwelling units served by this system assignment.
- *CFA per Unit.* The average conditioned floor area per dwelling unit in this system assignment.
- *Name(s) of Systems(s).* The water heating system names associated with this assignment. Names must correspond to system names defined in the Water Heating Systems table.

**Special Features and Modeling Assumptions.** This listing must **stand out and command the attention** of anyone reviewing this form to emphasize the importance of verifying these Special Features and the aspects of these features that were modeled to achieve compliance or the energy use results reported. This is a free format section for the C-2R report to note any special features about the building that are needed to verify compliance.

SPECIAL FEATURES AND MODELING ASSUMPTIONS: (Example Listing)

This house has zonal control and multiple zones,
This house uses a non-NAECA large storage gas water heater . Check the C-2R SPECIAL WATER HEATER/BOILER DETAILS listing for specifications.
This house has an attached sunspace with interzone surfaces, interzone ventilation, and custom solar heat distribution.



**HERS Required Verification.** Specific features that require diagnostic testing to assure proper installation require field testing and verification by a certified home energy rater under the supervision of a Commission-approved HERS provider, and must be listed in this section. This listing must **stand out and command the attention** of anyone reviewing this form to emphasize the importance of HERS verification of these features and the aspects of these features that were modeled to achieve compliance. or the energy use results reported.

HERS REQUIRED VERIFICATIONS (Example Listing)

This house is using an HVAC system with all ducts and the air handler located within the conditioned space. This results in a higher distribution efficiency rating and must be visually confirmed by a certified HERS rater under the supervision of a CEC-approved HERS provider. This verification must be reported on a CF-6R form.

This 1600 square foot house has tight construction with reduced infiltration and a target blower door test range of 586 to 1250 CFM at 50 pascals. The blower door test must be performed using the *ASTM Standard Test Method for Determining Air Leakage Rate by Fan Pressurization*, ASTM E 779-87 (Reapproved 1992).

WARNING: If this house tests below 586 CFM at 50 pascals, the house must either be provided with a ventilation opening that will increase the tested infiltration to at least 586 CFM at 50 pascals (SLA = 1.5) OR mechanical supply ventilation must be provided that can maintain the house at a pressure of at least -5 pascals relative the outside average air pressure while other continuous ventilation fans are operating.

WARNING - Houses modeled with reduced infiltration and/or mechanical unbalanced exhaust ventilation are prohibited from having vented combustion appliances that use indoor air for combustion inside conditioned space.







<b>2. STANDARD REPORTS</b>	<b>1</b>
2.1 Certificate of Compliance (CF-1R)	2
2.2 Computer Method Summary (C-2R)	25



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### 3. Defining the Proposed and Standard Designs

The space conditioning energy budget for the low-rise residential Standards is a custom budget, that is, the energy that would be used by a building similar to the *Proposed Design*, but that is modified to just meet the requirements of the prescriptive standards. The building that is modeled to create the custom budget is the *Standard Design*. This section of the *ACM Approval Manual* describes how the *Proposed and Standard Designs* are defined.

The *Proposed Design* is modeled based upon user inputs that are subject to a variety of restrictions as well as a variety of fixed and restricted assumptions regarding dwelling design and operation. The user enters information to describe the thermal characteristics of the building envelope including its surface areas, air leakage, shading structures and attachments, thermal mass elements, heating and cooling equipment and distribution systems, and water heating equipment and distribution systems.

The process of generating the *Standard Design* and calculating the custom budget must be performed automatically by the program based on the allowed and default inputs for the *Proposed Design* as well as the fixed and restricted inputs and assumptions for both designs. These operations shall not be accessible to program users for modification when the program is used for compliance purposes or when compliance forms can be generated by the program. The *Standard Design* generator must automatically take user input about the *Proposed Design* and create input data for the *Standard Design*, using all the applicable fixed and restricted inputs and assumptions. All assumptions and algorithms used to model the *Proposed Design* must also be used in a consistent manner in the *Standard Design* building.

Defining the *Standard Design* building involves two steps. First, the geometry of the proposed building is modified from the description entered for the proposed design. Second, building features are modified to meet the minimum requirements of compliance with package D of the Standards.

The following sections present the details on how the *Standard Design* is to be developed.

---

#### 3.1 Basis of the Standard Design - Package D

The basis of the *Standard Design* is package D. The requirements of package D are contained in Section 151(f) of Title 24, Part 6 of the State Building Standards. These prescriptive requirements are not repeated here.

---

#### 3.2 Building Physical Configuration

**Proposed Design:** The building configuration is defined by the user entries for heavy and light floor areas, wall areas, roof and ceiling areas, fenestration areas, and door areas which are entered along with the orientation of these building elements. The user entries for all of these building elements must be consistent with the actual building design and configuration. If the ACM actually models the specific geometry of the



building by using a coordinate system or graphic entry technique, the building geometry must be as consistent as reasonably possible with the actual building design to achieve thermal modeling accuracy.

**Standard Design:** The *Standard Design* building has the same floor area, volume, and configuration as the *Proposed Design*, except that wall and window area are distributed equally between the four main compass points, North, East, South, and West. The details are described below.

---

### 3.2.1 Conditioned Floor Area

**Proposed Design:** The ACM must require the user to enter the total conditioned floor area of the *Proposed Design* as well as the conditioned slab floor area. The conditioned slab floor area is the area of a slab floor with a minimum slab thickness of 3.5 inches or a minimum heat capacity of 7.0 Btu/ft<sup>2</sup>-°F and conditioned space above and unconditioned space or the ground/gravel below. The non-slab conditioned floor area is the total conditioned floor area minus the conditioned slab floor area.

**Standard Design:** The total conditioned floor area and the conditioned slab floor area of the *Standard Design* building is the same as the *Proposed Design*.

**Proposed Design & Standard Design:** ACMs must keep track of the conditioned floor area and must at least be able to keep separate track of the total conditioned floor area and conditioned slab floor area. These areas are used to determine the default thermal mass for the *Proposed Design* and the thermal mass for the *Standard Design*. Stairwell floor area is the horizontal area of the stairs and landings between two floors of each story of the house. The conditioned slab floor area may be either on-grade or a raised slab.

---

### 3.2.2 Volume

**Proposed Design:** The volume of the *Proposed Design* is the conditioned volume of air enclosed by the building envelope. The volume must be consistent with the air volume of the actual design and may be determined from the total conditioned floor area and the average height or from a direct user entry for volume.

**Standard Design:** The volume of the *Standard Design* building is the same as the *Proposed Design*.

---

### 3.2.3 Ceilings

**Proposed Design:** The ACM shall allow a user to enter one or more ceiling/roof areas for the *Proposed Design* from an approved list of roof/ceiling construction types. Some of these construction types may be user-defined but the ACM must determine the output names for user-defined construction types for all building envelope constructions. The ACM shall not allow the user to specify output names for construction types or envelope elements. The roof/ceiling areas, construction assemblies, and tilts modeled must be consistent with the corresponding areas, construction assemblies, and tilts in the actual building design and must total the



overall roof/ceiling area with conditioned space on the inside and unconditioned space on the other side. Except as indicated in the next sentence, the U-value of the modeled assembly must be the same as the U-value of the actual assembly.. Ceiling construction assemblies that do not meet the mandatory minimum U-value required by Title 24 shall not be allowed.

**Standard Design:** The ceiling/roof areas of the *Standard Design* building are equal to the ceiling/roof areas of the *Proposed Design*. The *Standard Design* roof and ceiling surfaces are assumed to be horizontal (no tilts) and have a U-value specific to the package D requirements. The *Standard Design* generator must consider all exterior surfaces in the *Proposed Design* with a tilt less than 60 degrees as roof elements. Surfaces that tilt 60 degrees or more are treated as walls.

### 3.2.4 Walls

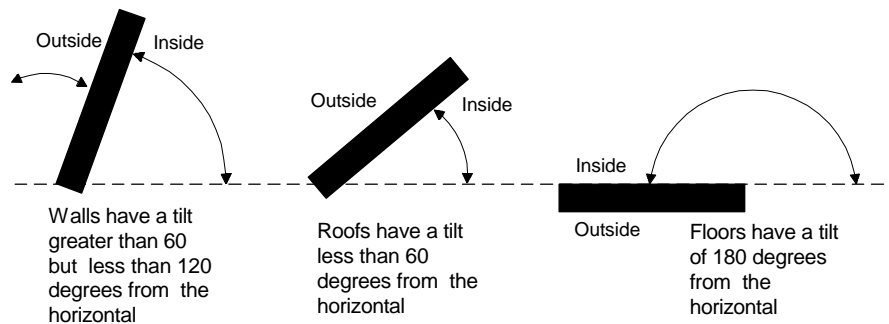


Figure 3-1 Surface Definitions

**Proposed Design:** The ACM shall allow a user to enter one or more wall areas for the *Proposed Design* from an approved list of wall construction types. Some of these construction types may be user-defined but the ACM must determine the name for user-defined construction types for all building envelope constructions. The ACM shall not allow the user to specify names for construction types or envelope elements. The wall areas modeled must be consistent with the corresponding wall areas in the actual building design and the total wall area must be equal to the gross wall area with conditioned space on the inside and unconditioned space or exterior conditions on the other side.

**Standard Design:** The gross wall area in the *Standard Design* run is equal to the gross wall area of the *Proposed Design*, including knee walls in the ceiling construction of the *Proposed Design*. The gross wall area in the *Standard Design* is equally divided between the four main compass points, North, East, South, and West. Window and door areas are subtracted from the gross wall area to determine the net wall area in each orientation. All surfaces included in the *Proposed Design* run input file with a tilt from the horizontal of 60 degrees or more and less than 120 degrees are treated as walls. Surfaces that have a tilt less than 60 degrees are considered to be roof surfaces.



---

### 3.2.5 Basement Walls and Floors

**Proposed Design:** Portions of basement walls above grade must be modeled as conventional walls above grade. The user must be requested to enter the area of basement walls below grade as the area of below grade wall at each of 3 depths for Zero to 2 feet below grade (shallow), from 2 feet to 6 feet below grade (medium), and greater than 6 feet below grade (deep). The ACM shall allow users to enter as many wall types as necessary to model the proposed construction. The ACM must use the same method for determining the U-value and mass characteristics for below grade walls as used for above grade walls. The default value for the proposed design wall construction shall be the same as the *Standard Design*.

**Standard Design:** The *Standard Design* shall have the same basement wall areas as the *Proposed Design*. The *Standard Design* basement wall shall be assumed to be a wall with a Heat Capacity of 15.7 Btu/(ft<sup>2</sup>-°F), a thickness of 8 inches, and an uniform R-value of 1.5.

---

### 3.2.6 Floors

**Proposed Design:** In addition to the total conditioned floor area and total conditioned slab floor area, ACMs must allow the user to enter floor areas for the standard raised floor construction types listed in Table 3-1 and at least three user-defined construction types. The ACM must require user input to be able to distinguish floor areas and constructions that are over crawl spaces. The ACM and its documentation must inform the user that the floor constructions and areas must be consistent with the actual building design.

The effect of a conventional crawl space is approximated with a thermal resistance of R-6; however, for controlled ventilation crawl spaces (an optional capability), the crawl space is modeled as a separate thermal zone and R-6 is not assumed. The R-6 value for a conventional crawlspace shall be automatically calculated by the ACM and shall not be allowed as a user input.

**Standard Design:** The exposed raised floor U-value used in the *Standard Design* is independent of the proposed construction assembly. It does vary, however, depending on whether or not the floor assembly is located over a crawl space. The ACM must keep track of which raised floor surfaces are over crawl spaces and which are not.

**Proposed Design & Standard Design:** The effect of a crawl space is approximated with a thermal resistance of R-6 and this is accounted for in the *Standard Design* U-value in Table 3-1. Raised floors in the *Proposed Design* that are not located over a crawl space shall not include the R-6 thermal resistance used for floors over a crawl space.

---

### 3.2.7 Slab-on-Grade Perimeter

**Proposed Design:** The ACM must allow users to enter at least two different slab perimeter constructions and their corresponding lengths. ACMs must assume that 80% of any slab edge length entered is adjacent to rug-covered (R-2 for carpet and pad) slab and 20% is adjacent to exposed slab on the conditioned side and determine



an overall F2 factor for the total length or specify that the user enter or choose such a weighted F2 factor. The ACM must be able to determine the amount of slab edge adjacent to unconditioned spaces separately from the slab edge adjacent to the outside so that the ACM can determine the appropriate *Standard Design*. In the *Proposed Design*, the F2 factor(s) may account for slab perimeter insulation for both slab edges exposed to the outside and slab edges adjacent to unconditioned spaces such as garages. Slab edges adjacent to garages and unconditioned spaces may be considered to be insulated with R-7 insulation and have an F2 factor of 0.51.

**Standard Design:** The total slab perimeter length in the *Standard Design* is the same as in the *Proposed Design*. For the *Standard Design*, the slab edge heat loss factor, F2, is 0.76 for all climate zones except Climate Zone 16 where F2 is 0.51. For the *Standard Design* unconditioned spaces such as the garage are assumed to be detached, hence the slab perimeter between conditioned spaces and unconditioned spaces such as garages is assumed to meet the Alternative Component Package D requirements in Section 151 of the building efficiency standards and is assumed to be exposed to the outside conditions. See Section 4.7.1 for details.

---

### 3.2.8 Doors

**Proposed Design:** ACMs must allow users to enter at least two different door construction types, their areas, and orientations. These door types must include the standard door type specified in Table 3-1 plus at least one user-defined door type with an ACM specified name or designator. For the user-defined door type, the ACM must at least allow the user to enter the area, the orientation, and the U-value or R-value of the door.

**Standard Design:** The *Standard Design* has 40 square feet of door area for each dwelling unit. All doors are assumed to face north. This means that the net opaque wall area facing north is reduced 40 ft<sup>2</sup> for each dwelling unit for the *Standard Design* run.

---

### 3.2.9 Fenestration Types and Areas

**Proposed Design:** ACMs must allow users to select fenestration or window types from the default tables in the standards or from several user-defined fenestration types where the user must enter the *Number of Fenestration Assemblies*, the *U-value* and *Solar Heat Gain Coefficient (SHGC)* for any user-defined window type. For each user-defined fenestration type the ACM must require the user to enter the Fenestration Area, tilt and orientation.

**Standard Design:** Fenestration area in the *Standard Design* is determined by the package D specification for the appropriate climate zone. If package D for the climate zone permits 20% of the conditioned floor area in glass, then the *Standard Design* has a fenestration area equal to 5% of the conditioned floor area facing in the direction of each major compass point. If package D for the climate zone permits 16% of the conditioned floor area in glass, then the *Standard Design* has a fenestration area equal to 4% of the conditioned floor area facing in the direction of each major compass



point. There is no skylight area in the *Standard Design* run. The net wall area on each orientation is reduced by the fenestration area (and door area) on each facade.

---

### 3.2.10 Overhangs

**Proposed Design:** ACMs must allow users to enter a set of basic generic parameters for a description of an overhang for each individual fenestration or window area entry. The basic parameters must include *Fenestration Height*, *Fenestration Width*, *Overhang Length*, and *Overhang Height*. ACM user entries for overhangs may also include *Overhang Left Extension* and *Overhang Right Extension*.

**Standard Design:** The *Standard Design* does not have overhangs.

---

## 3.3 Envelope Heat Loss Factors

Heat loss factors include U-values for ceilings/roofs, walls, floors, windows and doors. For the slab edges of slabs-on-grade the heat loss factor is expressed as an F2 factor

**Proposed Design:** Except for user-defined walls, ACMs must automatically assign heat loss factors based on the user's selection of one of the standard building elements from the approved lists of standard building elements.

ACM vendors should note that user entered U-values are developed with an outside air film resistance of 0.17 based on a 15 mph wind speed. The vendors may internally adjust the U-value in the simulation for average wind conditions (3 mph wind) by assuming an outside air film resistance of 0.38 or they may strip off the fixed outside air film R-value of 0.17 and calculate an hourly R-value for the outside air film coefficient based on the wind speed and surface roughness.

**Standard Design:** Heat loss factors in the *Standard Design* are determined by the Package D specification. They are independent of the construction assembly in the proposed building. The heat loss factors used in the *Standard Design* are given in the table below. The *Standard Design* U-values for roof/ceilings and walls depends only on the package specification and is independent of the actual construction assembly proposed. The standard design U-values include an external air film with an R-value of 0.17 based on a 15 mile per hour wind speed. The adjustment to this air film for the standard design shall be the same as that used for the proposed design.

For slab edges, the heat loss factor (F2 factor) is one of two fixed values in the *Standard Design* run. For climate zones with no slab edge insulation requirement and slab edges adjacent to unconditioned spaces F2 is 0.76 and for slab edges required to be insulated it is 0.51. For the climate zone package(s) that require slab edge insulation (Climate Zone 16), the slab edge for the *Standard Design* has insulation on the total perimeter length and has an F2 factor of 0.51.

The door U-value is fixed at 0.330 Btu/(hr-ft<sup>2</sup>-°F) in the *Standard Design* run.



Table 3-1 - Basecase Heat Loss Factors

Building Component	Package Specification or Mandatory Minimum	U-value
Roof	R-19	0.051
	R-30	0.034
	R-38	0.028
Wall	R-13	0.088
	R-19	0.065
	R-21	0.059
Raised Concrete Floor	R-0	
	R-4	
	R-8	
Raised Floor (crawl space)	R-19	0.037
(no crawl space)	R-19	0.049
Fenestration	U = 0.75	0.75
	U = 0.65	0.65
	U = 0.60	0.60
Doors	na.	0.330
Slab Edge		<b>F2 Factor<sup>1</sup></b>
	None	0.76
	R-7	0.51

<sup>1</sup> The F2 Factor is determined based on the required assumption that 80% of the slab edge is adjacent to rug-covered slab and 20% is adjacent to exposed slab.

### 3.4 Solar Heat Gain Coefficients

**Proposed Design:** ACMs must require the user to enter the fenestration Solar Heat Gain Coefficient for each window, skylight, or other fenestration system type with a separate area. This requirement may be met by having the user select from a standard list of fenestration systems and sizes or by direct entry for user-defined windows or skylights. In addition, for each window, skylight and fenestration element the ACM must require the user to select an interior and exterior shading treatment from the lists given in the tables below. The ACM will then determine the overall SHGC for the complete fenestration system based on the fenestration SHGC and the SHGCs assigned to the Commission-approved interior and exterior shading devices.

**Standard Design:** The *Standard Design* fenestration Solar Heat Gain Coefficients (SHGCs) are determined by the appropriate Package D specifications for the applicable climate zone. Note that the frame type and the presence or absence of muntins or dividers is now irrelevant for the *Standard Design* since the Package D



values for  $SHGC_{fen}$  and the U-value include the effects of fenestration features such as framing, dividers, and muntins.

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### 3.5 *Shading Devices and their Solar Heat Gain Coefficients*

Internally, ACMs shall use two values to calculate solar heat gain through windows:  $SHGC_{open}$  and  $SHGC_{closed}$ .  $SHGC_{open}$  is the total solar heat gain coefficient of the fenestration and its exterior shading device when the operable interior shading device is open.  $SHGC_{closed}$  is the total solar heat gain coefficient when the interior shading device is closed.  $SHGC_{open}$  is the setting that applies when the air conditioner is not operating, which typically is most of the 24-hour period, while  $SHGC_{closed}$  applies only for periods when the air conditioner operates. The *Standard Design* values for these SHGCs are shown in Table 3-4 below.  $SHGC_{open}$  and  $SHGC_{closed}$  are not user specified inputs.

The ACM must require the user to directly or indirectly specify  $SHGC_{fen}$  and frame type. The ACM must require the user to specify interior and exterior shading devices as the types listed in Tables 3-2 and 3-3. The ACMs must calculate the overall SHGC for the fenestration with shading devices as shown in Chapter 4.

For both the *Proposed Design* and the *Standard Design*, all windows are assumed to have some type of interior shading (draperies) even if *NoRqmt* is specified for compliance purposes and none are present at final inspection. The ACM Compliance Supplement and the ACM output must indicate that interior shading devices or attachments other than *Drapes* that receive credit for solar heat gain reduction must be present at final inspection. The ACM Compliance Supplement must also explicitly indicate that the ACM automatically gives credit for draperies for all windows that do not use higher performance interior shading devices and that credit is allowed only for one interior shading device and one exterior shading device. The default interior shading is a drapery which is given a fixed Solar Heat Gain Coefficient specified in the standards regardless of the type of drapery that might be installed. That is, no additional credit may be taken due to the color or weave density of draperies.

***Proposed Design:*** The ACM must require the user to either accept the default shading devices or select from specific Commission-approved lists of interior and exterior shading devices for each fenestration element. The default choice for interior shading device is *Standard* which uses the drapery SHGC of 0.68 specified in the Standards. The default choice for exterior shading device is *Standard*, which is assigned an average SHGC of 0.76

***Standard Design:*** The ACM uses the default values for interior and exterior shading devices for the *Standard Design*.



Table 3-2 Allowed Interior Shading Devices and Recommended Descriptors

Recommended Descriptor	Interior Shading Attachment Reference	Solar Heat Gain Coefficient before 1/1/200	Solar Heat Gain Coefficient after 1/1/2002
		12	
<i>Standard</i>	Draperies or No Special Interior Shading - Default Interior Shade	0.68	0.68 <sup>1</sup>
<i>Blind</i>	Venetian Blind, Vertical Blind or MiniBlind	0.47	0.47
<i>OpRollShd</i>	Opaque Roller Shades	0.47	0.68
<i>None</i> <sup>2</sup>	No Interior Shading - Only for Skylights (Fenestration tilt <60 degrees)	1.00	1.00

Note (general): No other interior shading devices or attachments are allowed credit for compliance with the building efficiency standards.

Note 1: Default drapery shading shall be assumed whenever no other interior shading is specified for a window. Output shall note that although *Standard* is specified, a drapery is modeled but is not required to be installed and present at final inspection. Output shall note for any interior shading device other than drapery that it must be installed and present at final inspection

Note 2: *None* is the default for fenestration tilted less than 60 degrees from horizontal (skylights) and is only allowed for fenestration tilted less than 60 degrees from horizontal (skylights), i.e. *None* is not an interior shading option for ordinary vertical windows.

Table 3-3 Allowed Exterior Shading Devices and Recommended Descriptors

Recommended Descriptor	Exterior Shading Device Reference	Solar Heat Gain Coefficient
<i>Standard</i>	Bu Screen or No Shading - Default Bugscreens are modeled	0.76
<i>WvnScrn</i>	Woven SunScreen (SC<0.35)	0.30
<i>LvrScrn</i>	Louvered Sunscreen	0.27
<i>LSASnScrn</i>	LSA Sunscreen	0.13
<i>RIDownAwng</i>	Roll-down Awning	0.13
<i>RIDownBlnds</i>	Roll -down Blinds or Slats	0.13
<i>None</i> <sup>1</sup>	For skylights only - No exterior shading	1.00

Note 1: *None* is the default for fenestration tilted less than 60 degrees from horizontal (skylights) and is only allowed for fenestration tilted less than 60 degrees from horizontal (skylights), i.e. *None* is not an exterior shading option for ordinary vertical windows.



Table 3-4- Standard Design Shading Conditions

Characteristic	Package Specification	
	SHGC <sub>fen</sub> = NR	SHGC <sub>fen</sub> = 0.40
SHGC <sub>fen</sub>	0.70	0.40
SHGC <sub>open</sub>	0.68	0.39
SHGC <sub>closed</sub>	0.63	0.37
Glazing	Double Clear	Double Clear
SHGC <sub>fen+int</sub>	0.647	0.378
Interior Shade	Drapes (Standard)	Drapes (Standard)
SHGC <sub>int</sub>	0.68	0.68
Exterior Shade	Bugscreen (Standard)	BugScreen (Standard)
SHGC <sub>ext</sub>	0.76	0.76

### 3.6 Thermal Mass

The performance approach is based on prescriptive Package D of the efficiency standards which has no thermal mass requirements. Package D and the performance approach assume that both the *Proposed Design* and *Standard Design* building have a minimum mass as a function of the conditioned area of slab floor and nonslab floor.

**Proposed Design:** The ACM may require the user to identify whether or not the *Proposed Design* is a high mass building that exceeds the specified mass threshold. Unless the *Proposed Design* has thermal mass that exceeds a thermal mass minimum threshold, the ACM shall model thermal mass for the *Proposed Design* the same as the *Standard Design*.

**Standard Design:** The ACM shall model the *Standard Design* as 20 percent of the *Proposed Design*'s conditioned slab floor area as exposed slab, 80% of the conditioned slab floor area as rug-covered slab, and 5% of the *Proposed Design*'s nonslab floor area as exposed 2 inch thick concrete. No other mass elements are modeled in the *Standard Design*.

The conditioned slab floor area (slab area) shall be modeled as 20 percent exposed thermal mass having a thickness of 3.5 inches, a volumetric heat capacity of 28 Btu/ft<sup>3</sup>-°F, a conductivity of 0.98 Btu-in/hr-ft<sup>2</sup>-°F, and a surface conductance of 1.3 Btu/hr-ft<sup>2</sup>-°F (no thermal resistance on the surface). The remaining 80% of the conditioned slab floor area shall be modeled as covered thermal mass with the same



characteristics as the exposed mass, but with the addition of a surface R-value of 2.0 Btu/hr-ft<sup>2</sup>-°F typical of a carpet and pad.

Conditioned nonslab floor area shall be modeled with 5% of the nonslab floor area as exposed thermal mass. This thermal mass is modeled in both the *Proposed Design* and *Standard Design* with a thickness of 2.0 inches, a volumetric heat capacity of 28 Btu/ft<sup>3</sup>-°F, a conductivity of 0.98 Btu-in/hr-ft<sup>2</sup>-°F, a surface conductance of 1.3 Btu/hr-ft<sup>2</sup>-°F (no added thermal resistance on the surface).

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### 3.7 High Mass Threshold

**Proposed Design:** The ACM may only allow the user to model additional thermal mass when the equivalent thermal mass for the *Proposed Design* reaches a specific mass threshold. The ACM may require that a user indicate a high mass design before the user is allowed to enter additional mass elements and mass characteristics other than what is assumed for the *Standard Design*. The high mass threshold is determined by an amount of mass equivalent to 30% of the conditioned slab floor area as exposed slab, 70% of the conditioned slab floor area as rug-covered slab and 15% of the conditioned nonslab floor area as 2 inch thick exposed concrete with the same specifications as those given in the **Thermal Mass** section above. To determine the threshold, this mass is converted to a standard Interior Mass Capacity using the Unit Interior Mass Capacity (UIMC) method described in Appendix I.

The thermal mass of the *Proposed Design*, other than the mass modeled for the *Standard Design* is only modeled and displayed on compliance output if the design has more equivalent thermal mass than the high mass threshold. The ACM may require that the user specify that the design is a high mass design before the entry of mass elements not related to the slab floor and nonslab floor defaults. For example, a *Proposed Design* with all of the conditioned floor area as slab-on-grade construction designed with 25% exposed slab is still modeled with 20% exposed slab because the designed thermal mass does not exceed the threshold. If the same house is designed with 30% of the conditioned floor area as exposed slab and 70% rug-covered slab then the permit applicant may model that amount of thermal mass in the *Proposed Design*. In addition, a *Proposed Design* may model and take credit for other forms of thermal mass such as masonry fireplaces or extra-thick sheetrock using the UIMC method to determine if the threshold mass is reached. Additional mass elements are not modeled in the *Standard Design*.

**Standard Design:** The *Standard Design* thermal mass is the same as described in Section 3.6.

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### 3.8 Heating and Cooling System

**Proposed Design:** ACMs must require the user to enter simple heating and cooling seasonal efficiencies that are used to characterize basic package single zone HVAC



systems used to heat and/or cool the modeled building. ACMs must be able to distinguish what fuel is being used to heat the building and what fuel is used to cool the dwelling. This may be based on direct user input or indirectly determined from the user's selection of HVAC equipment types. ACMs must require the user to enter the type of distribution system that is used in the proposed design.

**Standard Design:** The standard heating and cooling system for central HVAC systems is a single zone system with ducts in the attic. The standard heating and cooling system for non-central HVAC systems is an unducted system.

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### 3.8.1 Heating Equipment

**Proposed Design:** ACMs must be able to model the basic types of heating equipment listed in Table 2-3 except for combined hydronic space and water heating systems which is an optional modeling capability. ACMs must require the user to enter the basic information to model the energy use of these pieces of equipment. At the minimum this includes some type of seasonal efficiency for heating and whether or not the HVAC system has ducts. When using a gas heating system, the ACM must require the user to identify if the gas heating system is ducted or non-ducted and if it is a central gas furnace system, or a non-central gas furnace system. If the system is a non-ducted non-central gas furnace system, the ACM must require the user to select the type and size of the equipment from Table 3-5 where the system size, as a default, may be determined as 34 Btu/hour per square foot of conditioned floor area.



Table 3-5 -- Non-Ducted Non-Central Heating Equipment Default Efficiencies

Gas Fired Wall Furnaces, Floor Furnaces and Room Heaters			Seasonal Efficiency
Wall	fan type	up to 42,000 Btu/hour	73%
		over 42,000 Btu/hour	74%
	gravity type	up to 10,000 Btu/hour	59%
		over 10,000 Btu/hour up to 12,000 Btu/hour	60%
		over 12,000 Btu/hour up to 15,000 Btu/hour	61%
		over 15,000 Btu/hour up to 19,000 Btu/hour	62%
		over 19,000 Btu/hour up to 27,000 Btu/hour	63%
		over 27,000 Btu/hour up to 46,000 Btu/hour	64%
		over 46,000 Btu/hour	65%
Floor		up to 37,000 Btu/hour	56%
		over 37,000 Btu/hour	57%
Room		up to 18,000 Btu/hour	57%
		over 18,000 Btu/hour up to 20,000 Btu/hour	58%
		over 20,000 Btu/hour up to 27,000 Btu/hour	63%
		over 27,000 Btu/hour up to 46,000 Btu/hour	64%
		over 46,000 Btu/hour	65%

**Standard Design:** When electricity is used for heating, the heating equipment for the *Standard Design* shall be an electric heat pump with a Heating Seasonal Performance Factor (HSPF) of 6.8 except when *Proposed Designs* use a single package heat pump only, the *Standard Design* shall assume an HSPF of 6.6. When electricity is not used for heating, the equipment used in the *Standard Design* building shall be either a gas furnace with an Annual Fuel Utilization Efficiency (AFUE) of 0.78 for central systems, or shall be a gas furnace of the type specified in the proposed design at the efficiency level shown in Table 3-5 for non-central systems. If the *Proposed Design* has both electric and fossil-fuel-fired heating equipment types, the standard system shall be based on the floor area weighted Source Seasonal Efficiency (SSE). In calculating the weighted average SSE, the efficiencies of all heating equipment and distribution systems are converted to source seasonal efficiencies (SSE), as shown in Equations 3.1 and 3.2.

Seasonal air distribution efficiencies ( $\eta_{\text{dist, seasonal}}$ ) for the *Proposed Design* and the *Standard Design* shall be calculated using the procedures and algorithms in Appendix F. The seasonal distribution efficiencies for the *Standard Design* shall be calculated using the defaults specified in Appendix F. The seasonal distribution system efficiency shall be calculated using the seasonal delivery effectiveness ( $\text{DE}_{\text{seasonal}}$ ), the equipment efficiency factor ( $F_{\text{equip}}$ ), and the thermal recovery factor ( $F_{\text{recov}}$ )



$$h_{dist, seasonal} = DE_{seasonal} \times F_{equip} \times F_{re cov} \quad \text{Equation 3.1}$$

$$SSE_{gas\ with\ fan} = \left( \frac{1 + (0.005 \times 3.413)}{\left\{ \frac{1}{AFUE} \right\} + (0.005 \times 10.239)} \right) h_{dist, seasonal} = 0.7628 \times h_{dist, seasonal} \quad \text{Equation 3.2}$$

$$SSE_{electric} = \left( \frac{HSPF}{10.239} \right) \times h_{dist, seasonal} \quad \text{Equation 3.3}$$

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### 3.8.2 Cooling Equipment

**Proposed Design:** ACMs must be able to model the basic types of cooling equipment listed in Table 2-4. ACMs must require the user to enter the basic information to model the energy use of these pieces of equipment. At the minimum this includes some type of seasonal distribution system efficiency for cooling, identification of whether the cooling system is ducted or non-ducted and central or non-central. If the cooling system is non-ducted non-central, the ACM must require the user to select the type and size of the equipment from those shown in Table 3-6.



Table 3-6 -- Non-Ducted Non-Central Cooling Equipment Default Efficiencies

Room Air Conditioner Type		Cooling Capacity	Energy Efficiency Ratio
Reverse Cycle	Side Louvers		
Without	with	less than 6,000 Btu	8.0
		6,000 to 7,999 Btu	8.5
		8,000 to 13,999 Btu	9.0
		14,000 to 19,999 Btu	8.8
		20,000 and more Btu	8.2
	without	less than 6,000 Btu	8.0
		6,000 to 7,999 Btu	8.5
		8,000 to 13,999 Btu	8.5
		14,000 to 19,999 Btu	8.5
		20,000 and more Btu	8.2
With	with	All	8.5
	without	All	8.0

**Standard Design:** If a packaged ducted central air conditioner (*PkgAirCond* or *LrgPkgAirCond*) or ducted central packaged heat pump (*PkgHeatPump* or *LrgPkgHeatPump*) is used for the *Proposed Design*, the cooling system used in the *Standard Design* building shall be a single package air conditioner (*PkgAirCond* or *LrgPkgAirCond*) with an SEER (seasonal energy efficiency ratio) of 9.7. Otherwise, the cooling system for the *Standard Design* building with a central system shall be a split system central air conditioner (*SplitAirCond*) with an SEER of 10.0. For non-ducted non-central cooling equipment, the efficiencies shall be as shown in Table 3-6 for the type and size in the *Proposed Design* where the size may be a user input or shall default to 24 Btu per hour per square foot of conditioned floor area. In the case of *NoCooling* for the *Proposed Design*, the cooling system for the *Standard Design* building shall be a split system air conditioner (*SplitAirCond*) with an SEER of 10.0. When a *Proposed Design* uses both a split system air conditioner and another type of air conditioner, the *Standard Design* SEER shall be a conditioned floor area weighted average of the equivalent SEER of the cooling equipment.

### 3.8.3 Ducts and HVAC Seasonal Distribution System Efficiency for Ducted Systems

**Proposed Design:** As a default, HVAC ducts for ducted systems are assumed to exist and are located in the attic. Likewise, as a default, the air handler is assumed to be located in the attic. Proposed HVAC systems with a duct layout and design on the plans may locate the ducts in the crawlspace or a basement if the layout and design specify that all of the supply registers are located in the floor and show the appropriate



locations for the ducts. When all of the supply registers are located in the floor or all of the supply registers are located in the ceiling, the ACM can use Table 4.1 of Appendix F to allocate the duct surface areas. If all supply registers are in the floor, but the building has both a crawlspace and a basement, the duct location may be taken as a floor area weighted average of the entries in Table 4.1 of Appendix F. If any story of a building has supply registers in both the floor and more than two feet above the floor, the duct location for that story must be modeled as 100% ducts in the attic. If the modeled duct location for a given story is not in the attic, the ACM must specify that all supply registers for that story of the building (or the whole building) are located in the floor in the *Special Features and Modeling Assumptions* listings for special verification by the local enforcement agency.

Proposed HVAC systems with a complete ACCA Manual D design including the duct layout and design on the plans may allocate duct surface area in more detail in the ACM model but the distribution of duct surface areas by location must appear on the *HERS Required Verification* list for verification by a HERS rater.

In a similar fashion, the supply duct surface area (and the location of the ducts) of an ACCA Manual D designed duct system may be modeled explicitly in the ACM and receive energy efficiency credit. When a non-default supply duct surface area is modeled, the supply duct surface area is subject to verification by a HERS rater and must be listed on the *HERS Required Verification* listings. The HERS rater must also verify the existence of the ACCA Manual D design and layout and the general consistency of the actual HVAC distribution system with the design. The HERS rater must also measure and verify the fan flow and confirm that it is consistent with the ACCA Manual D design specifications.

The ACM shall allow users to specify if they will be using diagnostic testing of HVAC distribution efficiency of a fully-ducted system by a HERS rater during the construction of the building to confirm the modeling of improved HVAC distribution efficiency measures such as duct leakage. The default shall be that no diagnostic testing will be done. Duct efficiency credits may not be taken and diagnostic testing may not be done on any HVAC system that uses building cavities such as plenums or a platform return. If the user does not select diagnostic testing, the ACM shall require users to input at least two (2) basic parameters to determine HVAC distribution efficiency: the total conditioned floor area of the building as specified above and the R-value of the duct insulation which may be defaulted to R4.2. Additional data may be required to determine seasonal distribution system efficiency, the default input parameters are presented in Appendix F. If the user specifies diagnostic testing to be performed during construction, the ACM shall request the user to enter the data described in Section 4.18, *Duct Efficiency* and shall report all required measurements and the features used to achieve higher HVAC distribution efficiencies in the *HERS Required Verification* listings. When the user chooses diagnostic testing, the diagnostic testing shall be performed as described in Appendix F. Diagnostic testing must be reported in the *HERS Required Verification* listings on the CF-1R and C-2R as described in Chapter 2.



**Standard Design:** The standard heating and cooling system for central systems is assumed to have air distribution ducts located in an attic space, 22% total duct leakage, non-ACCA Manual D designed duct system, and no radiant barrier. R-4.2 duct insulation is assumed for the *Standard Design* building. The *Standard Design* building is assumed to have the same number of stories as the *Proposed Design* for purposes of determining the duct efficiency. HVAC distribution system efficiencies must be calculated using the algorithms and equations in Appendix F of this manual for both the *Proposed Design* and the *Standard Design*. The *Standard Design* calculation must use the default values of that procedure. For non-central HVAC systems, the *Standard Design* shall have no ducts.

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### 3.9 Infiltration/Ventilation

The intentional or unintentional replacement of conditioned indoor air by unconditioned outdoor air creates heat gains or heat losses for a conditioned building. This exchange of indoor and outdoor air occurs for all buildings to a greater or lesser extent. Mechanical ventilation gives a certain degree of control of the rate of this exchange and depending on the balancing of the ventilation may create building pressurization.

**Proposed Design:** As a default, ACMs shall not require the user to enter any values related to infiltration or mechanical ventilation for air quality and shall set the infiltration level to be the same as the standard design. ACMs shall allow a user to specify if they will be using diagnostic testing during building construction or if they wish to take infiltration reduction credit for an air-retarding wrap or reduced duct leakage. An air retarding wrap can qualify for a default reduction in Specific Leakage Area (SLA) of 0.50 without confirmation by diagnostic testing. The air retarding wrap must be tested and labeled by the manufacturer to comply with ASTM E1677-95, *Standard Specification for an Air Retarder (AR) Material or system for Low-Rise Framed Building Walls* and have a minimum perm rating of 10. The air-retarding wrap must be installed per the manufacturer's specifications that must be provided to comply with ASTM E1677-95. The default infiltration (no diagnostic testing and measurement of infiltration) credit for reduced duct leakage is also an SLA reduction of 0.50. Neither of these credits may be taken if the user chooses a diagnostic testing target for reduced infiltration. Either of these prescriptive infiltration reduction credits are special features and must be listed in the *Special Features and Modeling Assumptions* listings of the CF-1R and C-2R. The air retarder specifications listed above must also be reported in the *Special Features and Modeling Assumptions* listings when an air retarder is modeled by the ACM. If the user specifies they will be using diagnostic testing during construction, for either reduced infiltration or reduced infiltration with mechanical ventilation, the ACM must require the user to choose an input menu to enter a target value for measured CFM50<sub>H</sub> or the SLA corresponding to the target CFM50<sub>H</sub>, and, if mechanical ventilation is to be used, the wattage and cfm of the ventilation supply and exhaust fans. Note that when the *Proposed Design* target value for reduced infiltration falls below a value corresponding to an SLA of 3.0, mechanical ventilation is required and this requirement must be reported as described in Chapter 2. Whenever mechanical ventilation is modeled (required or not), the



volumetric capacity modeled must be at least 0.047 cfm/ft<sup>2</sup> of conditioned floor area. This minimum capacity is needed to provide adequate ventilation for indoor air quality. If the user attempts to model total mechanical volumetric capacity (balanced + unbalanced) less than 0.047 cfm/ft<sup>2</sup>, then the ACM must indicate an input error and automatically block compliance output.

Tested infiltration below a value corresponding to an SLA of 1.5 is not allowed unless mechanical **supply** ventilation is installed adequate to maintain the residence at a pressure greater than -5 pascals relative to the outside average air pressure with other continuous ventilation fans operating. When the user chooses diagnostic testing, the diagnostic testing shall be performed using fan pressurization of the building in accordance with ASTM E 779-1987 (Reapproved 1992), *Standard Test Method for Determining Air Leakage Rate by Fan Pressurization* and the equipment used for this test must meet the instrumentation specifications found in Section 4.1 of Appendix F. The specifications for diagnostic testing and the target values specified above must be reported in the *HERS Required Verification* listings on the CF-1R and C-2R as described in Chapter 2.

**Standard Design:** The *Standard Design* does not use mechanical ventilation and assumes infiltration corresponding to an Specific Leakage Area (SLA) of 4.9 for ducted HVAC systems and an SLA of 3.8 for non-ducted HVAC systems.

Refer to Sections 4.17 and 4.17.1 for more detailed information.

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### 3.10 Additions

Additions are treated as separate new buildings except for the determination of internal heat gains which are specified in Section 4.5 for the purpose of determining a *Standard Design* for the addition. The modeling of additions or alterations must be reported in the *Special Features and Modeling Assumptions* listings which must state that the building vintage, the input assumptions corresponding to this vintage must be verified prior to alteration to receive credit.

When an existing HVAC system is extended to serve an addition, the default assumptions for duct and HVAC distribution efficiency must be used for both the *Proposed Design* and the *Standard Design*. However, when a new, high efficiency HVAC distribution system is used to serve the addition or the addition and the existing building, that system may be modeled to receive energy credit subject to diagnostic testing and verification of proper installation by a HERS rater.

**Proposed Design:** The user must enter an indication that an addition is being modeled and the conditioned floor area of the addition for the *Proposed Design*. When an ACM has the capability of running an existing building plus an addition in a single pass, the addition and the existing building must be entered independently and reported independently. Special output must be created to clearly indicate existing building components separately from new components. Likewise altered existing components must have separate accounting and reporting. Existing building components must be



reported exclusively in lowercase type and new or altered components exclusively in UPPERCASE type for single pass Addition with Existing Building runs or Alteration runs. ACMs that require two or more passes to model these situations do not require these restrictions on type case for existing and new (or altered) component reporting but these ACMs must clearly indicate which run corresponds to existing conditions and which run corresponds to the new or altered conditions and the *Special Features and Modeling Assumptions* listings for both runs must report that two output files, two CF-1Rs and two C-2Rs are required to be checked.

An existing building plus an addition may be modeled by means of two separate compliance runs:

The user or the ACM models the *Existing Building* and the *Addition plus the Altered Existing Building*. There will be two sets of energy use figures for each of these energy simulation runs, the predicted energy use of the modeled building (EU) and the predicted energy budget calculated based on the rules specified in this manual (EB).

Let

$EU_e$  = the energy use of the existing building (*Proposed Design*).

$EB_e$  = the energy budget for the existing building (*Standard Design*).

$EU_{e+a}$  = the energy use of the altered existing building with the addition.

$EB_{e+a}$  = the energy budget of the altered existing building with the addition.

and

$A_e$  = the conditioned floor area of the existing building.

$A_{e+a}$  = the conditioned floor area of the altered existing building with the addition.

$$F = \frac{A_e}{(A_{e+a})} \quad \text{Equation 3.4}$$

The altered existing building with the addition complies with the Standards when Equation 3.5 is satisfied:

$$EU_{e+a} \leq EB_{e+a} + F \times (EU_e - EB_e) \quad \text{Equation 3.5}$$

When no water heating is proposed for the addition, the ACM must report that no water heating energy is being calculated and the energy budgets cannot reflect the use of water heating energy. When a new water heater is replacing the existing water heater for the whole dwelling, the ACM must use the existing plus addition approach to compliance with the water heater modeled with the existing building. When the specifications of the existing water heater are unknown, the water heating budget is determined as if the dwelling were all new construction.

If the addition increases the number of water heaters in the dwelling then the addition *Standard Design* must be modeled with a non-circulating, gas-fired water



heater with a volume which is the lessor of the *Proposed Design* volume or 50 gallons and an Energy Factor of 0.60. If the building does not have gas service, the ACM may allow the *Standard Design* water heater to be a non-circulating electric water heater with an Energy Factor of 0.98.

***Standard Design:*** For additions, the *Standard Design* shall have a total glazing area equal to that allowed by Package D and the conditioned floor area of the addition just as for new buildings. For the *Standard Design* the glazing orientation, U-value, and SHGC of the fenestration shall be modeled in the same manner as a new building.

When additions are modeled with an existing building, the ACM must require the user to determine and enter the vintage of the existing building. The ACM shall then use the default assumptions specified in Table 3-7 for modeling the existing structure. If the ACM allows the user to enter higher U-values, higher F2 values, higher SHGCs, lower efficiencies, or lower energy factors than the vintage defaults from Table 3-7 for the existing building's *Proposed Design*, the ACM must report such values as special features on the *Special Features and Modeling Assumptions* listings.



Table 3-7: Default Assumptions for Existing Buildings						
Default Assumptions for Year Built (Vintage)						
Conservation Measure		Before 1978	1978 to 1983	1984 to 1991	1992 to 1998	1999 +
INSULATION U-VALUE						
Roof		0.076	0.047	0.047	0.047	0.047
Wall		0.386	0.096	0.096	0.088	0.088
Raised Floor -CrawlSp		0.097	0.097	0.097	0.037	0.037
Raised Floor-No CrawlSp		0.239	0.239	0.239	0.097	0.097
Slab Edge	F2 =	0.76	0.76	0.76	0.76	0.76
Ducts		R-2.1	R-2.1	R-2.1	R-4.2	R-4.2
LEAKAGE						
Building (SLA)		4.9	4.9	4.9	4.9	4.9
Ducts		28%	28%	28%	28%	28%
FENESTRATION						
U-value		Use Table 1-D - Title 24, Part 6, Section 116 for all Vintages				
SHGC		Use Table 1-E - Title 24, Part 6, Section 116 for all Vintages				
Shading Dev.		Use Tables 4.3 and 4.4 for all Vintages				
SPACE HEATING EFFICIENCY						
Gas Furnace (Central) AFUE		0.75	0.78	0.78	0.78	0.78
Heat Pump HSPF		5.6	5.6	6.6	6.6	6.8
Electric Resistance HSPF		3.413	3.413	3.413	3.413	3.413
SPACE COOLING EFFIC.						
All Types, SEER		8.0	8.0	8.9	9.7	9.7
WATER HEATING						
Energy Factor		0.525	0.525	0.525	0.525	0.58
Rated Input, MBH		28.0	28.0	28.0	28.0	28.0



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## 4. Required Modeling Assumptions and Algorithms

Most of the modeling assumptions and algorithms about building operation and climate are either fixed or restricted when an ACM is used for compliance. All approved ACMs must include and automatically use all the appropriate fixed and restricted inputs and calculation methods with no special entry required by the user. Users may not override the fixed inputs when the ACM is used for compliance calculations, nor may they be allowed to go beyond the limitations of the restricted assumptions.

The fixed and restricted modeling assumptions apply to both the *Standard Design* run and to the *Proposed Design* run. The *standard* fixed and restricted modeling assumptions always apply to the *Standard Design* run and are the *default* for the *Proposed Design* run. In some cases, the CEC has approved *alternate* fixed and restricted modeling assumptions that may be used in the *Proposed Design* run. The alternate modeling assumptions may only be used when the *Proposed Design* run has a special building feature (e.g. zonal control) that is recognized as an approved Exceptional Method, and the ACM has been approved with this optional modeling capability. The modeling of such building features for compliance purposes must always be documented as entries in the *Special Features and Modeling Assumptions* listings on the Certificate of Compliance and on the Computer Method Summary.

The following subsections describe the fixed and restricted modeling assumptions or computer inputs and explain how they apply to both the *Standard Design* run and the *Proposed Design* run.

When this manual describes the algorithms and calculational methods used by the reference method, an ACM may use alternative algorithms to calculate the energy use of low-rise residential buildings provided that the algorithms are used consistently for the *Standard Design* and the *Proposed Design* and provided that the ACM passes the applicable tests described in Chapters 5 and 6 and provided that the appropriate input summaries and output information is correctly produced by the ACM. The reference methods of calculation are implemented in the CALRES98 computer program and used to generate the tests in Chapters 5 and 6.

However, certain algorithms and calculational procedures such as water heating and duct efficiency calculations must be modeled to produce intermediate results precisely and in detail. Typically the tests for these procedures will consist of random testing and result comparison of these intermediate results from a large number of possible tests and conditions.

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### 4.1 Thermostats

***Standard Design & Proposed Design:*** The *standard* thermostat settings are shown in the table below. These thermostat setpoints apply to the *Standard Design* run and are the default for the *Proposed Design* run.



**Table 4-1 - Thermostat Settings**

	Cooling Mode	Heating Mode
Cooling Thermostat	78°F	78°F
Heating Thermostat	60°F	68°F
Heating Setback	60°F	60°F
Ventilation Setpoints	68°F	77°F
Change-over Temperature	60°F	60°F

It is assumed that the building has a constant cooling setpoint of 78°F. When the building is in a heating mode, the heating setpoint is 68°F with night setback to 60°F. The heating thermostat is set back from 11:00 pm until 7:00 am. During the summer or when the building is in a cooling mode, the heating setpoint is a constant 60°F.

The ventilation setpoint is 68°F when the building is in a cooling mode and 77°F when the building is in a heating mode. The state of the building's conditioning mode is dependent upon the outdoor temperature averaged over hours 1 through 24 of day 8 through day 2 prior to the current day. The ACM shall calculate and update daily this seven day running average of outdoor air temperature. When this average temperature is equal to or less than 60°F the building shall be set in a heating mode and all the thermostat setpoints for the heating mode shall apply. When the running average is greater than 60°F the building shall be set to be in a cooling mode and the cooling mode setpoints shall apply.

The standard heating and cooling setpoints are shown in Table 4-2 below for each hour of the day.

**Table 4-2 - Standard Thermostat Set Points**

Hour	Heating	Cooling	Hour	Heating	Cooling	Hour	Heating	Cooling
1	60	78	9	68	78	17	68	78
2	60	78	10	68	78	18	68	78
3	60	78	11	68	78	19	68	78
4	60	78	12	68	78	20	68	78
5	60	78	13	68	78	21	68	78
6	60	78	14	68	78	22	68	78
7	60	78	15	68	78	23	68	78
8	68	78	16	68	78	24	60	78

**Proposed Design:** An optional capability, described in Section 6.2, allows alternative thermostat schedules to be used for the *Proposed Design* run when the HVAC system meets the requirements for zonal control. With zonal control, the building is divided into sleeping and living areas and a separate schedule is used for each area. If the user selects this option the ACM shall select the appropriate alternative schedules based on the user's designations for sleeping and living zones and shall automatically report the use of this optional capability in the *Special Features and Modeling Assumptions* listings in the required standard reports.



Certain types of heating and/or cooling equipment are exempt from the mandatory requirement for setback thermostats, including wall furnaces and through-the-wall heat pumps. If setback thermostats are not installed, then the ACM shall model the *Proposed Design* with the standard thermostat schedule, except that the heating mode setback setpoint shall be 66°F instead of 60°F. In cases where setback thermostats are not mandatory but nonetheless are installed by the builder, the ACM shall model the *Proposed Design* using the standard heating setback setpoint of 60°F. The *Standard Design* always assumes the setback schedule shown in Table 4-2.

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## 4.2 R-Value/U-Value Determinations and Calculations

According to the Standards, the R-value of a material is “the [thermal] resistance of a material or building component to the passage of heat in (hr x ft<sup>2</sup> x °F)/Btu.”

The R-value indicates how well a material prevents heat from flowing through it. R-19 insulation, for example, is only half as effective at slowing heat transfer as R-38 insulation.

Overall thermal resistances (overall R-values) and overall thermal transmittance values (overall U-value) shall be calculated using algorithms and methods consistent with the algorithms and methods in the 1997 ASHRAE Handbook of Fundamentals, Chapters 22, 23 and 24. For construction assemblies or portions of construction assemblies that consist of two or more plane parallel layers of materials in series (such as exterior siding, insulation and interior gypsum board), the thermal resistance of the assembly is equal to the sum of the individual thermal resistances. When layers are penetrated or interrupted by wood framing or other framing elements that do not readily conduct heat, the parallel path method shall be used to calculate the R-value and U-value of the construction assembly. When metal framing is used or construction layers are penetrated by other significant amounts of highly heat conductive materials such as metals, the zonal calculation method, modified zonal calculation method, finite element or finite difference methods, or the Commission’s EZ-frame computer program must be used to determine overall R-value and overall U-value.

Most typical constructions can be calculated using the parallel path method and documented using the residential compliance Form 3R.

The U-value is the inverse of the total R-value:

$$U = 1/R_{\text{Total}} \quad \text{Equation 4.1}$$

The U-value is the heat transfer coefficient expressed in Btu/ft<sup>2</sup>-hr-°F, the rate at which heat flows through an assembly or material.

The total R-value shall be entered, displayed, and calculated to at least three significant figures, or, alternatively to two decimal places, and the total U-value to two significant figures or three decimal places whichever is more precise.



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### 4.2.1 Default R-values/U-values in Appendix E

Appendix E contains pre-calculated Form 3Rs for a number of standard assemblies. The Total R-values and U-values from these assemblies must be used in compliance calculations unless a Form 3R is completed for the actual proposed assembly, or unless the compliance approach only uses the insulation level alone. Table E-7 in Appendix E summarizes these default U-values.

Appendix E also includes Form 3Rs for assemblies that meet the default U-values with a combination of batt and rigid insulation, rather than only batt insulation (including metal frame assemblies). In addition, it contains R-values and other information on a variety of masonry wall assemblies.

To determine if an assembly meets the minimum insulation levels required by the mandatory measures or the prescriptive packages, obtain the U-value of the proposed assembly or complete a Form 3R and see if the proposed U-value is less than or equal to the standard U-value for that assembly type and insulation level as listed in Table 3-1 in Chapter 3 and Table E-2 in Appendix E. Compare the proposed U-value to the U-values listed for framing spacing of 16" o.c. for walls and 24" o.c. for roofs/ ceilings.

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## 4.3 *Basement Modeling - Basement Walls and Floors*

Below grade walls shall have no exterior absorptivity (no radiant gain from sunlight). Below grade walls are modeled with three exterior conditions depending on whether the depth is shallow, medium, or deep.

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### 4.3.1 Shallow Depth Walls

The first two feet (inclusive) of the below grade wall uses the average air temperature for hours 1 through 24 of the 7 days beginning 8 days prior to the current day (days -8 through -2). In addition, a thermal resistance with an R-value of 1.57 (hr.ft<sup>2</sup>.°F/Btu) is added between this average temperature and the outside of the below grade wall.

---

### 4.3.2 Medium Depth Walls

The basement walls from more than 2 feet below grade through 6 feet below grade have an exterior temperature that is the average of hours 1 through 24 of the 7 days of outdoor temperature from the period starting 68 days prior to the current day being simulated through 62 days prior to the first hour of the current day being simulated. In addition, a thermal resistance with an R-value of 7.28 (hr.ft<sup>2</sup>.°F/Btu) is added between this lagged average temperature and the outside of the below grade wall.

---

### 4.3.3 Deep Walls and Floors

Walls more than 6 feet below grade and basement floors have an exterior temperature that is typical of deep ground temperatures. These temperatures are given in Table 4-3 below for each of the sixteen climate zones. In addition, a thermal resistance with an R-value of 13.7 (hr.ft<sup>2</sup>.°F/Btu) is added between this average temperature and the outside of the below grade wall. For basement floors this added R-value is 17.6 hr.ft<sup>2</sup>.°F/Btu.



Table 4-3 Temperatures for Deep Walls and Floors by  
Climate Zone

Climate Zone	Deep Ground Temperature
1	49.1
2	64.5
3	62.8
4	61.4
5	56.8
6	64.1
7	61.6
8	63.9
9	66.4
10	68.9
11	69.5
12	67.8
13	67.6
14	68.6
15	74.6
16	54.1

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## 4.4 Shading Calculations

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### 4.4.1 Interior Shading and Exterior Sunscreen Operation

**Standard Design & Proposed Design:** The standard assumptions for operation of interior shading devices and sunscreens shall apply to both the *Standard Design* run and the *Proposed Design* run.

Internal shading devices, such as draperies and blinds, are assumed to be closed only for hours when the air conditioner operates. To approximate this affect during transitions between periods of operation and non-operation, ACMs may assume that



the internal device remains closed for the hour following the period of air conditioner operation. As soon as that hour passes, the internal shading device shall be opened. The internal device shall be either totally open or totally closed for any given hour.

External sunscreens are assumed to be in place all year, whether the building is in a heating or cooling mode.

The shading effects of overhangs, side fins and other fixed shading devices are determined hourly based on the altitude and azimuth of the sun for that hour, the orientation of the fenestration, and the relative geometry of the fenestration and the fixed shading devices.

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#### 4.4.2 Solar Heat Gain Coefficients

Solar Heat Gain Coefficients shall be determined according to Chapter 2 and 3 of this manual. ACMs use two values for setting the Solar Heat Gain Coefficient of shading devices: “ $SHGC_{open}$ ” and “ $SHGC_{closed}$ .” “ $SHGC_{open}$ ” applies when the air conditioner is not in operation (off) and “ $SHGC_{closed}$ ” applies when the air conditioner is in operation. The ACM user shall not be allowed to enter values for  $SHGC_{open}$  and  $SHGC_{closed}$ . These values must be automatically calculated from the specification of the SHGC for the fenestration ( $SHGC_{fen}$ ), the exterior shade and the interior shade as described below. ACMs shall forbid users from direct entry of SHGCs for interior and exterior shading devices. The ACM must automatically determine these values from the user’s choices of interior and exterior shading devices.

There are only a limited set of shading devices with fixed prescribed characteristics that are allowed to be modeled in the performance approach. These devices and their associated fixed Solar Heat Gain Coefficients are given in Tables 2-1 and 2-2 and are repeated below in Tables 4-4 and 4-5. Table 4-4 gives the allowed interior shading devices and Table 4-5 gives the allowed exterior shading devices.



Table 4-4 Allowed Interior Shading Devices and Recommended Descriptors

Recommended Descriptor	Interior Shading Attachment Reference	Solar Heat Gain Coefficient before 1/1/2002	Solar Heat Gain Coefficient after 1/1/2002
<i>Standard</i>	Draperies or No Special Interior Shading -- Default Interior Shade	0.68	0.68 <sup>1</sup>
<i>Blind</i>	Venetian Blinds, Vertical Blinds or MiniBlinds	0.47	0.47
<i>OpRollShd</i>	Opaque Roller Shades	0.47	0.68
<i>None</i> <sup>2</sup>	No Interior Shading - Only for Skylights (Fenestration Tilt < 60 degrees)	1.00	1.00

Note (general): No other interior shading devices or attachments are allowed credit for compliance with the building efficiency standards.

Note 1: Default drapery shading shall be assumed whenever no other interior shading is specified for a window. Output shall note that although *Standard* is specified, a drapery is modeled but it is not required to be installed and present at final inspection. Output shall note for any interior shading device other than drapery that it must be installed and present at final inspection.

Note 2: *None* is the default for fenestration tilted less than 60 degrees from horizontal (skylights) and is only allowed for fenestration tilted less than 60 degrees from horizontal (skylights)., i.e. *None* is not an interior shading option for ordinary vertical windows.



Table 4-5 Allowed Exterior Shading Devices and Recommended Descriptors

Recommended Descriptor	Exterior Shading Device Reference	Solar Heat Gain Coefficient
<i>BugScrn</i>	Bug Screen or No Shading - Default Bug Screens are modeled	0.76
<i>WvnScrn</i>	Woven SunScreen (SC<0.35)	0.30
<i>LvrScrn</i>	Louvered Sunscreen	0.27
<i>LSASnScrn</i>	LSA Sunscreen	0.13
<i>RIDownAwng</i>	Roll-down Awning	0.13
<i>RIDownBlnds</i>	Roll -down Blinds or Slats	0.13
<i>None</i> <sup>1</sup>	For skylights only - No exterior shading	1.00

Note 1: *None* is the default for fenestration tilted less than 60 degrees from horizontal (skylights) and is only allowed for fenestration tilted less than 60 degrees from horizontal (skylights), i.e. *None* is not an interior shading option for ordinary vertical windows.

The formula for combining Solar Heat Gain Coefficients is:

$$SHGC_{comb} = \left[ (0.2875 \times SHGC_{max}) + 0.75 \right] \times SHGC_{min}$$

Equation 4.2

Where

$SHGC_{comb}$  = the combined solar heat gain coefficient for a fenestration component and an attachment in series.

$SHGC_{max}$  = the larger of  $SHGC_{fen}$  and  $SHGC_{dev}$

$SHGC_{min}$  = the smaller of  $SHGC_{fen}$  and  $SHGC_{dev}$

where

$SHGC_{fen}$  = the Solar Heat Gain Coefficient of the fenestration which includes the window glazing, transparent films and coatings, and the window framing, dividers and muntins,

$SHGC_{dev}$  = the Solar Heat Gain Coefficient of the interior or exterior shading device when used with a metal-framed, single pane window.

For  $SHGC_{closed}$ , the combination  $SHGC$ ,  $SHGC_{fen+int}$ , (the combined  $SHGC$  for the fenestration and the interior device) is calculated first and then the combination  $SHGC_{fen+int+ext}$  is calculated to determine the overall  $SHGC_{closed}$ .  $SHGC_{open}$  is determined from the combination of  $SHGC_{fen}$  and  $SHGC_{ext}$ .



The combination  $SHGC_{fen+int}$  is calculated as above for the *Standard Design* when the Package D specification for SHGC is No Requirement with  $SHGC = NR$  (No Requirement) set to a default SHGC of 0.70, which is typical of a double pane, metal-framed window needed to meet the package U-value requirements.

$$SHGC_{fen+int} = [(SHGC_{fen} \times 0.2875) + 0.75] \times SHGC_{drap}$$

or

$$SHGC_{fen+int} = [(0.70 \times 0.2875) + 0.75] \times 0.68 = [0.95125] \times 0.68 = 0.64685$$

With the effects of the exterior shade,

$$SHGC_{fen+ext} = [(SHGC_{ext} \times 0.2875) + 0.75] \times SHGC_{fen+int}$$

or

$$SHGC_{closed} = SHGC_{fen+int+ext} = [(0.76 \times 0.2875) + 0.75] \times 0.64685$$

$$= [0.9685] \times 0.64685 = 0.626 \quad \text{and}$$

$$SHGC_{open} = SHGC_{fen+ext} = [(0.76 \times 0.2875) + 0.75] \times 0.70$$

$$= [0.9685] \times 0.70 = 0.678$$

## 4.5 Internal Gains

**Standard Design & Proposed Design:** Internal gain from lights, appliances, people and other sources shall be set to 20,000 Btu/day for each dwelling unit plus 15 Btu/day for each square foot of conditioned floor area (CFA) as shown in Equation 4.3.

$$IntGain_{total} = (20,000 \times N) + (15 \times \sum_{i=1}^N CFA_i) \quad \text{Equation 4.3}$$

where

N= number of dwelling units (NumDwellUnits)

$CFA_i$ =Conditioned Floor Area of  $i^{th}$  dwelling unit

For addition-alone compliance (single-zone), the gains are apportioned according to the fractional conditioned floor area, referred to as the Fractional Dwelling Unit (FDU). For zone j, the internal gain is determined by Equation 4.4:

$$IntGainZone_j = IntGain_{tot} \times FDU_j \quad \text{Equation 4.4}$$

where

$FDU_j$  = Fractional Dwelling Unit of  $j^{th}$  zone, calculated from Equation 4.5

$$FDU_j = \frac{CFA_j}{\sum_{i=1}^N CFA_i} \quad \text{Equation 4.5}$$



When zonal control is a feature of the *Proposed Design* for a single dwelling unit, the total internal gain is split between the living areas and the sleeping areas as described in Section 6.2.3, pg. 6-4

Building additions may be modeled in conjunction with the existing dwelling or modeled separately (see Sections 6.7.1 and 6.7.2). When modeled together the number of dwelling units for the proposed dwelling ( $NDU_{\text{proposed}}$ ) remains equal to the number of dwelling units for the existing structure ( $NDU_{\text{existing}}$ ), while the conditioned floor area ( $CFA_{\text{proposed}}$ ) is increased to include the contribution of the addition ( $CFA_{\text{addition}}$ ). When modeled separately, the internal gain of the addition ( $IntGain_{\text{addition}}$ ) is based on the value of the addition's fractional dwelling unit ( $FDU_{\text{addition}}$ ), as expressed in Equations 4.6 and 4.7.

Modeling additions is an optional capability described in Section 6.7, Page 6-17.

$$IntGain_{\text{addition}} = IntGain_{\text{total}} \times FDU_{\text{addition}} \quad \text{Equation 4.6}$$

where

$$FDU_{\text{addition}} = \frac{CFA_{\text{addition}}}{CFA_{\text{existing}} + CFA_{\text{addition}}} \quad \text{Equation 4.7}$$

## 4.6 Internal Gain Schedules

**Standard Design & Proposed Design:** For hourly computer models, the standard internal gain schedule shown in Table 4.6 applies. "Hour one" is between midnight and 1:00 am. This schedule shall always be used for the *Standard Design* run. It is the default for the *Proposed Design* run and shall be used unless the *Proposed Design* has zonal control. For zonal control assumptions, see Chapter 6, Section 6.2.

Table 4-6- Standard Internal Gain Schedule

Hour	Percent	Hour	Percent	Hour	Percent
1	2.4	9	5.6	17	5.7
2	2.2	10	6.0	18	6.4
3	2.1	11	5.9	19	6.4
4	2.1	12	4.6	20	5.2
5	2.1	13	4.5	21	5.0
6	2.6	14	3.0	22	5.5
7	3.8	15	2.8	23	4.4
8	5.9	16	3.1	24	2.7

Daily internal gain shall be modified each month according to the set of multipliers shown in Table 4-7. These multipliers are derived from the number of daylight hours each month.



Table 4-7 - Seasonal Internal Gain Multipliers

Month	Multiplier	Month	Multiplier	Month	Multiplier
Jan	1.19	May	0.84	Sep	0.98
Feb	1.11	Jun	0.80	Oct	1.07
Mar	1.02	Jul	0.82	Nov	1.16
Apr	0.93	Aug	0.88	Dec	1.21

## 4.7 Thermal Mass

**Standard Design & Proposed Design:** Thermal mass is modeled in both the *Proposed Design* and the *Standard Design*. The modeled mass includes the basic thermal mass such as framing, furniture, 0.5" sheetrock, and household appliances as "light" mass elements and specific "heavy" mass elements such as concrete slab floors. This modeled thermal mass has the ability to store heat and thus damp temperature fluctuations in the conditioned space. The *Proposed Design* and the *Standard Design* must have the same "light" mass elements and for most dwellings the *Standard* and *Proposed Designs* will also have and model the same "heavy" mass elements.

ACMs must assume that both the *Proposed Design* and *Standard Design* building have a certain amount of minimum "heavy" thermal mass as a function of the conditioned area of slab floor and conditioned nonslab floor. Unless the *Proposed Design* has thermal mass that exceeds a thermal mass minimum threshold, the modeled thermal mass for both the *Proposed Design* and the *Standard Design* is 20% of the *Proposed Design's* conditioned slab floor area as exposed slab, 80% of the conditioned slab floor area as rug-covered slab, and 5% of the *Proposed Design's* conditioned nonslab floor area as exposed 2 inch thick concrete.

The modeled exposed slab floor has the following default characteristics: a thickness of 3.5 inches, a volumetric heat capacity of 28 Btu/ft<sup>3</sup>-°F, a conductivity of 0.98 Btu-in/hr-ft<sup>2</sup>-°F, a surface conductance of 1.3 Btu/hr-ft<sup>2</sup>-°F (no thermal resistance on the surface). The remaining 80% of the conditioned slab floor shall be modeled as covered thermal mass with the same characteristics as the exposed mass, but with the addition of a surface R-value of 2.0 (hr-ft<sup>2</sup>-°F)/Btu typical of a carpet and pad.

Conditioned nonslab floor area shall be modeled with 5% of the nonslab floor area as exposed thermal mass. This thermal mass is modeled in the *Standard Design* with a thickness of 2.0 inches, a volumetric heat capacity of 28 Btu/ft<sup>3</sup>-°F, a conductivity of 0.98 Btu-in/hr-ft<sup>2</sup>-°F, a surface conductance of 1.3 Btu/hr-ft<sup>2</sup>-°F (no added thermal resistance on the surface). The ACM must also model it this way in the *Proposed Design* unless the *Proposed Design* exceeds the thermal mass threshold. The ACM may also require that the user specify a "high mass" or "passive solar" option before allowing the entry of special mass elements and the modeling of thermal mass when the total thermal mass exceeds the high mass threshold.

**Proposed Design:** The *Proposed Design* may model additional thermal mass when the user selects the ACM's "high mass" building input option by modeling thermal mass in excess of the assumed thermal mass for the *Standard Design* when the equivalent



design thermal mass for the *Proposed Design* reaches or exceeds a specific mass threshold. This threshold is determined by the amount of thermal mass equivalent to 30% of the conditioned slab floor area as exposed 3.5" thick concrete slab, 70% of the conditioned slab floor area as rug-covered 3.5" thick concrete slab and 15% of the conditioned raised floor area as 2 inch thick exposed concrete with the same specifications as those given above. To determine the threshold, this mass is converted to a standard Interior Mass Capacity using the Unit Interior Mass Capacity (UIMC) method described in Appendix I and compared to the design mass to determine if the mass threshold is exceeded.

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#### 4.7.1 Perimeters of Slab Floors and Carpeted Slabs

**Standard Design & Proposed Design:** For *Standard and Proposed Designs* all ACMs must use slab edge F2 values assuming that 20% of the slab floor perimeter is exposed to the conditioned air and 80% of the slab floor perimeter is carpeted or covered with an R-2 insulating layer between the slab and the conditioned air.

**Standard Design:** The slab perimeter shall be assumed to have an F2 value based on perimeter insulation as specified for Alternative Component Package D in Section 151 of the building efficiency standards. The Standard Design also assumes that no unconditioned spaces are attached to the conditioned space (in particular that the garage is detached), hence the total slab perimeter length is either insulated or uninsulated per the requirements of Alternative Component Package D. Hence, for the *Standard Design*, the slab edge heat loss factor, F2, is 0.76 for all climate zones except Climate Zone 16 where F2 is 0.51.

**Proposed Design:** Slab perimeter insulation shall be modeled using an F2 factor for the insulation to be installed and the perimeter length that is to be insulated. The slab perimeter length adjacent to unconditioned spaces such as a garage may be modeled as an R-7 insulated perimeter with an F2 factor of 0.51.

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### 4.8 Solar Gain Targeting

**Standard Design & Proposed Design:** Solar gains from windows or skylights shall not be targeted to mass elements within the conditioned space of the building. In the reference program, CALRES98, all solar gain is targeted to the air or a combined air- and lightweight, high surface area mass node within the building. This modeling assumption is used in both the *Standard Design* run and the *Proposed Design* run, except for sunspaces where the user has flexibility in targeting solar gains subject to certain constraints. Sunspace modeling is an optional capability discussed in Section 6.3.

For compliance purposes, when glazing surfaces enclose unconditioned spaces, such as sunspaces, the user is allowed to target all but 25% of the solar gains from these surfaces to mass elements located within the unconditioned space. Unassigned solar gain is targeted to the air or the combined air/lightweight mass or to high surface area lightweight mass in the unconditioned space. At least 25% of the solar gain from any sunspace fenestration surface must be targeted to high surface area lightweight mass



and/or the air. At most 60% of the solar gain may be targeted to the slab floor of a sunspace, especially in the summer. For compliance purposes, an ACM must automatically enforce these limits and inform the user of any attempt to exceed these limits.

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#### **4.9 Building Heat Capacity**

**Standard Design & Proposed Design:** The heat capacity associated with conventional framed construction includes 1/2 inch gypsum board, wall framing and building contents. The building heat capacity is assumed to be fixed at 3.5 Btu/°F per square foot of conditioned floor area. Other values may be used for unconditioned zones (see Chapter 6).

The assumed value shall apply to the *Standard Design* and shall be the default for the *Proposed Design*.

**Proposed Design:** The value may be adjusted in the *Proposed Design* run for a user-designated high mass design for special building features such as extra thick gypsum board or heavy mass elements. For such calculations, the surface area of gypsum board shall be assumed to be four times the conditioned floor area. The compliance supplement shall contain recommendations for modifying the building heat capacity, when applicable, and the ACM shall identify the variation in building heat capacity as a special feature of the building. This shall be noted in the "*Special Features and Modeling Assumptions*" listings of the standard reports.

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#### **4.10 Standard Weather Data**

**Standard Design & Proposed Design:** All ACMs must use standard weather data for all compliance runs. The standard weather data may be condensed, statistically summarized, or otherwise reduced. However, the basis must be the official Commission's hourly weather data.

The same weather data and weather data format must be used for both the *Standard Design* run and the *Proposed Design* run.

The official hourly weather data for energy compliance is available from the Commission on 1.44 megabyte, 3.5 inch floppy diskettes (IBM-PC format). There are 16 climate zones with a complete year of 8760 hourly weather records. Each climate zone is represented by a particular city. More detail on the weather formats is given in the description package mailed with the weather tapes. The weather data may be obtained by mailing a written request for the weather data, a self-addressed diskette mailer, and three IBM-formatted 1.44 Megabyte diskettes to: RESACM Weather Data, Residential Office, California Energy Commission, 1516 Ninth Street MS#25, Sacramento, California 95814-5512.



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### 4.11 Ground Reflectivity

**Standard Design & Proposed Design:** ACMs shall assume that the ground surrounding residential buildings has a reflectivity of 20 percent in both summer and winter. This applies to both the *Standard Design* run and *Proposed Design* run.

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### 4.12 Natural Ventilation

The natural ventilation model is derived from the 1997 *ASHRAE Handbook of Fundamentals*. The model considers both wind effects and stack effects.

- Wind effects include wind speed, prevailing direction and local obstructions, such as nearby buildings or hills.
- Stack effects include the temperature difference between indoor air and outdoor air and the difference in elevation between the air inlet and the outlet.

For compliance purposes, the air outlet is always assumed to be 180 degrees or on the opposite side of the building from the air inlet and the inlet and outlet areas are assumed to be equal. The default inlet area (= outlet area) is five percent of the total window area.

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#### 4.12.1 Effective Ventilation Area (EVA)

Both wind and stack driven ventilation depends linearly on the effective ventilation area (EVA). The EVA is a function of the area of the air inlet and the area of the air outlet. For compliance purposes, the default area of air inlet and outlet are both equal to five per cent (half of the total default standard window opening area) of the total window area. For compliance purposes a different window opening areas may be determined from the areas of different window opening types - fixed, sliders, and hinged windows. For research (as opposed to compliance) purposes, inputs for ACMs may enter separate values for inlet and outlet areas.. For compliance purposes, the air inlet and the air outlet are each equal to one-half of the *Free Ventilation Area* described in Section 4.13 below.

When the inlet area and outlet area are equal, the EVA is the same, i.e. equal to the inlet area or the outlet area. Hence for compliance purposes the EVA is equal to one-half of the *Free Ventilation Area*.

---

#### 4.12.2 Stack Driven Ventilation

Stack driven ventilation results when there is an elevation difference between the inlet and the outlet, and when there is a temperature difference between indoor and outdoor conditions.

$$CFM_S = 9.4 \times EVA \times EFF_S \times \sqrt{H \times \Delta T}$$

Equation 4.8

Where:

$CFM_S$  = Air flow due to stack effects, cfm.

9.4 = Constant from ASHRAE.



$EVA$  = Effective ventilation area as discussed above, sf.

$EFF_s$  = Stack effectiveness.

$H$  = Center-to-center height difference between the air inlet and outlet.

$DT$  = Indoor to outdoor temperature difference, °F.

For compliance purposes the stack effectiveness shall be set at 1.0. The ACM user shall not be permitted to alter this value.

$H$  is the *ventilation height difference*. See Section 4.14 for details.

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#### 4.12.3 Wind Driven Ventilation

The general equation for wind driven ventilation is shown below. This equation works in either a direction dependent implementation or a direction independent implementation, as explained later in the text.

$$CFM_w = EVA \times 88 \times MPH \times WF \times EFF_o \times EFF_d \quad \text{Equation 4.9}$$

Where:

$CFM_w$  = Ventilation due to wind, cfm.

$EVA$  = Effective vent area as discussed above, sf.

88 = A constant that converts wind speed in mph to wind speed in feet per minute.

$MPH$  = Wind speed from the weather tape, mph.

$WF$  = A multiplier that reduces local wind speed due to obstructions such as adjacent buildings.

$EFF_o$  = Effectiveness of opening used to adjust for the location of the opening in the building, e.g. crawl space vents.

$EFF_d$  = Effectiveness that is related to the direction of the wind relative to the inlet surface for each hour.

$WF$  is the *wind correction factor*; this input is fixed at 0.25 for compliance calculations.

The effectiveness of the ventilation opening,  $EFF_o$ , is used to account for insect screens and/or other devices that may reduce the effectiveness of the ventilation opening. This input is also used to account for the location of ventilation area, e.g. the exceptional method for two zone crawl space modeling provides for an alternative input for  $EFF_o$ .

This input is fixed at 1.0 for compliance calculations other than crawlspace modeling.

ASHRAE recommends that the effectiveness of the opening,  $EFF_d$ , be set to between 0.50 and 0.60 when the wind direction is perpendicular or normal to the inlet and outlet. A value of 0.25 to 0.35 is recommended for diagonal winds. When the wind direction is parallel to the surface of the inlet and outlet,  $EFF_d$  should be zero.

For compliance calculations, the orientation of the inlet and outlet is not considered.

ACMs shall assume that the wind angle of incidence at 45 degrees on all windows and



only the wind speed dependence is maintained. In this case, the product of  $EFF_o$  and  $EFF_d$  is equal to 0.28 regardless of the direction of the wind.

---

#### 4.12.4 Combined Wind and Stack Effects

Stack effects and wind effects are calculated separately and added by quadrature, as shown below. This algorithm always adds the absolute value of the forces; that is, wind ventilation never cancels stack ventilation even though in reality this can happen.

$$CFM_t = \sqrt{CFM_w^2 + CFM_s^2} \quad \text{Equation 4.10}$$

Where:

$CFM_t$  = Total ventilation rate from both stack and wind effects, cfm.

$CFM_w$  = Ventilation rate from wind effects, cfm.

$CFM_s$  = Ventilation rate from stack effects, cfm.

---

#### 4.12.5 Determination of Natural Ventilation for Cooling

The value of  $CFM_t$  described in Equation 4.10 above gives the maximum potential ventilation when the windows are open. The amount of natural ventilation used by ACMs for natural cooling is the lesser of this maximum potential amount available and the amount needed to drive the interior zone temperature down to the natural cooling setpoint temperature when natural cooling is needed and available. When natural cooling is not needed or is unavailable no natural ventilation is used. ACMs shall assume that natural cooling is needed when the building is in “cooling mode” and when the outside temperature is below the estimated zone temperature and the estimated zone temperature is above the natural cooling setpoint temperature. Only the amount of ventilation required to reduce the zone temperature down to the natural ventilation setpoint temperature is used and the natural ventilation setpoint temperature must be constrained by the ACM to be greater than the heating setpoint temperature.

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### 4.13 Free Ventilation Area

Free ventilation area is the adjusted area taking into account bug screens, window framing and dividers, and other factors.

**Standard Design:** The *Standard Design* value for free ventilation area is 10% of the fenestration area (rough frame opening). This value is also used for the window Opening Type *Slider*. The approved ACM compliance manual shall note that fenestration-opening type *Slider* also may be selected by the user or automatically used by the ACM as a default or “*Standard*” opening type. This is based upon the assumption that approximately 40% of the rough frame opening is available for ventilation. Half of this area is considered an air inlet and half an air outlet. This value shall always be used for the *Standard Design* run. It is also the default for the *Proposed Design* run.



**Proposed Design:** Other values may be used in the *Proposed Design* run only when special windows are installed, high mass is installed, and the “high mass” input option is selected [or the ACM determines that *Proposed Design*’s thermal mass exceeds the mass threshold]. The free ventilation area is assumed to be 20% of the fenestration area for hinged type windows such as casements, awnings, hoppers, patio doors and French doors that are capable of a maximum ventilation area of approximately 80% of the rough frame opening. If the ACM user increases the ventilation area for hinged type windows, the ACM must also consider the possible effect of fixed glazing in the building which has no free ventilation area (window opening type *Fixed*). The ACM user may account for additional free ventilation area by entering the total area for sliding windows, the total area for hinged windows, and the total area of fixed windows in the “high mass” menu of the ACM. The ACM must verify that the total area entered for these three types is the same as the total area of windows calculated elsewhere or the ACM may determine the area of fixed windows by subtracting the slider window area and the hinged window area from the total window area if it is less than the total window and skylight area. If the total window and skylight area is less than the area specified for sliding windows and hinged windows the ACM must reduce the area of hinged windows by the difference. The total ventilation area is calculated from the areas of the three possible fenestration opening types, as shown below:

$$\text{Vent}_{\text{Area}} = (\text{Area}_{\text{Slider}} \times 0.1) + (\text{Area}_{\text{Hinged}} \times 0.2) + (\text{Area}_{\text{Fixed}} \times 0.0) \quad \text{Equation 4.11}$$

The ACM’s ability to accept a customized ventilation area is an optional capability. When this optional capability is used, the fact that the user entered a customized free ventilation area and the total areas of each of these three fenestration opening types must be reported in the *Special Features and Modeling Assumptions* listings on the CF-1R and C-2R. Note that the maximum free ventilation area that may be modeled by any ACM for compliance purposes is 20% of the total area of windows and skylights assuming that all windows and skylights are hinged.

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#### 4.14 Ventilation Height Difference

**Standard Design:** The *Standard Design* modeling assumptions for the elevation difference between the inlet and the outlet is two feet for one story buildings and eight feet for two or more stories.

**Proposed Design:** For the *Proposed Design* run, the assumption is the same as the *Standard Design* except that greater height differences may be used with special ventilation features such as high, operable clerestory windows. In this case the height difference is the height between the average center height of the lower operable windows and the average center height of the upper operable windows. Such features must be fully documented on the building plans and noted on the ACM standard reports in the *Special Features and Modeling Assumptions* listings as a condition that requires special verification.



### 4.15 Wind Speed and Direction

**Standard Design & Proposed Design:** Wind speed affects the infiltration rate and the natural ventilation rate. The infiltration and ventilation rate in the reference method accounts for local site obstructions. For infiltration in the reference method this is done by using Shielding Class 4 coefficients in the Sherman-Grimsrud equation (Section 4.17.1, Equation 4.17) to determine the stack and wind driven infiltration and ventilation. This Shielding Class determination was made on the basis of the description of the Shielding Classes given in the 1997 ASHRAE Handbook of Fundamentals, Table 7, Page 25.22. For Shielding Class 4 the description reads:

Heavy shielding; obstructions around most of the perimeter, buildings or trees within 30 feet in most directions; typical suburban shielding.

For natural ventilation in the reference method, the wind speed used in calculations is adjusted for differences between the measured wind speed height and the inlet opening height and local obstructions by using a wind factor (WF in Equation 4.9) of 0.25.

### 4.16 Solar Gain

Solar gain through glazing shall be calculated using the methods documented in the *Algorithms and Assumptions Report, 1988*. This method is modified, however, for the 1998 standards. Solar gain through windows is reduced to 67.5 percent of the full solar gain and a new algorithm is used to calculate the transmitted solar gain as a function of the angle of incidence on the glazing. The 0.675 reduction is intended to compensate for exterior shading from landscaping, terrain, and adjacent buildings, as well as dirt and other window obstructions.

The formulas used to calculate the solar heat gain through windows as a function of the angle of incidence are given below in the form of two multipliers: -  $G_{dir}$  - the ratio of the solar heat gain to the space relative to direct beam insolation at normal incidence, and  $G_{dif}$  - the ratio of solar heat gain to the space relative to the diffuse insolation on a horizontal surface. These ratios have no units of measure.

$$G_{dir} = SHGC_{fen} * Area * [fsunlit * CosI * P(CosI) + GrndFac] \quad \text{Equation 4.12}$$

and

$$G_{dif} = SHGC_{fen} * Area * DMSHGC * (vfSky + vfGrnd * GrndRf) \quad \text{Equation 4.13}$$

where

$$P(CosI) = C1 * CosI + C2 * Cos^2 I + C3 * Cos^3 I + C4 * Cos^4 I \quad \text{Equation 4.14}$$

$$GrndFac = vfGrnd \times CosG \times GrndRf \times DMSHGC \quad \text{Equation 4.15}$$

$SHGC_{fen}$  = Fenestration Solar Heat Gain Coefficient at normal beam incidence - primary user input  
[unitless]



$CosI$	=	The cosine of the angle of incidence of the direct beam insolation on the window. [unitless]
$CosG$	=	The cosine of the angle of incidence of the direct beam insolation on the ground. [unitless]
DMSHGC	=	Diffuse Multiplier for Solar Heat Gain Coefficient [unitless]
$f_{sunlit}$	=	fraction of the window sunlit by direct beam at this hour [unitless]
$C1, ..., C4$	=	polynomial coefficients for angular dependence (cosine of the angle of incidence) of solar heat gain - see Table 4-8.
$vf_{sky}$	=	view factor of window to sky [unitless]
$vf_{grnd}$	=	view factor from window to ground [unitless]
$GrndRf$	=	Ground Reflectance [unitless] = 0.20

Table 4-8 Polynomial Coefficients for Angular Dependence

Glazing Type:	Single Pane (1 light)	More Than One Pane (2 or more lights)
$SHGC_{fen}$	0.860	0.695
C1	3.549794	1.881643
C2	-4.597536	1.014431
C3	2.432124	-4.009235
C4	-0.384382	2.113160
DMSHGC	0.905814	0.828777

### 4.17 Infiltration/Ventilation

The effective leakage area method of calculating infiltration for conditioned zones was implemented with the 1992 standards and is still used, but Shielding Class 4 is used for infiltration wind speed reduction, based on the description in the 1997 *ASHRAE Handbook of Fundamentals*.

Effective leakage areas with ACMs is specified in terms of a default specific leakage area of 4.9 for designs with ducted HVAC systems and an SLA of 3.8 for nonducted HVAC systems. These Specific Leakage Areas (SLA) are the defaults for the *Proposed Design* and the assumed standard value for the *Standard Design*. The specific leakage area is the ratio of the effective leakage area to the floor area of the building in the same units. The value is increased by 10,000 to provide a more manageable metric.

$$SLA = \left( \frac{ELA}{CFA} \left( \frac{ft^2}{144in^2} \right) 10000 \right) = \left( \frac{ELA}{CFA} \right) 69.444 \quad \text{Equation 4.16}$$

Where:

ELA = Effective leakage area in square inches



CFA = Conditioned floor area

SLA = Specific leakage area

For both the *Standard Design* and the *Proposed Design*, ACMs shall assume that occupants will open the windows if the house becomes “too stuffy.” When natural ventilation, infiltration, and mechanical ventilation fall below a threshold value, the occupants are assumed to open the windows at the beginning of the next hour sufficient to provide an indoor air quality increment which is equal to an additional 0.35 air changes per hour for an eight foot high ceiling. The windows are assumed to remain open and provide this increment of (0.35 air changes per hour) as long as the previous hour’s infiltration, mechanical and natural ventilation rate without this window ventilation for indoor air quality is below the threshold value (see Equations 4.22 through 4.24)

Calculation of Infiltration and Ventilation

#### 4.17.1 Calculation of Infiltration and Ventilation

The Effective Leakage Area (ELA) method of calculating infiltration for conditioned zones is documented below and in Chapter 25 of the 1997 ASHRAE Handbook of Fundamentals. The ELA for the *Standard Design* and for the default values for the *Proposed Design* if diagnostic tests are not used, is calculated using the Conditioned Floor Area (CFA) and the Specific Leakage Area (SLA) from Section 4.16 above.. (The SLA is the ratio of the effective leakage area to the conditioned floor area of the building, in the same units, multiplied by a factor of 10,000 to provide a more manageable metric.) The energy load on the conditioned space from infiltration heat gains or losses are calculated as follows.

$$CFM_{infil} = ELA \times \sqrt{A \times \Delta T_2 + B \times V^2} \quad \text{Equation 4.17}$$

$$CFM_{infil+unbalfan} = \sqrt{CFM_{infil}^2 + MECH_{unbal}^2} \quad \text{Equation 4.18}$$

$$CFM_{infil+totfan} = CFM_{infil+unbalfan} + MECH_{bal} \quad \text{Equation 4.19}$$

The volumetric air flow (cfm) due to natural ventilation is derived from the natural ventilation cooling for the hour:

$$CFM_{natv} = \frac{Q_{natv}}{1.08 \times \Delta T_1} \quad \text{Equation 4.20}$$

The total ventilation and infiltration (in cfm) including indoor air quality window operation is:

$$CFM_{total} = CFM_{natv} + CFM_{infil+totfan} + CFM_{iaq} \quad \text{Equation 4.21}$$

The value of  $CFM_{iaq}$  depends on the sum of  $CFM_{natv}$  and  $CFM_{infil+totfan}$  from the previous time step:

When



$$CFM_{natv} + CFM_{infil+totfan} < \frac{(AFT \times CFA)}{7.5} \quad \text{Equation 4.22}$$

then

$$CFM_{iaq} = \frac{(0.35 \times CFA)}{7.5} \quad \text{Equation 4.23}$$

otherwise

$$CFM_{iaq} = 0.000 \quad \text{Equation 4.24}$$

where

CFA = the total conditioned floor area of the residence

AFT = 0.18 for Climate Zones 2 through 15 inclusive, and;

AFT = 0.25 for Climate Zones 1 and 16.

When the windows are opened they provide a ventilation rate equal to 0.35 air changes per hour for a residence of the same floor area but with eight foot high ceilings.  $CFM_{iaq}$  simulates the opening of windows to achieve an acceptable indoor air quality by the occupants when ventilation and infiltration from other sources does not provide an adequate quantity of outdoor air to dilute pollutants and refresh the indoor air.

The energy load on the conditioned space from all infiltration and ventilation heat gains or losses is calculated as follows:

$$Q_{total} = 1.08 \times CFM_{total} \times \Delta T_1 \quad \text{Equation 4.25}$$

where

$Q_{total}$  = Energy from ventilation and infiltration for current hour (Btu)

$CFM_{infil}$  = Infiltration in cubic feet per minute (cfm)

$CFM_{infil+unbalfan}$  = combined infiltration and unbalanced mechanical ventilation in cubic feet per minute (cfm)

$CFM_{infil+totfan}$  = infiltration plus the balanced and unbalanced mechanical ventilation in cubic feet per minute (cfm)

$MECH_{bal}$  = the balanced mechanical ventilation in cfm. This value is the smaller of the total supply fan cfm and the total exhaust fan cfm.

$MECH_{unbal}$  = the unbalanced mechanical ventilation in cfm. This value is derived from the absolute value of the difference between the total supply fan cfm and the total exhaust fan cfm.

1.08 = conversion factor in (Btu-min)/(hr-ft<sup>3</sup>-°F)

$\Delta T_1$  = difference between indoor and outdoor temperature for current hour (°F)

$\Delta T_2$  = difference between indoor and outdoor temperature for previous hour (°F)



A =	stack coefficient, (cfm <sup>2</sup> /in <sup>4</sup> / F)
B =	wind coefficient, (cfm <sup>2</sup> /in <sup>4</sup> /mph <sup>2</sup> )
V =	average wind speed for current hour (mph)
ELA=	effective leakage area (in <sup>2</sup> ), measured or calculated using Equation 4.26

The stack (A) and wind (B) coefficients to be used are shown in Table 4-9

Table 4-9 - Infiltration Coefficients

Coefficient	Floor levels		
	one	two	three
A (stack)	0.0156	0.0313	0.0471
B (wind) (Shielding Class 4)	0.0039	0.0051	0.0060

The ELA is calculated from the SLA as follows:

$$ELA = CFA \times SLA \times \left( \frac{144 \text{ in}^2}{1 \text{ ft}^2} \right) \times \left( \frac{1}{10,000} \right) \quad \text{Equation 4.26}$$

where

CFA = conditioned floor area (ft<sup>2</sup>)

SLA = specific leakage area (ft<sup>2</sup>/ft<sup>2</sup>)

ELA = effective leakage area ( in<sup>2</sup> )

Alternatively, ELA and SLA may be determined from blower door measurements:

$$ELA = 0.055 \times CFM50_H \quad \text{Equation 4.27}$$

where

CFM50<sub>H</sub> = the measured air flow in cubic feet per minute at 50 pascals for the dwelling with air distribution registers unsealed.

Substituting Equation 4.27 into Equation 4.16 gives the relationship of the measured air flow rate to SLA:



$$SLA = 3.819 \times \frac{CFM50_H}{CFA} \quad \text{Equation 4.28}$$

For compliance with the 1998 Standards, ACM users may take credit for reduced infiltration and mechanical ventilation for low-rise, single-family dwellings when verified by site diagnostic testing. For 1998 the model for infiltration has been modified to allow for reduced infiltration entries but also assumes that dwelling occupants will open windows when natural ventilation and infiltration do not provide adequate air quality. When infiltration falls below the threshold described in Equation 4.22, ACMs shall assume that occupants open windows in the next hour and add window ventilation to supplement the infiltration and cooling ventilation to achieve an effective air change rate consistent with ASHRAE Standard 62-1989 as described in Equations 4.20 and 4.21.

The Effective Leakage Area (ELA) of the dwelling may be reduced and the algorithm will result in less energy use due to infiltration unless window ventilation is needed. Lower ELAs will result in more frequent window ventilation and at some point higher energy use. Air quality ventilation may also be added and if this ventilation plus infiltration and cooling ventilation provides adequate air exchange, window ventilation will no longer occur or will occur very infrequently. The energy use of both ventilation exhaust fans and ventilation supply fans must be entered. These ventilation fans are assumed to operate continuously and the energy use of these fans must be included as energy use in the energy budget calculated for the dwelling. Except for the set 0.5 SLA reduction credits, both reduced ELA/SLA and ventilation fans are conditions which require field verification or diagnostic testing by a HERS rater and must be reported in the *HERS Required Verification* listings on the Certificate of Compliance and the Computer Method Summary forms. Controlled ventilation crawl spaces (CVC) and sunspaces are modeled using the air changes per hour method. Modeling of CVC's and sunspaces are optional capabilities covered in Sections 6.1 and 6.3, respectively. All optional capabilities that are used in the *Proposed Design* must be reported in the *Special Features and Modeling Assumptions* listings on the Certificate of Compliance and the Computer Method Summary forms.

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#### **4.18 Heating Equipment and Air Distribution Fans**

The efficiency of fossil-fuel-fired heating equipment (furnaces, boilers, etc.) is rated as an Annual Fuel Utilization Efficiency (AFUE) with the 1998 standards. The test method for calculating AFUE ignores electric energy used by air distribution fans and the contribution of the fan motor input to the heating output. The fan energy is calculated at the rate of 0.005 watt-hours per Btu of heat delivered by the equipment.

The vast majority of residential furnaces have the fan motor in the air stream so the heat generated by the motor contributes to heating the house. This effect may be considered in calculating the source energy for heating.

The heating source energy may be calculated using an effective AFUE which accounts for both the heat contribution of the fan and the source energy used by the fan. The effective AFUE is a similar number to the seasonal efficiency used in pre 1992 ACMs.



$$AFUE_{eff} = \frac{1 + 0.005(3.413)}{\frac{1}{AFUE} + 0.005(10.239)} \quad \text{Equation 4.29}$$

The effective AFUE is used for all furnaces and boilers that use ducted distribution systems.

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#### 4.19 Duct Efficiency

The Commission has approved algorithms and procedures for determining duct and HVAC distribution efficiency. Details are presented in Appendix F.

There are two calculation procedures to determine seasonal air distribution efficiency using either 1) default input assumptions or 2) diagnostic measurement values. Air distribution efficiencies for heating and cooling shall be calculated separately. The ACM shall require the user to choose values for the following parameters to calculate seasonal duct efficiencies. The ACM shall use the defaults shown in [brackets] for the *Standard Design* and for the *Proposed Design* when the user does not enter a specific value for these parameters or for all proposed designs of dwellings that are not low-rise, single-family dwellings<sup>1</sup>. The defaults must also be used for the *Proposed Design* whenever building cavities such as plenums and platform returns are used in lieu of ductwork in some parts of the HVAC air supply or return system:

1. Location of the duct system [ducts in the attic]
2. Insulation level of ducts [R 4.2]
3. The surface area of ducts or separate supply and return surface areas for diagnostic verification. [27% of conditioned floor area (CFA) for supply duct surface area; 5% CFA for return duct surface area in single story dwellings and 10% CFA for return duct surface area in dwellings with two or more stories] or the measured reduced surface area of supply ducts in conjunction with ACCA Manual D design and measured verified fan flow consistent with the ACCA Manual D design.
4. the leakage level of the duct system [22% of fan flow]. Two values are possible: the default or 6% of fan flow if measured and verified at no more than 6% of fan flow.
5. ACCA manual D design, duct layout and system fan flow [No] This requires that engineering calculations and a duct layout have been prepared as part of the building plans and that system fan flow specified in those calculations be diagnostically verified by a HERS rater.
6. Designation for systems with less than 12 feet of duct outside conditioned space [No].

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<sup>1</sup> All proposed designs except those using building cavities, such as plenums or platform returns, in lieu of ductwork may model additional insulation (R>4.2) for ducts when installed. The R-value modeled must be the minimum installed insulation level for the entire duct system except as noted in Appendix F even though part of the ducts may serve nonmodeled dwellings or spaces.



When any duct efficiency credit is claimed beyond the default assumptions that requires diagnostic testing or verification by a HERS rater or the local enforcement agency, i.e. when non-default values (except HVAC equipment capacities) are used to determine duct efficiency, the leaks in the air distribution system connections shall not be sealed with cloth back rubber adhesive duct tapes unless such tape is used in combination with mastic and drawbands and this requirement must be specified in the *Special Features and Modeling Assumptions* listings and the *HERS Required Verification* listings on the CF-1R and the C-2R.

The ACM shall automatically use the following values from the description of the *Proposed Design* when calculating the distribution system efficiency:

- Number of stories
- Building Conditioned Floor Area
- Building Volume
- Floor Type
- Presence of radiant barriers
- Presence of insulation between floor above crawlspace or unconditioned basement, and on or within crawlspace or basement walls adjacent to outside conditions or the ground below
- Outdoor summer and winter design temperatures for each climate zone

When more than one HVAC system serves the building or dwelling, the HVAC distribution efficiency is determined for each system and an conditioned floor area-weighted average seasonal efficiency is determined based on the inputs for each of the systems.

When an existing HVAC system is extended to serve an addition, the default assumptions for duct and HVAC distribution efficiency must be used for both the *Proposed Design* and the *Standard Design*. However, when a new, high efficiency HVAC distribution system is used to serve the addition or the addition and the existing building, that system may be modeled to receive energy credit subject to diagnostic testing and verification of proper installation by a HERS rater.

---

## 4.20 Absorptivity

**Standard Design:** In the *Standard Design* run, the absorptivity of all surfaces is assumed to be the same as the *Proposed Design*.

**Proposed Design:** In the *Proposed Design*, the absorptivity of walls or other surfaces adjacent to unconditioned spaces, such as crawl space floors and walls adjacent to attached garages, may be assumed to be zero, otherwise all surfaces shall be assumed to have an absorptivity of 0.50.



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## 4.21 Water Heating Calculation Method

This section describes the calculation methods to use with residential water heating systems. The equations listed here must be implemented exactly in general purpose ACMs.

---

### 4.21.1 Water Heating Energy Use

The total water heating energy use is the water heating energy use summed over all water heating systems, all water heaters, and all dwelling units being modeled.

$$WHEU_{tot} = \sum_{k=1}^M (WHEU_k \times NmbrWHtr_k) \quad \text{Equation 4.30}$$

For the *Proposed Design*, Equation 4.31 applies:

$$WHEU_{proposed} = WHEU_{tot} \times \frac{1000}{CFA_{tot}} \quad \text{Equation 4.31}$$

$$CFA_{tot} = \sum_{i=1}^N CFA_i \quad \text{Equation 4.32}$$

- WHEU<sub>tot</sub> = total water heating energy use
- WHEU<sub>k</sub> = water heating energy use for the  $k^{\text{th}}$  water heating system
- NmbrWHtr<sub>k</sub> = number of water heaters in  $k^{\text{th}}$  water heating system
- CFA<sub>i</sub> = conditioned floor area of the  $i^{\text{th}}$  dwelling unit (ft<sup>2</sup>). The CFA is limited to a maximum of 2,500 ft<sup>2</sup>
- N = Number of dwelling units.

---

### 4.21.2 Water Heating Energy Budget

The water heating energy budget (WHEB) for a water heating system or a building is determined from the following equation. The budget may be calculated for a system that serves a set of dwelling units or for the entire building. The budget for individual units in a multi-family applications may be expressed as a total, as shown in Equation 4.33.

$$WHEB = 0.00485 \times \sum_{i=1}^N CFA_i + 16.37N \quad \text{Equation 4.33}$$

Where CFA<sub>i</sub> and N are as described in Section 4.21.1

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### 4.21.3 Water Heating Systems

Water heating distribution systems may serve more than one dwelling unit and may have more than one piece of water heating equipment. The energy used by a water heating

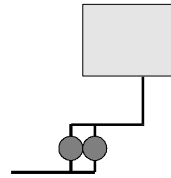


system is calculated as the sum of the energy used by each individual water heater in the system. Energy used for the whole building is calculated as the sum of the energy used by each of the water heating systems. To delineate different water heating elements several indices are used.

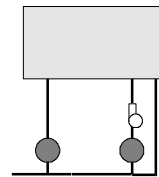
- i Used to describe an individual dwelling unit. For instance  $CFA_i$  would be the conditioned floor area of the  $i$ th dwelling unit. "N" is the total number of dwelling units.
- j Used to refer to the number of water heaters in a system. "M" is the total number of water heaters.
- k Used to refer to a water heating system or distribution system. A building can have more than one system and each system can have more than one water heater.

The following diagrams illustrate some of the cases that are recognized by the Commission water heating method.

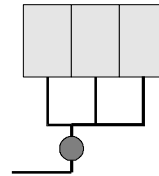
- 1 One distribution system with two water heaters serving a single dwelling unit.



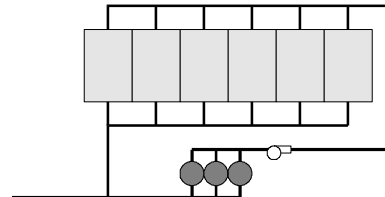
- 2 Two distribution systems, each with a single water heater serving a single dwelling unit.



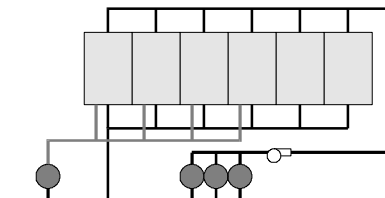
- 3 One distribution system with one water heater serving multiple dwelling units.



- 4 Single distribution system with multiple water heaters serving multiple units.



- 5 Two distribution systems, one with multiple water heaters serving multiple dwelling units. The recirculating distribution system serves all the units. The other serves only four units.





The following rules apply to the calculation of water heating system energy use:

- 1 water heater type per system
- 1 solar or woodstove credit (but not both) per system

---

#### 4.21.4 Adjusted Recovery Load (ARL)

The adjusted recovery load is calculated separately for each water heating distribution system,  $k$ . It accounts for the number of units served, the size of each unit and the type of distribution system.  $ARL_k$  is given by the following equations for the  $k$ th distribution system.

$$ARL_k = SRL_k DSM_k SSM_k \quad \text{Equation 4.34}$$

Where

$SRL_k$  = Standard water heating recovery load of the  $k$ th water heating distribution system (million Btu/yr).

$DSM_k$  = Distribution system multiplier (unitless) for the  $k$ th water heating system. A value of one is used for standard distribution systems. (See Table 4-10)

$SSM_k$  = Solar savings multiplier (unitless) for the  $k$ th water heating system. See equation below.

$$SSM_k = 1 - (SSF_k A) \quad \text{Equation 4.35}$$

$SSF_k$  = Solar savings fraction taken from an f-Chart analysis or other approved method (unitless).

$A$  = Adjustment to the  $SSF$  (unitless). This value is 0.80 to account for pumping energy and piping heat loss effects when these losses are not accounted for in the f-Chart analysis and 1.00 for passive systems (no circulation pump) and systems where pump energy and piping losses were included in the f-Chart analysis. (Piping loss effects are accounted for in the Commission Passive Solar Credit calculation procedure). Approved ACM compliance supplements shall state that pipe losses are not to be accounted for in the f-Chart analysis of active solar water heating systems.

When a water heating system has more than one water heater, the total load on the system is assumed to be shared equally by each water heater. The ARL for the  $j$ th water heater is then shown in the following equation.

$$ARL_j = \frac{ARL_k}{NmbrEquip_k} \quad \text{Equation 4.36}$$

Where

$NmbrEquip_k$  = The number of water heaters in the  $k$ th system.

##### 4.21.4.1 Standard Recovery Load



The standard water heating recovery load for the kth system is the load assuming a standard distribution system and no solar or wood stove credits. It depends on the size of the dwellings and number of units and is given in the following equation (million Btu/yr).

$$SRL_k = \sum_{i=1}^n \frac{0.0855347 \left( \frac{CFA_i}{1000} \right)^2 + 3.61307 \left( \frac{CFA_i}{1000} \right) + 6.036}{NmbrSys_i} \quad \text{Equation 4.37}$$

Where

CFA<sub>i</sub> = Conditioned floor area of the ith dwelling unit served by the water heater (ft<sup>2</sup>). The CFA is limited to a maximum of 2,500 ft<sup>2</sup> per dwelling unit.

n = Number of dwelling units served by the kth water heating system.

NmbrSys<sub>i</sub> = Number of water heating systems that serve the ith dwelling unit. When a dwelling unit is served by more than one system, the assumption is that the load is shared equally by each system.

#### 4.21.4.2 Distribution System Multiplier

The distribution system multiplier (unitless) is an adjustment for alternative water heating distribution systems. A value of one is used for standard distribution systems. Values for other systems are given in the following table

**Table 4-10 Distribution System Multipliers (DSMs)**

Distribution System	DSM - Single Family	DSM-MultiFamily
Standard	1.00	1.00
POU	0.82	1.00
HWR	0.82	1.00
Pipe Insulation	0.92	0.92
Parallel Piping	0.86	0.86
Recirc/NoControl	1.52	1.52
Recirc/Timer	1.28	1.52
Recirc/Temp	1.05	1.05
Recirc/Demand	0.98	1.52
Recirc/Time+Temp	0.96	1.52
Recirc/Demand + HWR	0.80	1.52
Recirc/Demand + Pipe Insulation	0.90	1.52



### 4.21.5 Energy Use of Individual Water Heaters

Once the adjusted recovery load is determined for each water heater, the energy use for each water heater is calculated as described below for each water heater type.

#### 4.21.5.1 Storage Gas, Storage Electric and Heat Pump Water Heaters

The energy use of storage gas, storage electric and heat pump water heaters is given by the following equation.

$$WHEU_j = \left[ \frac{ARL_j \times HPAF_j}{LDEF_j} \right] WSAF_j \quad \text{Equation 4.38}$$

Where

$WHEU_j$  = Energy use of the water heater (millions Btu/yr), adjusted for tank insulation and wood stove boilers.

$ARL_j$  = Adjusted recovery load (millions Btu/yr). Equations for this value are given in Section 4.21.4.

$SEM_j$  = Source energy multiplier (unitless). This multiplier is 3.0 for electric and heat pump water heaters and 1.0 for gas or oil water heaters.

$HPAF_j$  = Heat pump adjustment factor from the table below based on climate zone. This value is one for storage gas, storage oil and storage electric water heaters.

**Table 4-11 - Heat Pump Adjustment Factors**

Climate Zone	Heat Pump Adjustment Factor	Climate Zone	Heat Pump Adjustment Factor
1	1.040	9	0.920
2	0.990	10	0.920
3	0.990	11	0.920
4	1.070	12	1.070
5	1.070	13	0.920
6	0.920	14	1.040
7	0.920	15	0.920
8	0.920	16	1.500

$LDEF_j$  = The load dependent energy factor (LDEF) is given by the following equation. This equation adjusts the standard EF for different load conditions.

$$LDEF_j = \ln \left( \frac{ARL_j \times 1000}{365} \right) (a \times EF_j + b) + (c \times EF_j + d) \quad \text{Equation 4.39}$$

a,b,c,d = Coefficients from the table below based on the water heater type.



Table 4-12 - LDEF Coefficients

Coefficient	Storage Gas	Storage Electric	Heat Pump
a	-0.098311	-0.91263	0.44189
b	0.240182	0.94278	-0.28361
c	1.356491	4.31687	-0.71673
d	-0.872446	-3.42732	1.13480

$EF_j$  = Energy factor of the water heater (unitless). This is based on the DOE test procedure.

$WSAF_k$  = Wood stove boiler adjustment factor for the kth water heating system. This is given in Section 4.21.5.5. This is an optional capability and is set to 1.00 for ACMs without wood stove boiler modeling capability.

#### 4.21.5.2 Instantaneous Gas or Oil

The energy use for instantaneous gas or oil water heaters is given by the following equation.

$$WHEU_j = \left[ \frac{ARL_j \times SEM_j}{EF_j} + \frac{PILOT_j \times 8760}{1000000} \right] WSAF_j \quad \text{Equation 4.40}$$

Where

$ARL_j$  = Adjusted recovery load from Section 4.21.4..

$SEM_j$  = Source energy multiplier (unitless). This multiplier is 1.0 for gas or oil water heaters and can therefore be ignored.

$EF_j$  = Energy factor from the DOE test procedure (unitless). This is taken from manufacturers literature or from the CEC Appliance Database.

$PILOT_j$  = Energy consumption of the pilot light (Btu/h).

$WSAF_k$  = Wood stove boiler adjustment factor for the kth water heating system. This is given in Section 4.21.5.5. This is an optional capability and is set to 1.00 for ACMs without wood stove boiler modeling capability.

#### 4.21.5.3 Instantaneous Electric

Energy use for instantaneous electric water heaters is given by the following equation.

$$WHEU_j = \left[ \frac{ARL_j \times SEM_j}{EF_j} \right] WSAF_j \quad \text{Equation 4.41}$$

$ARL_j$  = Adjusted recovery load from Section 4.21.4.



- SEM<sub>j</sub> = Source energy multiplier (unitless). This multiplier is 3.0 for electric water heaters.
- EF<sub>j</sub> = Energy factor from DOE test procedure (unitless).
- WSAF<sub>k</sub> = Wood stove boiler adjustment factor for the kth water heating system. This is given in Section 4.21.5.5. This is an optional capability and is set to 1.00 for ACMs without wood stove boiler modeling capability.

#### 4.21.5.4 Large storage gas and Indirect Gas

Energy use for large storage gas and indirect gas water heaters is given by the following equation. Note: large storage gas water heaters are defined as any gas storage water heater with an input rate not less than 75,000 Btu/h.

$$WHEU_j = \left[ \frac{ARL_j + (JL_j)}{EFF_j \times EAF_j} + PILOT_j \left( \frac{8760}{1000000} \right) \right] WSAF_j \quad \text{Equation 4.42}$$

[SBL<sub>j</sub> has been deleted from this equation]

Where

- ARL<sub>j</sub> = Adjusted recovery load (defined later).
- JL<sub>j</sub> = Jacket loss (millions Btu/yr). Equations are given in Section 4.21.7.
- EFF<sub>j</sub> = Efficiency (fraction, not %). To be taken from CEC Appliance Database or from manufacturers literature. These products may be rated as a recovery efficiency, thermal efficiency or AFUE.
- EAF<sub>j</sub> = Efficiency adjustment factor (unitless). This value is 1.0 for large storage gas water heaters and 0.98 for indirect gas water heaters.
- PILOT<sub>j</sub> = Pilot light energy (Btu/h).
- WSAF<sub>k</sub> = Wood stove boiler adjustment factor for the kth water heating system. This is given in Section 4.21.5.5. This is an optional capability and is set to 1.00 for ACMs without wood stove boiler modeling capability.

#### 4.21.5.5 Wood Stove Adjustment Factors

This is an optional capability and the Wood Stove Boiler Adjustment Factor is set to 1.00 for ACMs without wood stove boiler modeling capability. The wood stove adjustment factor (unitless) reduces water heating energy to account for the heat contribution of wood stove boilers. This multiplier is taken from the table below, based on climate zone and whether or not the wood stove boiler has a recirculation pump. The inclusion of this factor and its relevant input parameters is an optional capability for ACMs. However, when this optional capability is implemented the algorithms and procedures given below must be used.



**Table 4- 13 - Wood Stove Adjustment Factors**

Climate Zone	Wood Stoves with Pumps	Wood Stoves without Pumps
1	0.775	0.750
2	0.775	0.750
3	0.775	0.750
4	0.865	0.850
5	0.865	0.850
6	0.910	0.900
7	0.910	0.900
8	0.955	0.950
9	0.910	0.900
10	0.955	0.950
11	0.910	0.900
12	0.865	0.850
13	0.910	0.900
14	0.910	0.900
15	1.000	1.000
16	0.730	0.700

#### 4.21.6 Tank Surface Area

Tank surface area (TSA) is used to calculate the jacket loss (JL) for large storage gas and indirect gas water heaters. TSA is given in the following equation as a function of the tank volume.

$$TSA_j = e (f VOL_j^{0.33} + g)^2 \quad \text{Equation 4.43}$$

Where

$VOL_j$  = Actual tank capacity (gallons).

e,f,g = Coefficients given in the following table.

**Table 4-14 - Coefficients for Calculating Tank Surface Areas**

Coefficient	Storage Gas	Large Storage Gas and Indirect Gas	Storage Electric and Heat Pumps
e	0.00793	0.01130	0.01010
f	15.67	11.8	11.8
g	1.9	5.0	5.0



### 4.21.7 Jacket Loss

The jacket loss for large storage gas and indirect gas water heaters

$$JL_j = \left( \frac{TSA_j(135 - 60.3)}{RTI_j + REI_j} + (FTL_j)(EFF_j)(EAF_j) \right) \left( \frac{8760}{1000000} \right) \quad \text{Equation 4.44}$$

Where

$TSA_j$  = Tank surface area (ft<sup>2</sup>).

$FTL_j$  = Fitting losses<sup>2</sup>. This is a constant 61.4 Btu/h.

$REI_j$  = R-value of exterior insulating wrap.

$$RTI_j = \left( \frac{TSA_j(135 - 60.3)}{(8.345(VOL_j)(SBL_j)(135 - 60.3) - FTL_j - PILOT_j)(EFF_j)(EAF_j)} \right) \quad \text{Equation 4.45}$$

$SBL_j$  = Standby loss expressed as a fraction of the heat content of the stored water lost per hour from the CEC Appliance Database or from manufacturer's literature.

Where  $EFF_j$  and  $EAF_j$  are efficiencies as described in *Section 4.21.5.4*

## 4.22 Slab Heat Loss (F2 Factor)

See Section 4.7.1.

## 4.23 Fenestration Products

Information concerning fenestration products, specifically the default table for fenestration U-values and the default table for fenestration SHGC values, is included in Sections 101 and 116 of Title 24, Part 6, the energy efficiency standards for buildings.

## 4.24 Radiant Barriers

**Standard Design:** The *Standard Design* does not have or use radiant barriers.

**Proposed Design:** Energy credit for radiant barriers may be used with approved 1998 alternative calculation methods (ACMs). Approved ACMs must be able to model radiant barriers. The reference method models radiant barriers by calculating ceiling U-value modifiers that are functions of the ceiling insulation and the season and by using different seasonal attic temperatures for attics with radiant barriers which result in better HVAC distribution efficiencies for ducts in the attic below a radiant barrier.

Radiant barriers must meet specific eligibility and installation criteria to be modeled by any ACM and receive energy credit for compliance with the energy efficiency standards for low-rise residential buildings.

<sup>2</sup> See Davis Energy Group report, Section III, Page A-8.



- The emissivity of the radiant barrier must be less than or equal to 0.05 as tested in accordance with ASTM Test Method C-1371-97.
- Installation must be in conformance with ASTM C-1158-90 (Standard Practice For Use and Installation Of Radiant Barrier Systems (RBS) In Building Construction.), ASTM C-727-90 (Standard Practice For Installation and Use Of Reflective Insulation In Building Constructions.), ASTM 1313-95 (Standard Specification for Sheet Radiant Barriers for Building Construction Applications), and ASTM C-1224-93 (Standard Specification for Reflective Insulation for Building Applications) and the radiant barrier must be securely installed in a permanent manner with the shiny side facing down toward the attic floor. Moreover, radiant barriers must be installed to the roof truss/rafters (top chords) in *any* of the following methods, with the material:
  1. Draped over the truss/rafter (the top chords) before the upper roof decking is installed.
  2. Spanning between the truss/rafters (top chords) and secured (stapled) to each side.
  3. Secured (stapled) to the bottom surface of the truss/rafter (top chord). A minimum air space must be maintained between the top surface of the radiant barrier and roof decking of not less than 1.5 inches at the center of the truss/rafter span.
  4. Attached [laminated] directly to the underside of the roof decking. The radiant barrier must be laminated and perforated by the manufacturer to allow moisture/vapor transfer through the roof deck.

In addition, the radiant barrier must be installed to cover all gable end walls and other vertical surfaces in the attic.

- The attic must be ventilated to:
  1. conform to manufacturer's instructions.
  2. provide a minimum free ventilation area of not less than one square foot of vent area for each 150 square feet of attic floor area.
  3. provide no less than 30 percent upper vents.
  4. have a minimum gap of 3.5 inches provided at the bottom of the radiant barrier and at the top of the ceiling insulation (except for method 4 above).
  5. have a minimum of six (6) inches (measured horizontally) left at the roof peak to allow hot air to escape from the air space between the roof decking and the top surface of the radiant barrier (except for method 4 above).

(Ridge vents or gable end vents are recommended to achieve the best performance. The material should be cut to allow for full air flow to the venting.)

- The product must meet all requirements for California certified insulation materials [radiant barriers] of the Department of Consumer Affairs, Bureau of Home Furnishings and Thermal Insulation as indicated in the *Consumer Guide and Directory of Certified Insulation Products*.



The use of a radiant barrier and the criteria specified above shall be listed in the *Special Features and Modeling Assumptions* listings of the CF-1R and C-2R and described in detail in the ACM Compliance Supplement.

For the heating season, Equation 4.46 is the expression for the U-value modifier; for the cooling season, Equation 4.47. To determine the U-value for a ceiling with a radiant barrier, multiply the U-value of the ceiling assembly without the radiant barrier times the U-value modifier. The U-value modifiers are calculated from equations 4.46 and 4.47.

For installed insulation greater than R-8:

$$UvalMod_{heating} = (-11.404 \times U^2) + (0.21737 \times U) + 0.92661 \quad \text{Equation 4.46}$$

$$UvalMod_{cooling} = (-58.511 \times U^2) + (3.22249 \times U) + 0.64768 \quad \text{Equation 4.47}$$

Otherwise these modifiers are 1.000.

---

#### 4.25 No Cooling

**Standard Design:** The *Standard Design* has a cooling system as described in Section 3.8.2. for a central ducted cooling systems the same as the *Proposed Design*.

**Proposed Design:** Where no air conditioning system is proposed for use, the *Proposed Design* is required to model a split system air conditioner with an SEER of 10.0 with R-4.2 ducts located in the attic with default duct characteristics.

---

#### 4.26 Commission Equivalent Efficiencies

The approved ACM compliance supplement must include the following conversions and substitution:

For equipment without an HSPF rating, the HSPF may be calculated as:

- $HSPF = (3.2 \times COP) - 2.4$  Equation 4.48
- The EER may be used in lieu of the SEER for equipment not required to be tested for an SEER rating.











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## 5. Minimum Capabilities Tests

This section describes the methods used to test the minimum modeling capabilities of candidate ACMs. There are three sets of tests: space conditioning tests, water heating tests and standard design generator tests. The space conditioning tests are performed using a simple square building prototype. The water heating tests are performed relative to several prototype water heating systems. The standard design generator tests use a single prototype building designed to have a wide variety of features. Most of the tests are performed in only five climate zones, but some require consideration in all sixteen climate zones.

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### 5.1 *Prototype Buildings*

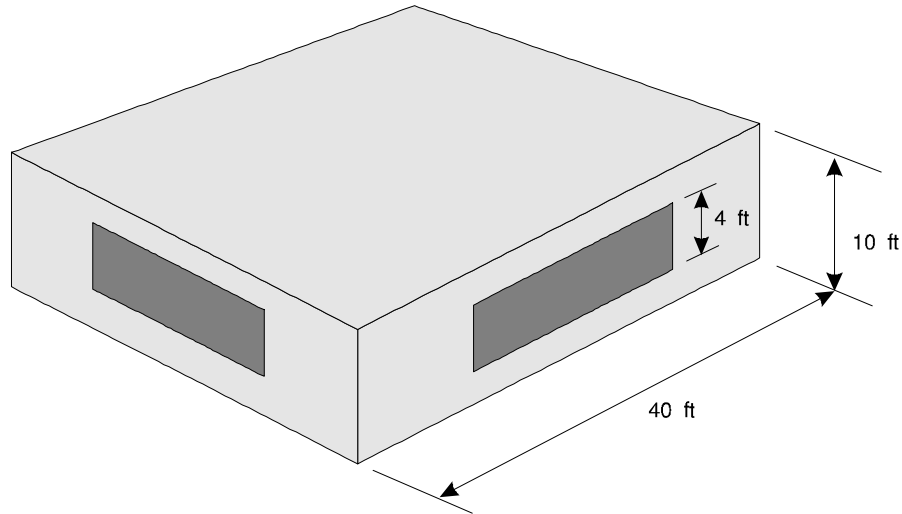
The prototype buildings are illustrated below and described in the following paragraphs. Each is presented in much greater detail on diskettes available from the California Energy Commission<sup>1</sup>. Letter designations are used for the prototype buildings. The letter is used as part of the label for each computer run.

- A This prototype is a square box used for most of the space conditioning tests.
- B The second prototype building is identical to the first except that it has raised floor construction, instead of a slab-on-grade.
- C This prototype is a 3,534 ft<sup>2</sup>, one and two-story, single-family detached custom home.

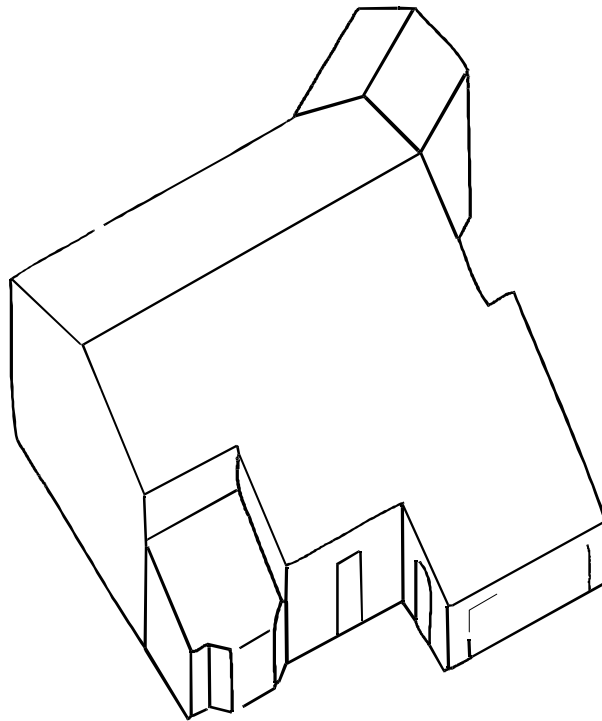
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<sup>1</sup> Write to ACM TEST FILES, California Energy Commission, 1516 Ninth St., MS#25, Sacramento, CA 95814-5512 to obtain copies of these input files on 3.5 inch, 1.44 Mbyte diskettes.





**Figure 5-1 - Prototype Buildings A and B**



**Figure 5-2 - Prototype C**

Prototype buildings A and B have the same conservation features in all climate zones (see Table 5-1 below). The specific values associated with each of the basecase conservation measures is also summarized in the CALRES98 input files available from the Commission (see footnote 1 for this Chapter).



Table 5-1 - Basecase Conditions for Prototypes A and B

Component	Basecase Level	Notes
Roof U-value	0.034	
Wall U-value	0.088	
Floor U-value	0.037	
Slab F2 factor	0.76	4
Door U-value	0.330	
Thermal Mass	Slab 20% exposed, 80% covered	3
SHGC (exterior device) - (bugscreen)	0.76	
SHGC (interior)	0.68	
SHGC (fenestration - includes framing)	0.70	
Window type	Sliders	5
Fenestration U-Value	0.75	
Gas furnace AFUE	0.78	1
Air conditioner SEER	10.0	
HVAC ducts	R-4.2 Ducts in Attic	2
SLA	4.9	6

## Notes:

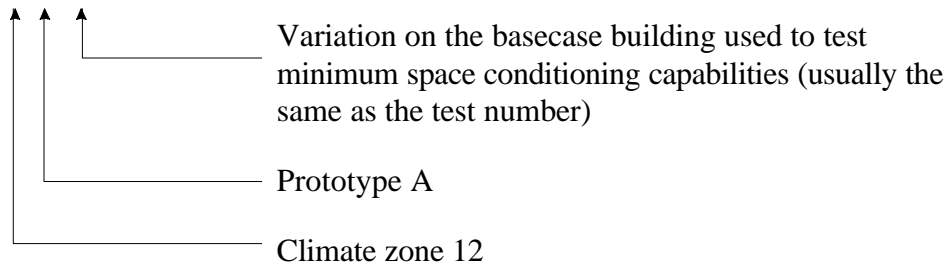
- 1 The AFUE(eff) is 0.7629 when the heat contribution and energy use of the fan is considered.
- 2 Duct efficiencies are as described for the standard design in Chapter 3 using the default values for an air conditioner with 36,000 Btu/hr cooling capacity.
- 3 Prototype B has thermal mass equivalent to 5% of the raised floor area in 2 inch thick exposed concrete per Section 3.6..
- 4 Assumes 80% of the slab at building perimeter is carpeted or covered.
- 5 The default natural ventilation assumptions are used. 10% of the window area is operable (half of this is inlet and half is outlet). Height difference between inlet and outlet is 2 feet.
- 6 Based on having ducts in unconditioned attic space.

The computer runs used to generate the ACM tests are based on the standard modeling assumptions described in Chapter 4. Copies of these computer runs are available to assist candidate ACMs in setting their programs up for CEC approval. These input files may be obtained by writing the Residential Buildings Office, California Energy Commission, 1516 Ninth Street (MS-25), Sacramento, California 95814.

## 5.2 Labeling Computer Runs

Each computer run used to test the minimum space conditioning capabilities is given a precise designation to make it easier to keep track of the runs and to facilitate analysis. The following scheme is used:



**12 A 04****5.2.1 Basecase Runs**

The first series of runs establish the basecase against which the other runs are compared. The variation number for the basecase run is "00". The basecase energy use is calculated for prototype A in all sixteen climate zones. The energy usage for the other prototypes is calculated only for climate zones 3, 9, 12, 14 and 16. It is important to note that only two input files are required for these computer runs since measures do not change from climate zone to climate zone. The label for these tests are shown in the table below. Total of 21 Runs.

**Table 5-2 - Basecase Run Labels**

Climate Zone	Building Prototype	
	A	B
1	01A00	—
2	02A00	—
3	03A00	03B00
4	04A00	—
5	05A00	—
6	06A00	—
7	07A00	—
8	08A00	—
9	09A00	09B00
10	10A00	—
11	11A00	—
12	12A00	12B00
13	13A00	—
14	14A00	14B00
15	15A00	—
16	16A00	00B16



### 5.2.2 Test One

The purpose of the first test is to check the prediction of the ACM for relative heating and cooling loads. The heating efficiency is increased and the cooling equipment efficiency is decreased. When the changes in heating and cooling efficiency are made, additional energy use must result. *Total of 19 Runs.*

**Table 5-3 - Test One Inputs**

Run Label	New Heating Efficiency	New Cooling Efficiency
02A01	0.85	8.0
03A01	0.85	5.5
04A01	0.85	7.0
05A01	0.85	5.5
06A01	0.95	6.5
07A01	0.95	7.0
08A01	0.95	7.5
09A01	0.95	8.0
10A01	0.95	8.5
11A01	0.95	8.1
12A01	0.95	7.8
13A01	0.95	8.8
14A01	0.95	8.4
16A01	0.85	5.5
03B01	0.85	6.0
09B01	0.95	8.8
12B01	0.95	7.5
14B01	0.95	8.2
16B01	0.85	5.8

### 5.2.3 Test Two

Test two is similar to test one except that the cooling efficiency is increased and the heating efficiency is decreased, just the opposite of test one. When the changes in heating and cooling efficiency are made, additional energy use must result. *Total of 19 Runs.*



**Table 5-4 - Test Two Inputs**

Run Label	New Heating Efficiency	New Cooling Efficiency
02A02	0.65	12.5
03A02	0.72	12.5
04A02	0.66	12.5
05A02	0.65	12.5
06A02	0.55	12.5
07A02	0.50	12.5
08A02	0.49	12.5
09A02	0.45	12.5
10A02	0.45	12.5
11A02	0.63	12.5
12A02	0.62	12.5
13A02	0.52	12.5
14A02	0.57	12.5
16A02	0.75	12.5
03B02	0.70	12.5
09B02	0.46	12.5
12B02	0.61	12.5
14B02	0.59	12.5
16B02	0.74	12.5

### 5.2.4 Test Three

Test three is performed only for prototype A in five climate zones, 3, 9, 12, 14 and 16. The ceiling U-value is reduced to 0.023 from the basecase of 0.033. The south glass area is increased a specific amount for each climate zone. Each of these computer runs must result in greater energy use than the prototype A basecase. *Total of five runs.*

**Table 5-5 - Test Three Inputs**

Run Label	Roof U-value	South Glass Area
03A03	0.023	200
09A03	0.023	120
12A03	0.023	140
14A03	0.023	160
16A03	0.023	160



### 5.2.5 Test Four

Test four is performed only for prototype A in five climate zones, 3, 9, 12, 14 and 16. The wall U-value is reduced to 0.060 from the basecase of 0.088. The west glass area is increased a specific amount for each climate zone. Each of these computer runs must result in greater energy use than prototype A. *Total of five runs.*

**Table 5-6 - Test Four Inputs**

Run Label	Wall U-value	West Glass Area
03A04	0.060	170
09A04	0.060	130
12A04	0.060	119
14A04	0.060	121
16A04	0.060	150

### 5.2.6 Test Five

Test five is performed only for prototype A in five climate zones, 3, 9, 12, 14 and 16. R-7 slab edge insulation is added, i.e. an F2 factor of 0.65 is used instead of the 0.76 used in the basecase. The north glass area is increased a specific amount for each climate zone. Each of these computer runs must result in greater energy use than prototype A. *Total of five runs.*

**Table 5-7 - Test Five Inputs**

Run Label	F2 Factor	North Glass Area
03A05	0.51	220.5
09A05	0.51	150
12A05	0.51	170
14A05	0.51	160
16A05	0.51	180

### 5.2.7 Test Six

Test six is performed only for prototype A in four climate zones: 9, 12, 14 and 16. The glazing U-value is changed to 0.54 instead of the 0.75 used in the basecase. The north glass area is increased a specific amount for each climate zone. Each of these computer runs must result in greater energy use than prototype A. *Total of four runs.*



**Table 5-8 - Test Six Inputs**

Run Label	Glazing U-value	North Glass Area
09A06	0.54	192
12A06	0.54	286
14A06	0.54	269
16A06	0.54	300

### 5.2.8 Test Seven

Test seven is performed only for prototype A in five climate zones: 3, 9, 12, 14 and 16. The fenestration U-value is increased to 1.28 (single glass) from the basecase 0.75 (mild climate zone standard). The solar heat gain coefficients for the window are also changed to account for the single glass ( $SHGC_{fen} = 0.80$ ). The glass area is reduced uniformly on all orientations. Ventilation area also varies with glass area, remaining at 10% of the total area. Each of these computer runs must result in greater energy use than prototype A.

*Total of five runs*

**Table 5-9 - Test Seven Inputs**

Run Label	Glass U-value	SHGC <sub>fen</sub>	Glass Area on Each Orientation
03A07	1.28	0.80	55
09A07	1.28	0.80	71
12A07	1.28	0.80	65
14A07	1.28	0.80	63
16A07	1.28	0.80	51

### 5.2.9 Test Eight

Test eight is performed only for prototype A in five climate zones: 3, 9, 12, 14 and 16. The percent of the slab-on grade that is exposed thermal mass is increased: 500 ft<sup>2</sup> is exposed and 1100 ft<sup>2</sup> is carpeted. The slab edge heat loss, however, is unaffected; the F2 factor remains at 0.76. The south glass area is increased a specific amount for each climate zone. Each of these computer runs must result in greater energy use than prototype A. *Total of five runs.*



**Table 5-10 - Test Eight Inputs**

Run Label	Exposed Mass	South Glass Area
03A08	31.25%	195
09A08	31.25%	128
12A08	31.25%	131
14A08	31.25%	160
16A08	31.25%	128

### 5.2.10 Test Nine

Test nine is identical to test eight except west glass area is increased. This test is performed only for prototype A in five climate zones: 3, 9, 12, 14, and 16. Each of these computer runs must result in greater energy use than prototype A. *Total of five runs.*

**Table 5-11 - Test Nine Results**

Run Label	Exposed Mass	West Glass Area
03A09	31.25%	158
09A09	31.25%	131
12A09	31.25%	118
14A09	31.25%	113
16A09	31.25%	128

### 5.2.11 Test Ten

Test ten is identical to test eight except north glass area is increased. This test is performed only for prototype A in five climate zones: 3, 9, 12, 14 and 16. Each of these computer runs must result in greater energy use than prototype A. *Total of five runs.*

**Table 5-12 - Test Ten Results**

Run Label	Exposed Mass	North Glass Area
03A10	31.25%	152
09A10	31.25%	199
12A10	31.25%	141
14A10	31.25%	126
16A10	31.25%	112

### 5.2.12 Test Eleven

Test eleven is identical to test eight except east glass area is increased. This test is performed only for prototype A in five climate zones: 3, 9, 12, 14 and 16. Each of these computer runs must result in greater energy use than the prototype A basecase. *Total of five runs.*



Table 5-13 - Test Eleven Results

Run Label	Exposed Mass	East Glass Area
03A11	31.25%	184
09A11	31.25%	150
12A11	31.25%	127
14A11	31.25%	117
16A11	31.25%	119



### 5.2.13 Test Twelve

Test twelve is performed only for prototype A in five climate zones, 3, 9, 12, 14 and 16. The floor is changed from a slab-on-grade floor to a raised wooden floor over a crawl space with an overall U-value of 0.037. Exterior shading devices are used in other climate zones 9, 12 and 14 on all windows, to achieve the  $SHGC_{fen}$  values indicated below. Glass area on the west facade is increased a specific amount for each climate zone. Each of these computer runs must result in greater energy use than prototype A. *Total of five runs.*

**Table 5-14 - Test Twelve Inputs**

Run Label	Raised Floor - U-value	$SHGC_{fen}$	West Glass Area
03A12	0.037	0.80	64
09A12	0.037	0.40	180
12A12	0.037	0.40	125
14A12	0.037	0.40	140
16A12	0.037	0.80	120

### 5.2.14 Test Thirteen

In test thirteen, an interior shading device is used on all windows which has a solar heat gain coefficient of 0.47 when the device is used with single pane, metal-framed fenestration ( $SHGC_{fen} = 0.80$ ) and is closed. The area of south glass is increased a specific amount for each climate zone. This test is performed for the prototype A building in five climates. Each of these computer runs must result in greater energy use than the prototype A basecase. *Total of five runs.*

**Table 5-15 - Test Thirteen Inputs**

Run Label	SHGC Interior Shade	South Glass Area
03A13	0.47	200
09A13	0.47	200
12A13	0.47	222
14A13	0.47	244
16A13	0.47	160

### 5.2.15 Test Fourteen

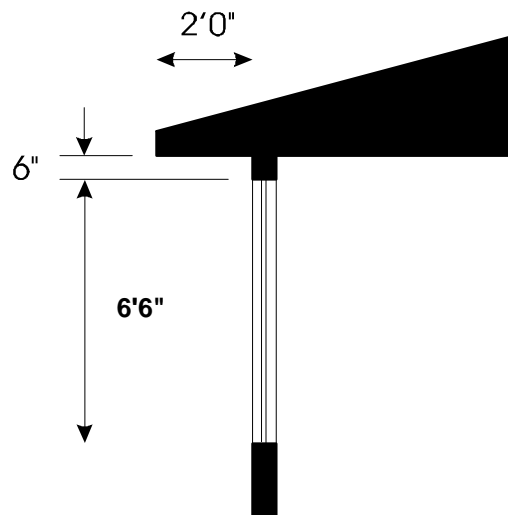
Test fourteen evaluates how the ACM treats south overhangs. It is performed for the prototype A building in five climate zones: 3, 9, 12, 14 and 16. In each case a south overhang is added to the building. The overhang has a two foot projection from the surface of the south glass. Its bottom edge is located six inches above the top of the window. It is assumed that the south glazing consists of six-foot six-inch high windows.



The overhang is assumed to extend an infinite distance beyond the sides of the windows. The overhang characteristics are illustrated below. South glazing area is then increased by increasing its width. Each case must result in greater energy use than prototype A. *Total of five runs.*

**Table 5-16 - Test Fourteen Inputs**

Run Label	South Overhang	South Glass Area
03A14	yes	169
09A14	yes	132
12A14	yes	144
14A14	yes	129
16A14	yes	100



**Figure 5-3 - Overhang Characteristics**

### 5.2.16 Test Fifteen

This test is for the infiltration and ventilation model. It is performed for the prototype A building in five climate zones: 3, 9, 12, 14 and 16. The basecase building has ducts in unconditioned space, therefore, the fixed and restricted inputs specify a SLA of 4.9. In this test building leakage is reduced to an SLA of 2.9 by infiltration reduction measures and is modeled with and without 80 cfm (0.375 air changes per hour) of mechanical ventilation which consumes 20 watts of power continuously. Glass area is increased on all orientations so that the building fails to comply. *Total of ten runs.*



**Table 5-17 - Test Fifteen Inputs**

Run Label	Specific Leakage Area	Fan Volume & Wattage	Maximum Glass Area on Each Orientation A/B
03A15A	2.90	0 cfm/0 watts	110
03A15B	2.90	80 cfm/20 watts	131
09A15A	2.90	0 cfm/0 watts	96
09A15B	2.90	80 cfm/20 watts	100
12A15A	2.90	0 cfm/0 watts	80
12A15B	2.90	80 cfm/20 watts	100
14A15A	2.90	0 cfm/0 watts	80
14A15B	2.90	80 cfm/20 watts	100
16A15A	2.90	0 cfm/0 watts	72
16A15B	2.90	80 cfm/20 watts	100



### 5.3 Water Heating Tests

Testing of ACM minimum capabilities for water heating is completely separate from the space conditioning tests. One of the principal differences between water heating and space conditioning is that fixed energy budgets are used for water heating rather than custom budgets. The testing procedures are, therefore, fundamentally different. Candidate ACMs must exactly replicate the results of the official CEC water heating methodology for various system types.

#### 5.3.1 Prototype Water Heaters

There are seven water heaters that are used for the tests. These systems are labeled E, F, G, and J. Detailed specifications for each water heating system are given in Table 5-18 below. The energy use of each of the water heating systems is calculated with several distribution systems.

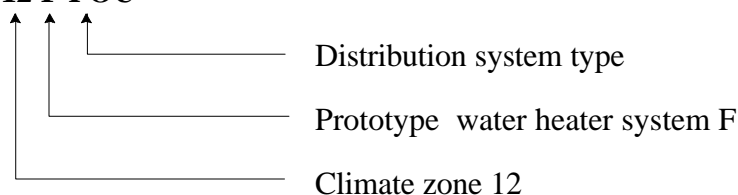
**Table 5-18 - Water Heating Systems**

		E	F	G	J
<b>System Level Information</b>					
Climate Zone		3	7	16	5
Dwelling Units		10	1	1	3
Average Dwelling Unit Size		1200	1500	3500	800
Number of Water Heaters		5	1	2	6
<b>Water Heating Equipment</b>					
Water Heater Type		LG	HP	HP	IE
Energy Factor (Note 1)		0.77	2.00	1.80	0.95
Tank Size	Gal	100	50	75	na.
Standby Loss	%	3%.	n.a.	n.a.	n.a.
Input Rating	kBtu/h	100	n.a.	n.a.	n.a.
<b>Notes</b>					
1. For instantaneous gas (IG) and large gas (LG) water heaters the value reported in this row is the recovery efficiency or thermal efficiency.					

#### 5.3.2 Labeling Computer Runs

Each water heating calculation is given a precise designation to make it easier to keep track of the runs and to facilitate analysis. The following scheme is used:



**12 F POU****5.3.3 Test Results**

Water heater types E, F, G, and J are analyzed in just one climate zone (except for heat pumps, the results should not change by climate zone). The results must exactly replicate the values shown in the following tables. A summary sheet is provided in Appendix A that must be completed by the vendor. *Total of 40 calculations.*

**Table 5-19 - Water Heater Results (kBtu/yr)**

			<b>E</b>	<b>F</b>	<b>G</b>	<b>J</b>
Energy Budget			221.900	23.645	28.495	60.750
Distribution System	DSM Single Fam.	DSM MultiFam.				
Standard	1.00	1.00	218.208	18.064	49.731	85.085
POU/HWR	0.82	1.00	218.208	15.875	43.940	85.085
Pipe Insulation	0.92	0.92	207.304	17.100	47.178	78.278
Recirc/NoControl	1.52	1.52	289.082	24.060	65.630	129.329
Recirc/Timer	1.28	1.52	289.082	21.345	58.427	129.329
Recirc/Demand	0.98	1.52	289.082	17.824	49.096	129.329
Recirc/Time+Temp	0.96	1.52	289.082	17.583	48.459	129.329
Recirc/Temp	1.05	1.05	225.023	18.660	51.310	89.339
Parallel Piping	0.86	0.86	199.126	16.367	45.242	73.123



### 5.4 Standard Design Generator Tests

The standard design generator must automatically define the standard design which is the basis of the custom budget. The standard design run is made automatically at the same time as the proposed design run, and the results are reported together on the Computer Method Summary discussed in Chapter 2. This test verifies that the standard design is correctly defined for the proposed design and that the custom budget is correctly calculated.

The standard design test consists of matched pairs of computer runs: a proposed design and its standard design equivalent. The standard design equivalent is the proposed design reconfigured according to the standard design rules in Chapter 3.

Two Computer Method Summaries are produced: one for the proposed design and one for the standard design equivalent. The standard design energy budget on the proposed design Computer Method Summary must be equal to the energy use shown in both the standard design energy budget and proposed design columns of the standard design equivalent computer run.

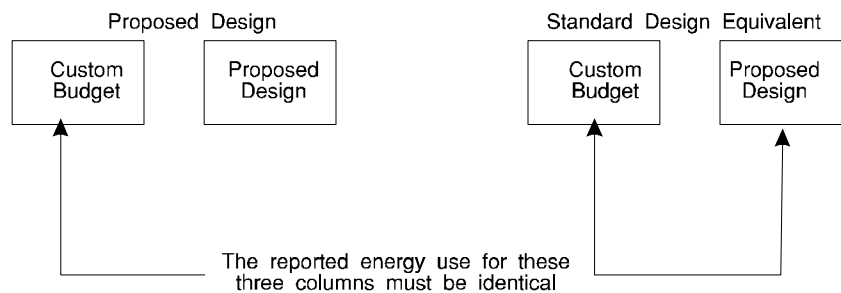


Figure 5-4 - Custom Budget Tests

#### 5.4.1 Slab Floor Test

The purpose of this test is to verify that the standard design generator correctly defines the standard design for proposed designs using slab-on-grade designs. Package D is now the basis of the standard design for all buildings including slab-on-grade buildings. The rules for determining how much thermal mass is modeled in buildings with both raised and slab-on-grade construction are contained in Chapters 3 and 4. The prototype C variation used for this test has both raised floors and slab-on-grade floors.

Prototype "xxC31" is run in all sixteen climate zones, and the standard design equivalent in each climate zone is also run. The results must be exactly identical as discussed above. The labels for this series of runs are summarized in the following table.  
*Total of 32 runs.*



**Table 5-20 - Slab Floor Standard Design Tests**

Climate Zone	Proposed Design	Standard Design Equivalent
1	01C31	01C31C
2	02C31	02C31C
3	03C31	03C31C
4	04C31	04C31C
5	05C31	05C31C
6	06C31	06C31C
7	07C31	07C31C
8	08C31	08C31C
9	09C31	09C31C
10	10C31	10C31C
11	11C31	11C31C
12	12C31	12C31C
13	13C31	13C31C
14	14C31	14C31C
15	15C31	15C31C
16	16C31	16C31C

#### 5.4.2 Raised Floor Test

The purpose of this test is to verify that the standard design generator correctly defines the standard design for a proposed design for a dwelling with a raised floor. This is a parallel test to the previous one except that a modification of the prototype building is used which is the prototype C building with no slab floor but with 5% of the nonslab floor covered with 2 inches of exposed concrete. This modification is labeled "xxC32" and is contained in Appendix C in the standard format of the Computer Method Summary.

The modified prototype C building is run in all sixteen climate zones, and the standard design equivalent in each climate zone is also run. The results must be exactly identical. The labels for this series of runs are summarized in the following table. *Total of 32 runs.*



**Table 5-21 - Raised Floor Standard Design Tests**

Climate Zone	Proposed Design	Standard Design Equivalent
1	01C32	01C32C
2	02C32	02C32C
3	03C32	03C32C
4	04C32	04C32C
5	05C32	05C32C
6	06C32	06C32C
7	07C32	07C32C
8	08C32	08C32C
9	09C32	09C32C
10	10C32	10C32C
11	11C32	11C32C
12	12C32	12C32C
13	13C32	13C32C
14	14C32	14C32C
15	15C32	15C32C
16	16C32	16C32C



### 5.4.3 Electric Heat Test

The purpose of this test is to verify that the standard design generator correctly defines the standard design for proposed designs with electric heating systems. This a parallel test to the previous custom budget tests, except that a modification of the prototype building is used. This modification is labeled "xxC33" and is contained in Appendix C in the standard format of the Computer Method Summary.

The modified prototype C building with electric resistance heating is run in all sixteen climate zones, and the standard design equivalent which uses an electric heat pump with an HSPF of 6.8 in each climate zone is also run. The results for the *Standard Designs* for both runs and the *Proposed Design* for the *Standard Design* equivalent must be exactly identical. The labels for this series of runs are summarized in the following table. *Total of 32 runs.*

**Table 5-22 - Electric Heat Standard Design Tests**

Climate Zone	Proposed Design	Standard Design Equivalent
1	01C33	01C33C
2	02C33	02C33C
3	03C33	03C33C
4	04C33	04C33C
5	05C33	05C33C
6	06C33	06C33C
7	07C33	07C33C
8	08C33	08C33C
9	09C33	09C33C
10	10C33	10C33C
11	11C33	11C33C
12	12C33	12C33C
13	13C33	13C33C
14	14C33	14C33C
15	15C33	15C33C
16	16C33	16C33C



#### 5.4.4 HVAC Distribution Efficiency Tests

The Standard Design uses the defaults of the HVAC distribution efficiency calculation method found in Appendix F to determine the HVAC distribution efficiency. These defaults result in seasonal HVAC distribution efficiencies of about 72-76% depending on the climate zone. The calculation method detailed in Appendix F gives efficiency credits for certain specific improvements in the HVAC distribution system, such as, higher duct insulation levels, careful duct design and layout, and reduced duct leakage due to better sealing techniques. HVAC distribution efficiency improvements must be independently verified and some are subject to site diagnostic testing by a certified HERS rater.

For these tests prototype building A is used. For the first series of tests, the ducts are designed to conform to ACCA Manual D specifications with room-by-room load calculations and have a duct layout design on the plans. The ducts are sealed and are modeled with total duct leakage of less than 6%. Roof insulation is reduced until the building fails to comply.

**Table 5-23 - Additions Tests Inputs**

Run Label	ACCA Manual D Design	Measured Reduced Duct Leakage	Maximum Roof /Ceiling U-value
03A34	Yes	<6%	0.073
09A34	Yes	<6%	0.082
12A34	Yes	<6%	0.066
14A34	Yes	<6%	0.094
16A34	Yes	<6%	0.066
03A35	No	<6%	0.052
09A35	No	<6%	0.043
12A35	No	<6%	0.043
14A35	No	<6%	0.043
16A35	No	<6%	0.040

For the second series of tests, duct location is run for six tests with 10 lineal feet of ducts and the air handler are in an unconditioned garage and the remainder of the ducts are in conditioned space. The tests are rerun with all of the ducts and the air handler in the conditioned space. For all of the tests in this series, duct leakage is reduced to less than 6% of the fan flow. Roof insulation is reduced until the building fails to comply



**Table 5-24 - Additions Tests Inputs**

Run Label	Duct Location	Measured Reduced Duct Leakage	Maximum Roof /Ceiling U-value
03A36	Cond./InEx12	<6%	0.094
09A36	Cond./InEx12	<6%	0.082
12A36	Cond./InEx12	<6%	0.094
14A36	Cond./InEx12	<6%	0.118
16A36	Cond./InEx12	<6%	0.127

The ACM or its research version must report the duct efficiencies for the HVAC distribution efficiency tests.

#### **5.4.5 Addition Plus Existing Building Test**

Additions are treated as new buildings except that internal heat gains are allocated on a fractional dwelling unit basis. When an addition is modeled in conjunction with an existing building, energy credit may be taken for improvements to the existing building. This series of tests exercises the various default assumptions based on the vintage of the existing building and the various reporting requirements for modeling an addition with an existing building. In addition, these tests verify the proper determination of the energy budget and compliance criteria for an addition with an improved existing building.

For these tests the existing building has the same physical configuration as Prototype A but has single pane, metal-framed windows on all four sides with a window on each vertical elevation that is 4' high and 20' wide centered on the facade. The 12' deep by 40' long addition covers the whole west side of the existing building. The addition faces west and has west-facing glazing with a U-value of 0.75 and an SHGC<sub>fen</sub> of 0.70. The addition covers 80 ft<sup>2</sup> of existing glass. For test series 37, the mandatory minimum R-values are used in the addition's roof/ceiling and walls. Hence for test series 37, the U-value for the roof/ceiling of the addition is 0.047 corresponding to R-19 insulation and the wall U-value is 0.088 corresponding to R-13 wall insulation. For test series 38, the existing building's roof and the addition roof insulation is brought up to the requirements for a new dwelling. The addition's west-facing glazing is increased until the building no longer complies with the budget determined from modeling the existing building and modeling the addition and area weighting the heating and cooling budgets for those runs.

These tests will also be used to confirm that output requirements are met when modeling an addition with an existing building and that the appropriate budgets have been correctly determined.



Table 5-25 - Additions Tests Inputs

Run Label	Vintage of Existing Building	SHGC <sub>fen</sub>	Covered Existing Glazing	U-Value of Roof/Ceiling Existing/Add.	West-Facing Glazing for the Addition (ft <sup>2</sup> )
03D37	1977	0.70	80 ft <sup>2</sup>	0.077/0.047	380
09D37	1977	0.70	80 ft <sup>2</sup>	0.077/0.047	270
12D37	1977	0.70	80 ft <sup>2</sup>	0.077/0.047	320.
14D37	1977	0.70	80 ft <sup>2</sup>	0.077/0.047	360
16D37	1977	0.70	80 ft <sup>2</sup>	0.077/0.047	370
03D38	1989	0.70	80 ft <sup>2</sup>	0.034/0.034	20
09D38	1989	0.70	80 ft <sup>2</sup>	0.034/0.0-34	100
12D38	1989	0.70	80 ft <sup>2</sup>	0.034/0.034	80
14D38	1989	0.70	80 ft <sup>2</sup>	0.028/0.028	80
16D38	1989	0.70	80 ft <sup>2</sup>	0.028/0.028	8







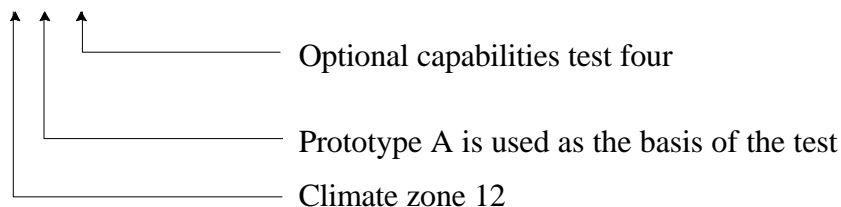
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## 6. Optional Capabilities Tests

This section of the Manual explains the tests that must be performed in order for residential ACMs to be approved for optional capabilities. Most of the tests are performed relative to one of the prototype buildings identified in the previous section. Each computer run used to test the minimum space conditioning capabilities is given a precise designation to make it easier to keep track of the runs and to facilitate analysis. Optional capabilities tests begin with the test number "51". The following scheme is used:

### 12 E 51



### 6.1 Controlled Ventilation Crawl Spaces (CVC)

Controlled ventilation crawl spaces is an optional capability based on the ability of an ACM to model more than one thermal zone. The crawl space of the building is modeled as a separate, unconditioned thermal zone. Details of the test model are provided in Appendix C, test file 12B51. Some key features are summarized below.

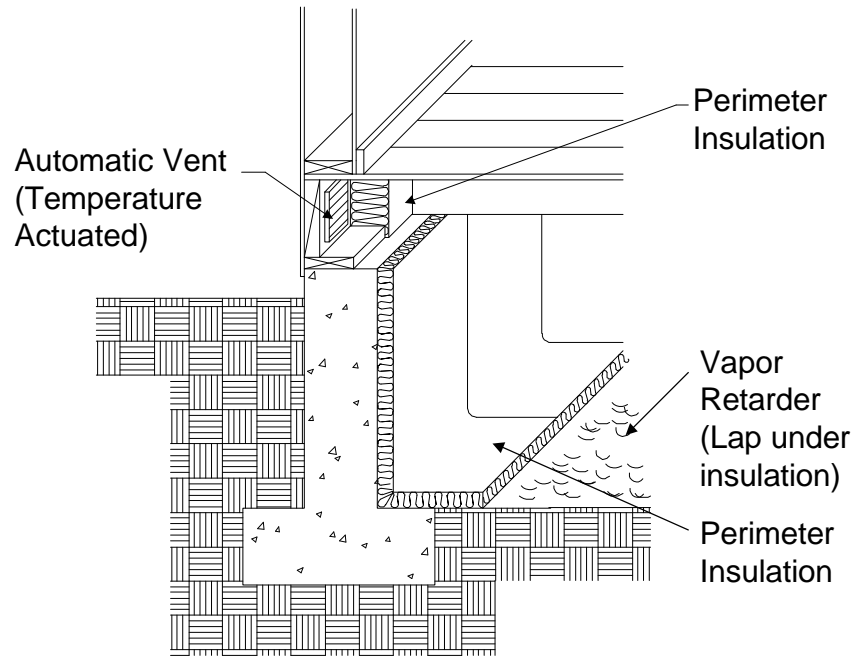
The CVC zone has an exterior perimeter length and floor area (i.e., the ground area) equal to the prototype building B perimeter and floor area. Crawlspace volume is 3467 ft<sup>3</sup>. CVC infiltration is modeled using the air changes per hour method and uses 0.22 air changes per hour.

The floor separating the crawl space from conditioned space becomes an interzone boundary. 400 ft<sup>2</sup> of this floor has a U-value of 0.342, representing an uninsulated, uncarpeted floor, and the remainder has a U-value of 0.199, representing an uninsulated, carpeted floor.

Insulation is placed in the perimeter walls of the crawl space, and the crawl space vents are modeled with automatic seasonally operated louvers to minimize ambient conditions within the crawl space. When the building is in a heating mode, the vents are closed (inlet and outlet are zero). When the building is in a cooling mode, the vents are open and the total vent area is 1/150 of the crawlspace floor area or 10.67 ft<sup>2</sup>. Half of this is inlet and half outlet. The ventilation height difference is zero. Only wind effects apply. Wind speed is reduced to 25% of that on the weather tape to account for ground level conditions. Heat capacity in the crawlspace is 1.4 Btu/F-ft<sup>2</sup>.

When insulation is placed in the perimeter walls of the crawl space in lieu of the floor assembly, other requirements are triggered for builders. The definition of "controlled ventilation crawlspace", in the glossary of the *Residential Manual*, should be consulted for more details.





**Figure 6-1 - Section at Crawlspace Perimeter**

CVC is tested only for prototype building B in five climate zones: 3, 9, 12, 14 and 16. CVC is added and the heating efficiency is modified accordingly. Each computer run must result in greater energy use than the prototype B basecase building. The computer runs are summarized below. *Total of five runs.*

**Table 6-1 - Controlled Ventilation Crawlspace Test Inputs**

Run Label	CVC	Heating AFUE
03B51	yes	0.63
09B51	yes	0.43
12B51	yes	0.64
14B51	yes	0.69
16B51	yes	0.74

The optional capability test also requires that the vendor demonstrate that the ACM correctly defines the standard design building and calculates the custom budget. This test involves running the standard design equivalent building for climate zone 12 and showing that the custom budget figures from computer run "12B51" are equal. The standard design equivalent building is included in Appendix C and labeled "12B51C".

## 6.2 Zonal Control

Zonal control is one of the optional capabilities based on the ability of an ACM to model more than one thermal zone at the same time. With zonal control, the sleeping and living



areas are modeled separately, each with its own separate thermostat schedule and internal gain assumptions. The specifications for the building with zonal control are detailed in CALRES98 input test file 12A52 available from the Commission on diskette. Further discussion is provided in the Residential Manual, in Section 8.9, and in the glossary under "zonal control". Key features are discussed below.

---

### 6.2.1 Prototype Zones

Figure 2 depicts the prototype building separated into living and sleeping zones. The boundary between the zones consists of a wall with U-value of 0.29 and net area of 360 square feet. The wall contains an uncloseable opening of 40 square feet, modeled with a U-value of 20.0.

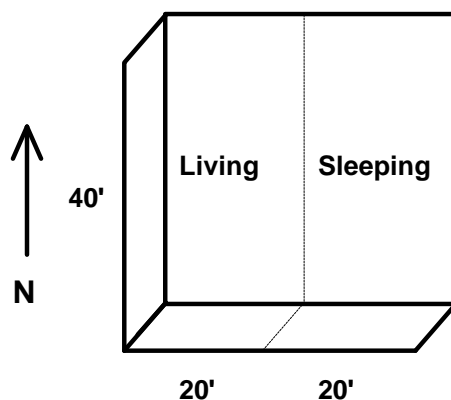


Figure 6-2 - Zoning the Prototype Building

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### 6.2.2 Thermostats

The thermostat schedule for the living area is the same as the standard assumptions except that the cooling setpoint is 83°F between 11:00 pm and 7:00 am.

The thermostat schedule for the sleeping area has two heating setback periods: between 11:00 pm and 7:00 am and between 8:00 am and 9:00 pm. The cooling thermostat has one setup period to 83°F, between 8:00 am and 9:00 pm. The thermostat schedules for zonal control are shown in Table 6-2 below.



Table 6-2 - Zonal Control Thermostat Set Points

Hour	Heating	Cooling	Hour	Heating	Cooling	Hour	Heating	Cooling
Living Areas								
1	60	83	9	68	78	17	68	78
2	60	83	10	68	78	18	68	78
3	60	83	11	68	78	19	68	78
4	60	83	12	68	78	20	68	78
5	60	83	13	68	78	21	68	78
6	60	83	14	68	78	22	68	78
7	60	83	15	68	78	23	68	78
8	68	78	16	68	78	24	60	83
Sleeping Areas								
1	60	78	9	60	83	17	60	83
2	60	78	10	60	83	18	60	83
3	60	78	11	60	83	19	60	83
4	60	78	12	60	83	20	60	83
5	60	78	13	60	83	21	60	83
6	60	78	14	60	83	22	68	78
7	60	78	15	60	83	23	68	78
8	68	83	16	60	83	24	60	78

### 6.2.3 Internal Gains

Total internal gains are split between the living areas and the sleeping areas as indicated in the following equations.

Equation 6-1

$$\text{Int-Gain}_{\text{living}} = (20,000) + (15 \times \text{CFA}_{\text{living}})$$

Equation 6-2

$$\text{Int-Gain}_{\text{sleeping}} = 15 \times \text{CFA}_{\text{sleeping}}$$

An alternate set of internal gain schedules are used: one for the living areas of the house and one for the sleeping areas. These alternate schedules are shown in Table 6-3.



Table 6-3 - Internal Gain Schedules for Zonal Control

Hour	Percent	Hour	Percent	Hour	Percent
Living Areas					
1	1.61	9	6.33	17	6.19
2	1.48	10	6.86	18	7.18
3	1.14	11	6.38	19	7.24
4	1.13	12	5.00	20	5.96
5	1.21	13	4.84	21	5.49
6	1.46	14	3.15	22	6.20
7	2.77	15	2.94	23	4.38
8	5.30	16	3.41	24	2.35
Sleeping Areas					
1	4.38	9	3.76	17	4.47
2	4.02	10	3.85	18	4.45
3	4.50	11	4.70	19	4.29
4	4.50	12	3.61	20	3.30
5	4.32	13	3.65	21	3.75
6	5.46	14	2.63	22	3.75
7	6.39	15	2.46	23	4.45
8	7.40	16	2.32	24	3.59

### 6.2.4 Tests

The zonal control feature is tested only for prototype A in five climate zones: 3, 9, 12, 14 and 16. Zonal control is added and the heating efficiency is modified accordingly. Each computer run must result in greater energy use than prototype A. The computer runs are summarized in Table 6-4 below. *Total of five runs.*

Table 6-4 - Zonal Control Test Inputs

Run Label	Zonal Control	Heating AFUE
03A52	yes	0.74
09A52	yes	0.55
12A52	yes	0.68
14A52	yes	0.68
16A52	yes	0.73

The optional capability test also requires that the vendor demonstrate that the ACM correctly defines the standard design building and calculates the custom budget. This test involves running the standard design equivalent building for climate zone 12 and showing that the custom budget figures from computer run "12A52" are equal. The standard design equivalent building is included in Appendix C and labeled "12A52C".



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### 6.3 Sunspaces

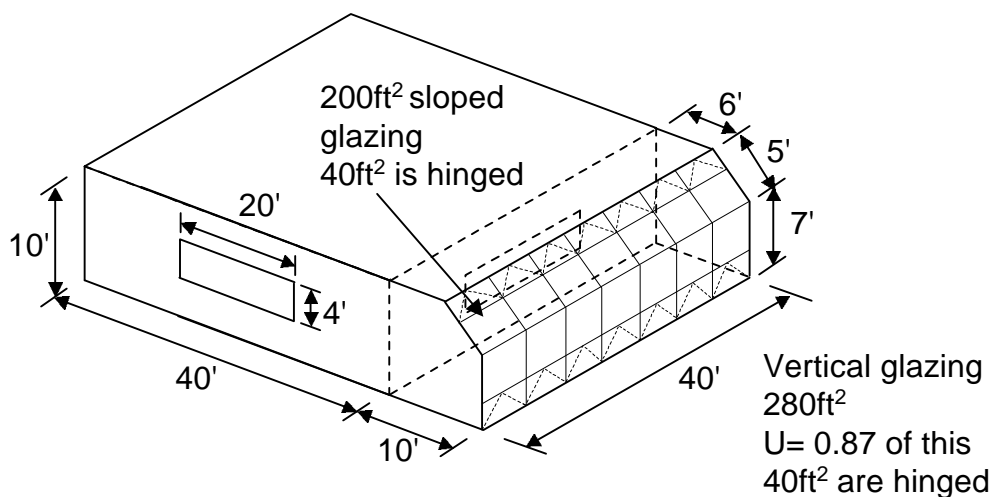
Sunspace modeling is one of the optional capabilities based on the ability of an ACM to model more than one thermal zone at the same time. The sunspace of the building is modeled as a separate, unconditioned thermal zone. The specifications for the test building are detailed in the CALRES98 input test file 12A53 available from the Commission on diskette, and key features are highlighted below.

An unconditioned sunspace is added to the south side of Prototype A as illustrated in Figures 3 and 4. The wall and window separating the sunspace and the house remains the same as in the base case, but the surfaces and vent openings of this wall are changed from exterior types to interzone types. The interzone vent is controlled to open only when temperature (T) conditions are  $T_{\text{house}} < T_{\text{desired}}$  and  $T_{\text{sunspace}} > T_{\text{house}}$  (in heating mode).

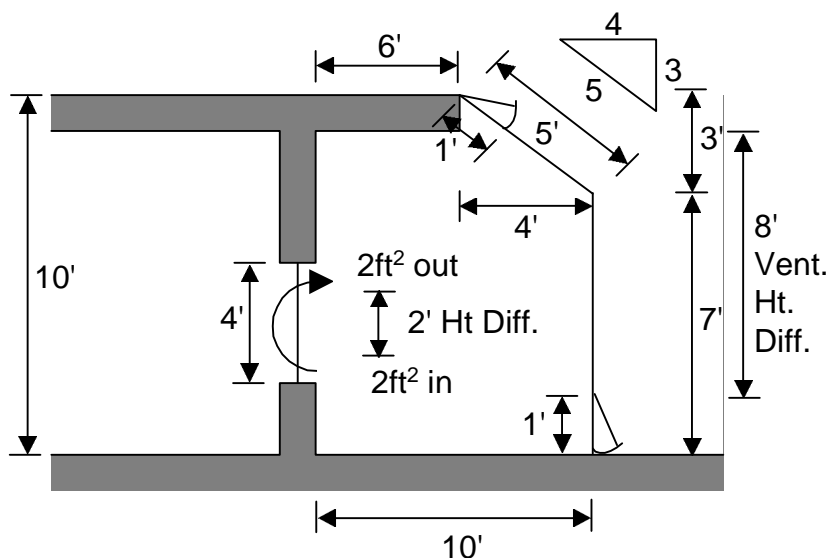
The performance characteristics of sunspace envelope components are the same as for the basecase prototype, except slab F2-value is 0.90; fenestration shading coefficient is 0.90, no internal shading device is assumed. Total vent area is assumed to be 40 ft<sup>2</sup> with an eight foot height difference

In the sunspace zone, assumptions for infiltration, heat capacity, solar gain targeting, and zone thermostat temperature settings vary from the conditioned zone. Sunspace zone infiltration is modeled using the air changes per hour method and the same infiltration factors as used in the 1988 ACM manual, 0.50 air changes per hour. There are no restrictions on targeting solar gains that enter unconditioned spaces such as sunspaces.





**Figure 6-3 Sunspace Prototype**



**Figure 6-4 Sunspace Section**

Sunspaces are tested only for prototype A in five climate zones: 3, 9, 12, 14 and 16. A sunspace is added and the heating efficiency is modified accordingly. Each computer run must result in greater energy use than prototype A. The computer runs are summarized below. *Total of five runs.*



Table 6-5 -

Run Label	Sunspace	Heating AFUE
03A53	yes	0.55
09A53	yes	0.29
12A53	yes	0.54
14A53	yes	0.54
16A53	yes	0.64

The optional capability test also requires that the vendor demonstrate that the ACM correctly defines the standard design building and calculates the custom budget. This test involves running the standard design equivalent building for climate zone 12 and showing that the custom budget figures from computer run "12A53" are equal.

#### 6.4 Side Fin Shading

Testing for side fins is performed relative to a modification of prototype A; the base building is rotated 30 degrees to the west. The test is performed in five climate zones: 3, 9, 12, 14 and 16. The specifications for the side fins are provided on the Commission's CALRES98 input file diskette as , test file 12A54. Key features are covered below.

The side fins extend 40 feet from the surface of a window that is assumed to be 10 feet wide. The fins are 5 feet from the edge of the window. The top of the side fins are 20 feet above the top of the window. Side fins are separately added to the east and west sides of the building and the heating efficiency is modified accordingly. Each computer run must result in greater energy use than prototype A. *Total of five runs.*

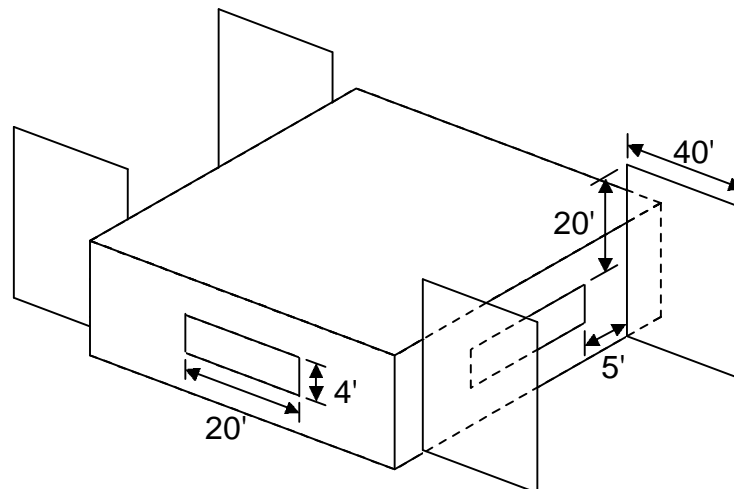


Figure 6-5 - Side Fins for Optional Capabilities Test



**Table 6-6 - Side Fin Test Inputs**

Run Label	Side Fins	Heating AFUE
03A54	Yes	0.87
09A54	yes	0.52
12A54	yes	0.72
14A54	yes	0.76
16A54	yes	0.81

The optional capability test also requires that the vendor demonstrate that the ACM correctly defines the standard design building and calculates the custom budget. This test involves running the standard design equivalent building for climate zone 12 and showing that the custom budget figures from computer run "12A54" are equal. The standard design equivalent building is included on the CALRES98 diskette as the input file labeled "12A54C".

### **6.5 Exterior Mass Walls**

The test for exterior mass walls is made relative to prototype A in five climate zones: 3, 9, 12, 14 and 16. All of the exterior walls of the building are assumed to be of mass construction: The mass is assumed to be 12 inches thick with a volumetric heat capacity of 10 Btu/F-cf and a conductivity of 1.064. The outside surface of the mass wall is modeled with a U-value of 2.63 ( $R = 0.38$ ) to approximate the effect of an air film. Insulation is assumed to be on the inside surface of the wall. This insulation is varied for each climate zone. Each computer run must result in greater energy use than prototype E. *Total of five runs.*

**Table 6-7 -**

Run Label	Exterior Mass Walls	Wall U-value
03A55	yes	0.134
09A55	yes	0.230
12A55	yes	0.140
14A55	yes	0.128
16A55	yes	0.112

The optional capability test also requires that the vendor demonstrate that the ACM correctly defines the standard design building and calculates the custom budget. This test involves running the standard design equivalent building for climate zone 12 and showing that the custom budget figures from computer run "12A55" are equal. The standard design equivalent building is included as the input file labeled "12A55C" on the CALRES98 input file diskette.



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## 6.6 Optional Water Heating Capabilities Tests

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### 6.6.1 Solar and Wood Stove Boiler Water Heating

Optional water heating capabilities include solar water heating and wood stove boiler-assisted water heating. Energy credit may be taken for the use of these technologies through the use of multipliers that adjust the water heating loads. For solar this adjustment is the Solar Savings Fraction (SSF<sub>j</sub>) derived from an f-Chart analysis and for wood stove boilers this adjustment is called the Wood Stove Adjustment Factor (WSAF<sub>j</sub>). These adjustments are used as shown in Section 4.21

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### 6.6.2 Combined Hydronic Space/Water Heating

Combined hydronic space/water heating is a system whereby a water heater is used to provide both space heating and water heating. Hydronic systems or water heaters dedicated solely to space heating are covered in Section 6.6.3.

For combined hydronic systems, an effective AFUE, or for electric water heaters or heat pumps, an effective HSPF, is calculated and used in the space heating energy calculations. When a fan coil is used to distribute heat, the fan energy and the heat contribution of the fan motor must be considered. This shall automatically be added when the distribution type is "ducts". The effective AFUE or HSPF is calculated according to the following equations for each water heater type.

#### 6.6.2.1 Storage Gas Water Heater

When storage gas water heaters are used in combined hydronic applications and there is no air distribution fan, then the effective AFUE is given by the following equation.

Equation 6-3

$$AFUE_{eff} = RE - \frac{PL}{RI}$$

Where

- AFUE<sub>eff</sub> = The effective AFUE of the gas water heater in satisfying the space heating load.
- RE = The recovery efficiency of the gas water heater. A default value of 0.76 may be assumed if the recovery efficiency is unknown.
- PL = Pipe losses (kBtu/h). This can be assumed to be zero when less than 10 feet of the piping between the water heater storage tank and the fan coil or other heating elements is located in unconditioned space.

Equation 6-4

$$PL = \sum_{i=1}^n \frac{FT_i \times PLR_i}{8760}$$



RI = The rated input of the gas water heater (kBtu/h).

When there is an air distribution fan, then the energy used by the fan and the heat contributed by the fan is considered in the same manner as it is for a furnace (see Section 4.18)

### 6.6.2.2 Storage Electric Water Heater

The HSPF of storage water heaters used for space heating in a combined hydronic system is given by the following equations. If the system has a fan coil, the HSPF<sub>eff</sub> is used.

HSPF<sub>w/o\_fan</sub> is used if there is no fan coil.

Equation 6-5

$$HSPF_{eff} = \frac{1+.005(3.413)}{\left[ \frac{1}{HSPF_{w/o\_fan}} \right] + .005}$$

Equation 6-6

$$HSPF_{w/o\_Fan} = 3.413 \left[ \frac{1 - \frac{PL}{3.413kW_i}}{1 + \frac{W_{PUMP}}{1000kW_i}} \right]$$

Where:

HSPF<sub>eff</sub> = The effective HSPF of the electric water heater in satisfying the space heating load.

W<sub>pump</sub> = The watts of the pump which circulates water between an electric storage water heater and the fan coil

PL = Pipe losses (kBtu/h). This can be assumed to be zero when less than 10 feet of the piping between the water heater storage tank and the fan coil or other heating elements is located in unconditioned space.

kWI = The kilowatts of input to the water heater.



### 6.6.2.3 Heat Pump Water Heater

The HSPF of heat pump water heaters used for space heating in a combined hydronic system is given by the following equations. If the system has a fan coil, the  $HSPF_{eff}$  is used.  $HSPF_{w/o\_fan}$  is used if there is no fan coil.

Equation 6-7

$$HSPF_{eff} = \frac{1+.005(3.413)}{\left[ \frac{1}{HSPF_{w/o\_fan}} \right] + .005}$$

Equation 6-8

$$HSPF_{w/o\_Fan} = 3.413 \left( \frac{RE_{hp}}{CZ_{adj}} - \frac{PL}{3.413kW_i} \right)$$

Where:

$HSPF_{eff}$  = The effective HSPF of the heat pump water heater in satisfying the space heating load.

$RE_{hp}$  = The recovery efficiency of the heat pump water heater. The following equation may be used as a default if the recovery efficiency is not known.

Equation 6-9

$$RE_{hp} = \frac{1}{\frac{1}{EF_{DOE}} - 0.1175}$$

$CZ_{adj}$  = The climate zone adjustment (see water heating calculation method) (see Table 4-11).

$PL$  = Pipe losses (kBtu/h). This can be assumed to be zero when less than 10 feet of the piping between the water heater storage tank and the fan coil or other heating elements is located in unconditioned space.

$kWI$  = The kilowatts of input.

$EF_{DOE}$  = The energy factor of the heat pump water heater when tested according to the DOE test procedure.

### 6.6.2.4 Pipe Losses

Pipe losses must be considered when pipes between the water heater storage tank and the fan coil or other heating element are located in unconditioned space. To simplify



compliance, pipe losses can be ignored when no more than ten feet of pipe (in plan view) is located in unconditioned space<sup>1</sup>. Hourly loss rates are given by the following equation.

Equation 6-10

$$PL = \sum_{i=1}^n \frac{FT_i PLR_i}{8760}$$

PL = Hourly pipe loss (kBtu/h).

PLR<sub>i</sub> = The annual pipe loss rate per foot of length for the i<sup>th</sup> pipe (kBtu/y-ft).

FT<sub>i</sub> = The length in feet of the i<sup>th</sup> pipe located within unconditioned space. Can be assumed to be zero if less than ten feet in plan view.

n = The number of unique pipe size or insulation conditions.  
The annual pipe loss rate per foot of length (PLR<sub>i</sub>) is calculated from the following equation

$$PLR_i = 8.76 \left( \frac{T_s - T_a}{\frac{\ln\left(\frac{D_{io}}{D_{po}}\right)}{2 \pi K_i} + \frac{1}{\pi h_a D_{io}}} \right)$$

Where

8.76 = Conversion factor from Btu/hour to kBtu/year

T<sub>s</sub> = Supply Temperature. This is assumed to be a constant 135 F.

T<sub>a</sub> = Ambient Temperature. This is assumed to be 60.3 in all California climate zones.

D<sub>io</sub> = Outside diameter of insulation. ft (actual not nominal).

D<sub>po</sub> = Outside diameter of pipe, ft (actual not nominal).

K<sub>i</sub> = Insulation conductivity, constant 0.023 Btu/h-ft-F

h<sub>a</sub> = Air film coefficient, constant 1.65 Btu/h-ft<sup>2</sup>-F

Pipe loss rates (PLR) values for typical conditions are shown in the table below

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<sup>1</sup> PL would have a value of about 0.10 for 10 feet of one inch pipe with R-4 insulation, which is required (see page 25 of ACM Approval Manual).



**Table 6-8 - Annual Pipe Loss Rates (kBtu/y-ft)**

Nominal Pipe Size	Insulation Thickness			
	None	1/2 inch	3/4 inch	1 inch
1/2 inch		71.6	60.9	54.2
3/4 inch		91.1	75.8	66.6
1 inch		109.9	90.1	78.1
1 - 1/2 inch		146.7	117.5	100.3
2 inch		182.9	144.3	121.7

**6.6.2.5 Tests**

Prototype A is used for this test, but combined hydronic systems are substituted for the gas furnace in the basecase. Three types of combined hydronic systems are tested -- labeled K, L and M.

- K A 75 gallon storage gas water heater is used for both space conditioning and water heating. Hot water base boards are used for heat distribution and insulated pipes are located in unconditioned space.
- L An electric water heater is used for both space conditioning and water heating and air is distributed through a fan coil system that delivers air to ducts located in an attic.
- M An electric heat pump is used for both space conditioning and water heating. Distribution is provided through hot water baseboards. All pipes are located within conditioned space.

The specifications for these three systems are shown in Table 6-9 below. When the combined hydronic system is substituted, the water heating energy and space heating energy must change by an exact ratio from the basecase (see boldface figures below).



Table 6-9 -Combined Hydronic Test Results

		K	L	M
Water Heater Type		SG	SE	HP
Recovery Efficiency	unitless	0.7800	n.a.	n.a.
Rated Input	kBtu/sf	60.0000	n.a.	n.a.
Rated Input	kW	n.a.	5.0000	n.a.
Wpump	W	n.a.	60.0000	n.a.
EF	unitless	n.a.	n.a.	2.0000
REhp	unitless	n.a.	n.a.	2.6144
CZadj (7)	unitless	n.a.	n.a.	0.9200
Pipe Length	ft	100.0000	n.a.	n.a.
PLR	kBtu/ft-y	60.9000	n.a.	n.a.
PL	kBtu/h	0.6952	n.a.	n.a.
AFUEheat	unitless	0.7684	n.a.	n.a.
AFUEeff	unitless	0.7519	n.a.	n.a.
DEh	unitless	0.8300	n.a.	n.a.
SEE	unitless	0.6241	0.3294	0.9188
<b>Ratio</b>	<b>unitless</b>	<b>1.0145</b>	<b>1.9219</b>	<b>0.6891</b>
HSPFw/o_fan	unitless	n.a.	3.3725	9.6988
HSPFeff	unitless	n.a.	3.3732	9.4081

The optional capability test also requires that the vendor demonstrate that the ACM correctly defines the standard design building and calculates the custom budget. This test involves running the standard design equivalent building for climate zone 12 and showing that the custom budget figures from computer run "12A56" are equal. The standard design equivalent building is included in Appendix D and labeled "12A56C".

### 6.6.3 Dedicated Hydronic Systems

Dedicated hydronic systems have boilers or other heating devices which produce hot water which is distributed through the building for heating. Such systems are permitted when the AFUE is known and can be entered. If the systems have pipes located in unconditioned space, then the AFUE must be adjusted for the pipe losses.

When water heaters are used in hydronic systems for space heating alone (a separate water heater for domestic service), the water heater functions as a boiler and is required by NAECA to have a minimum AFUE of 0.80. The AFUE of a water heater if tested as a boiler would be approximately equal to the average of the EF and the RE, and will generally not meet the minimum NAECA requirement. Water heaters proposed for use in hydronic systems for space heating only must be tested as a boiler using the DOE AFUE and appropriate safety standard test procedures.



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## 6.7 Building Additions

The low-rise residential Building Energy Efficiency Standards permit two ways of analyzing building additions using the performance approach. The addition may be analyzed alone, in which case the internal loads are prorated on a floor area basis. Alternatively, the addition may be analyzed together with the existing house. This second method permits improvements to be made to the existing house which may allow the building addition to have more glass or less insulation.

---

### 6.7.1 Addition Alone

When the addition is analyzed alone, the internal loads are prorated on a floor area basis in both the standard design and the proposed design runs. The total internal gain is based on the fractional dwelling unit value, which is used as the "Number-Dwelling-Units" in Equation 4.3 (see Section 4.5). An addition alone may not be modeled as zonal control.

Equation 6-11

$$\text{IntGainAdd} = \text{IntGainTotal} \times \text{FractionalDwellingUnit}$$

$$\text{FractionalDwellingUnit} = \text{CFAadd} \div (\text{CFAadd} + \text{CFAexisting})$$

---

### 6.7.2 Addition Plus Existing

When the building addition is analyzed together with the existing building, the procedure described in Chapter 6 of the *Residential Manual*, is followed.

It is necessary to manage information about the existing building and the addition in four categories as described below. These may be grouped in each table or separate C-2R forms may be generated for each category of information.

- 1 Features of the existing building that will not be upgraded or changed.
- 2 The current condition of existing building features that will be modified or upgraded.
- 3 The improved condition of existing building features that are upgraded. The total surface areas in this category will usually be less than those in the second category because an existing wall is usually eliminated where the addition is attached to the existing building.
- 4 Features of the proposed building addition.



## 6.8 Solar Water Heating and Space Heating

Modeling of solar water heating and space heating systems is not an optional capability for residential ACMs, but ACMs must provide an input for the energy provided by solar or other nondepletable sources. These inputs are described in Chapter 2.

The Commission has approved the use of various versions of the f-Chart program for analyzing active solar systems. These programs may be used to estimate the energy credit to enter in the ACM. Guidelines for the use of f-Chart are included in Chapter 7 of the *Residential Manual*.

This Manual does not address approval of solar analysis programs. The application package for approval of solar water heating and space conditioning programs is included as Appendix G.

When a credit is taken for nondepletable energy, the ACM standard input reports must flag this and include a statement in the *Special Features and Modeling Assumptions* section of the reports. The ACM user must also attach supporting calculations or worksheets of Commission approved methods.

## 6.9 Form 3 Report Generator

This test requires that ACMs correctly calculate the U-value of several construction assemblies. These construction assemblies are shown in Appendix E. The Form 3 generator must produce the values indicated in Table 6-10 for U-value. Construction assembly U-values must be calculated in a manner consistent with the manner and examples shown in the *Residential Manual*, in the glossary under "R-value" and "U-value", and in Appendix E.

**Table 6-10 - Form 3 Generator Results**

Construction Assembly Code	U-value
W.19.2x6.16	.065
R.38.2x4.24	.025
R.22.2x4.24	.041
RP.22.2x6.48	.044
FC.30.2x10.16	.028
FX.30.2x10.16	.034

## 6.10 Exceptional Methods Which May Be Approved In The Future

The Commission may approve additional Exceptional Methods in the future, for instance, additional water heating credits. All approved ACMs must provide an input for space heating, space cooling and water heating systems to allow the user to enter a value for these possible credits. The ACM standard reports identify all non-zero values and place a statement in the *Special Features and Modeling Assumptions* section of the standard reports. The ACM user must include supporting calculations, worksheets or equipment specifications with the building permit application.







<b>6. OPTIONAL CAPABILITIES TESTS</b>	<b>6-1</b>
<b>6.1 Controlled Ventilation Crawl Spaces (CVC)</b>	<b>6-1</b>
<b>6.2 Zonal Control</b>	<b>6-2</b>
6.2.1 Prototype Zones	6-3
6.2.2 Thermostats	6-3
6.1.3 Internal Gains	6-4
6.1.4 Tests	6-5
<b>6.3 Sunspaces</b>	<b>6-6</b>
<b>6.4 Side Fin Shading</b>	<b>6-8</b>
<b>6.5 Exterior Mass Walls</b>	<b>6-9</b>
<b>6.6 Optional Water Heating Capabilities Tests</b>	<b>6-10</b>
6.6.1 Solar and Wood Stove Boiler Water Heating	6-10
6.6.2 Combined Hydronic Space/Water Heating	6-10
6.6.3 Dedicated Hydronic Systems	6-15
<b>6.7 Building Additions</b>	<b>6-16</b>
6.7.1 Addition Alone	6-16
6.7.2 Addition Plus Existing	6-16
<b>6.8 Solar Water Heating and Space Heating</b>	<b>6-17</b>
<b>6.9 Form 3 Report Generator</b>	<b>6-17</b>
<b>6.10 Exceptional Methods Which May Be Approved In The Future</b>	<b>6-17</b>







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## **7. Home Energy Rating Systems (HERS) Required Verification And Diagnostic Testing**

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### ***7.1 California Home Energy Rating Systems***

The Commission is required to regulate home energy rating system (HERS) providers in California. It will soon be proposing the adoption of such regulations. When adopted, these regulations will appear in the California Code of Regulations, Title 20, Chapter 4, Article 8, Sections 1670-1676). Approved HERS providers will be authorized to certify raters and maintain quality control over ratings. Ratings will be based on visual inspection and diagnostic testing of the physical characteristics and energy efficiency features of houses, as constructed.

When compliance documentation indicates field verification and diagnostic testing of specific energy efficiency improvements as a condition for those improvements to qualify for Title 24 compliance credit, an approved HERS provider and certified HERS rater shall be used to conduct the field verification and diagnostic testing. HERS providers and raters shall be considered special inspectors by building departments, and shall demonstrate competence, to the satisfaction of the building official, for the visual inspections and diagnostic testing. The HERS provider and rater shall be independent entities from the builder or subcontractor installer of the energy efficiency improvements being tested and verified, and shall have no financial interest in the installation of the improvements

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### ***7.2 HERS Required Verification and Diagnostic Testing***

HERS diagnostic testing and field verification is required for compliance credit for:

- duct air sealing,
- ACCA Manual D design and installation,
- and building envelope sealing beyond improvements covered by default assumptions,

HERS field verification is required for compliance credit for:

- duct surface area reductions, and
- duct location improvements beyond those covered by default assumptions.

For compliance credit to be claimed for these features, they shall be listed as *HERS Verification Required* features on the *Certificate of Compliance* (CF-1R) and the *Computer Method Summary* (C-2R). Such verification constitutes “eligibility and installation criteria” for these features. Field verified and diagnostically tested features must be described in the *Compliance Supplement*.



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### **7.3 Installer Certification**

When compliance credit has been claimed for duct sealing, ACCA Manual D design and installation and envelope sealing, builder employees or subcontractors shall:

- complete diagnostic testing, and
- certify on the CF-6R the diagnostic test results and that the work meets the requirements for compliance credit.

For duct sealing completed at the rough-in stage of construction using aerosol sealant closures, builder employees or subcontractors shall:

- at rough-in, complete the fan pressurization test and certify on the CF-6R the diagnostic results,
- after installation of the interior finishing wall, verify sealing of the ducts using either the house pressure test or the pressure pan test or by visual inspection of all duct connections (including duct to air handler connections), and
- certify on the CF-6R the diagnostic results and that the work meets the requirements for compliance credit.

When compliance credit has been claimed for duct surface area reductions and duct location improvements beyond those covered by default assumptions, builder employees or subcontractors shall:

- record on the CF-6R the duct surface area in each duct location, and
- certify on the CF-6R that the duct surface area and locations match those on the plans, and that the work meets the requirements for compliance credit.

Installer certifications are required for each and every house.

---

### **7.4 HERS Verification Procedures**

At the builder's option HERS field verification and diagnostic testing shall be completed either for each house or for a sample of houses of the same model. To be considered the same model, houses shall be in the same subdivision and have the same energy designs and features, including the same floor area and volume, as shown on the CF-1R except that a house may differ in its shading. Field verification and diagnostic testing for compliance credit for duct sealing shall use the diagnostic duct leakage from fan pressurization of ducts in Section 4.3.8.2.1 of Appendix F.

The builder shall provide the HERS provider a copy of the CF-6R containing the installer certifications required in Section 7.3. Prior to completing field verification and diagnostic testing, the HERS rater shall first verify that the installer certifications have been completed.



If the builder chooses the sampling option, the procedures described in this section shall be followed. Sampling procedures described in this section shall be included in the *Compliance Supplement*.

#### **7.4.1 Initial Field Verification and Testing**

The HERS rater shall diagnostically test and field verify the first house of each model as specified in Section 7.2. This initial testing allows the builder to identify and correct any potential construction flaws or practices in the build out of each model. If field verification and diagnostic testing determines that the requirements for compliance are met, the HERS rater shall provide a signed and dated *Certificate of Field Verification and Diagnostic Testing* to the builder and the HERS provider.

#### **7.4.2 Sample Field Verification and Testing**

After the initial testing is completed, the builder shall identify a group of houses of the same model from which a sample will be selected for testing, and notify the HERS provider. The group shall include those houses expected to be ready for diagnostic testing within a 180 day period.

The builder shall identify these houses by location of County, City and either the street address or the subdivision and lot number, and shall identify the names and license numbers of subcontractors responsible for the duct installation, duct sealing or envelope sealing that requires diagnostic testing or field verification. The builder may add additional houses during the 180 day period by notifying the HERS provider.

The HERS provider shall select a minimum of one out of every seven sequentially completed houses in the group, rounded up to the next whole number, for diagnostic testing and field verification as described in Section 7.2.. When several houses are ready for testing at the same time, the HERS provider shall randomly select the houses to be tested. The HERS rater shall diagnostically test and field verify the houses selected by the HERS provider.

If field verification and diagnostic testing determines that the requirements for compliance are met, the HERS rater shall provide a signed and dated *Certificate of Field Verification and Diagnostic Testing* to the builder and the HERS provider. The *Certificate of Field Verification and Diagnostic Testing* shall report the successful diagnostic testing results and conclusions regarding compliance for the tested house.

The HERS rater shall provide a signed and dated *Certificate of Field Verification and Diagnostic Testing* to the builder and the HERS provider for up to six additional houses from the group. The *Certificate* shall not be provided for houses in which the feature requiring field verification and diagnostic testing has not been installed, sealed or completed.

The 180 day period shall begin on the date of the first *Certificate of Field Verification and Diagnostic Testing* for the group. The HERS provider shall determine the date the 180 day period ends, and shall notify the builder and rater. Houses within the group for which a *Certificate of Field Verification and Diagnostic Testing* has not been completed within 180 days from the date of the first *Certificate of Field Verification and*



*Diagnostic Testing* for the group, as determined by the HERS provider, shall either be individually tested or be included in a group of houses in a subsequent sample period.

Whenever the builder changes subcontractors who are responsible for the feature that is being diagnostically field verified and tested, the builder shall notify the HERS rater of any subcontractors who have changed, and terminate sampling for the identified group. The HERS rater shall cease certification. Whenever the builder changes HERS providers, the builder shall terminate sampling.

All houses using *HERS Required Verification* features for compliance that were installed by previous subcontractors or were subject to verification and testing under the supervision of a previous HERS provider, for which the builder does not have a completed *Certificate of Field Verification and Diagnostic Testing*, shall either be individually tested or included in a separate group for sampling. Houses with installations completed by new subcontractors shall either be individually tested or shall be included in a new sampling group following a new *Initial Field Verification and Testing*.

The HERS provider shall not notify the builder when sample testing will occur prior to the completion of the work that is to be tested. After the HERS provider notifies the builder when testing will occur, the builder shall not do additional work on the features being tested

#### **7.4.3 Re-sampling, Full Testing and Corrective Action,**

When a failure is encountered during sample testing, the HERS rater shall conduct re-sampling to assess whether that failure is unique or the rest of the houses are likely to have similar failings. The HERS provider shall select for re-sampling one out of every seven of all of the untested houses in the group that have been constructed since the beginning of the 180 day time period, rounded up to the next whole number.

If testing in all houses in the re-sample confirms that the requirements for compliance credit are met, then the house with the failure shall not be considered an indication of failure in the other houses in the group. The builder shall take corrective action for the house with the failure, and then the HERS rater shall retest to verify compliance and issue a signed and dated *Certificate of Field Verification and Diagnostic Testing* to the builder. Sampling shall then resume for the remainder of the group.

If field verification and testing in any of the houses in the re-sample results in a second failure, the builder shall take corrective action in all unoccupied houses in the group that have not been tested but for which a *Certificate of Field Verification and Diagnostic Testing* has been completed. The HERS rater shall conduct field verification and diagnostic testing in each of these houses to verify that problems have been corrected and that the requirements for compliance have been met, and shall report to the HERS provider.

Builders shall offer at no charge to homeowners in occupied houses in the group to complete field verification and testing and corrective action if necessary. Homeowners may decline this offer. Builders shall report the identifying location of any house in which the homeowner declines field verification and testing and corrective action to the HERS



provider. The HERS provider shall verify that the builder has made this offer. If a homeowner in an occupied house declines this offer, field verification, testing and corrective action will not be required for that house and the house will no longer be considered a part of the group. If a homeowner accepts this offer, the builder shall take corrective action. The HERS rater shall then conduct field verification and diagnostic testing to verify that problems have been corrected and that the requirements for compliance have been met, and shall report to the HERS provider.

The HERS provider shall file a report with the building department explaining all action taken (including field verification, testing, corrective action, offers to homeowners for testing and corrective action and homeowner declines of such offers) to bring into compliance houses for which a signed and dated *Certificate of Field Verification and Diagnostic Testing* has been provided to the builder. If corrective action requires work not specifically exempted by Section 112 of the UMC or Section 106 of the UBC, the builder shall obtain a permit from the building department prior to commencement of any of the work.

Until corrections, field verification and testing of all houses in the group have been completed or homeowners in occupied houses have declined corrective action, sampling of additional houses in the group shall cease. If additional houses in the group are completed during the time required to correct, field verify and test the previously completed houses in the group, the rater shall individually field verify and diagnostically test those additional houses to confirm that the requirements for compliance credit are met. Once corrections, field verification and testing is completed for all houses that have a *Certificate of Field Verification and Diagnostic Testing*, excepting those where homeowners have declined corrective action, the builder shall either resume sampling for the remainder of the houses in the group or terminate the group.

Corrections shall not be made to a sampled house to avoid a failure. If corrections are made to a sampled house, corrections, field verification and testing shall be performed on 100% of the houses in the group that have been constructed since the beginning of the 180 day period.

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## **7.5 Responsibilities and Documentation**

### **7.5.1 Builder**

Builder employees or sub contractors responsible for completing either diagnostic testing, visual inspection or verification as specified in Section 7.3 shall certify the diagnostic testing results and that the work meets the requirements for compliance credit on the CF-6R.

The builder shall provide the HERS provider with the identifying location of the group of houses to be included in the sample for field verification and diagnostic testing and the expected date that sampling may begin. The builder shall provide the HERS provider a



copy of the CF-6R signed by the builder employees or sub-contractors certifying that diagnostic testing and installation meet the requirements for compliance credit.

The builder shall provide a *Certificate of Field Verification and Diagnostic Testing* signed and dated by the HERS rater to the building official in conjunction with requests for final inspection for each house.

When resampling reveals a failure, builders shall offer at no charge to homeowners in occupied houses in the group to complete field verification, testing and corrective action if necessary. Homeowners may decline to have field verification and testing and corrective action completed. Builders shall report the identifying location of any house in which the homeowner declines field verification and testing and corrective action to the HERS provider. Builders shall take corrective action as required in all unoccupied houses in the group and in occupied houses in the group where homeowners have accepted field verification, testing and corrective action.

#### **7.5.2 HERS Provider and Rater**

The HERS provider shall maintain a list of the houses in the group from which sampling is drawn, the houses selected for sampling, the houses sampled and the results of the sampling, the houses selected for re-sampling, the houses that have been tested and verified as a result of re-sampling, the corrective action taken, and copies of all *Certificates of Field Verification and Diagnostic Testing* for a period of five years.

The HERS rater providing the diagnostic testing and verification shall sign and date a *Certificate of Field Verification and Diagnostic Testing* certifying that he/she has verified that the requirements for compliance credit have been met. *Certificates of Field Verification and Diagnostic Testing* shall be provided for the tested house and each of up to six other houses from the group for which compliance is verified based on the results of the sample. The HERS rater shall provide this certificate to the builder and the HERS provider.

The HERS Rater shall provide a separate *Certificate of Field Verification and Diagnostic Testing* for each house the rater determines has met the diagnostic requirements for compliance. The HERS rater shall identify on the *Certificate of Field Verification and Diagnostic Testing* if the house has been tested or if it was an untested house approved as part of sample testing. The HERS rater shall not sign a *Certificate of Field Verification and Diagnostic Testing* for a house that does not have a CF-6R signed by the installer as required in Sections 7.2 and 7.5.1.

If field verification and testing on a sampled house identifies a failure to meet the requirements for compliance credit, the HERS rater shall report to the HERS provider and the builder that re-sampling will be required.

If re-sampling identifies another failure, the HERS rater shall report to the HERS provider and the builder that corrective action and diagnostic testing and field verification will be required for all the untested houses in the group that have been constructed since



the beginning of the 180 day period. This report shall specify the identifying location of all houses that must be corrected and fully tested.

The HERS provider shall also report to the builder once diagnostic testing and field verification has shown that the failures have been corrected in all of the houses except those for which the homeowner has declined field verification, testing and corrective action.

When individual house testing and verification confirms that the requirements for compliance have been met, the HERS rater shall provide a *Certificate of Field Verification and Diagnostic Testing* for each previously untested/unverified house in the group and for each additional house of the same model completed during the time required to correct, verify and test the previously untested/unverified houses in the group.

The HERS provider shall file a report with the building department explaining all action taken (including field verification, testing, corrective actions, offers to homeowners for testing and corrective action, and homeowner declines of such offers) to bring into compliance houses for which a signed and dated *Certificate of Field Verification and Diagnostic Testing* has been provided to the builder.

### **7.5.3 Building Department**

The building department at its discretion may require independent testing and field verification in conjunction with the building department's required inspections, and/or observe the diagnostic testing and field verification performed by builder employees or subcontractors and the certified HERS rater in conjunction with the building department's required inspections to corroborate the results documented in installer certifications, and in the *Certificate of Field Verification and Diagnostic Testing*.

For houses that have used a compliance alternative that requires field verification and diagnostic testing, the building department shall not approve a house for occupancy until the building department has received from the builder a *Certificate of Field Verification and Diagnostic Testing* that has been signed and dated by the HERS rater.







<b>7. HOME ENERGY RATING SYSTEMS (HERS) REQUIRED VERIFICATION AND DIAGNOSTIC TESTING</b>	<b>7-1</b>
<b>7.1 California Home Energy Rating Systems</b>	<b>7-1</b>
<b>7.2 HERS Required Verification and Diagnostic Testing</b>	<b>7-1</b>
<b>7.3 Installer Certification</b>	<b>7-2</b>
<b>7.4 HERS Verification Procedures</b>	<b>7-2</b>
7.4.1 Initial Field Verification and Testing	7-3
7.4.2 Sample Field Verification and Testing	7-3
7.4.3 Re-sampling, Full Testing and Corrective Action,	7-4
<b>7.5 Responsibilities and Documentation</b>	<b>7-5</b>
7.5.1 Builder	7-5
7.5.2 HERS Provider and Rater	7-6
7.5.3 Building Department	7-7



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## **8. Compliance Supplement**

Each ACM vendor is required to publish a Compliance Supplement to the normal program users manual. The Compliance Supplement serves two major purposes. First, it helps building permit applicants to use the ACM correctly and to prepare complete documentation of their analyses. Second, it helps building officials to check permit applications for compliance with the low-rise residential Building Energy Efficiency Standards. As a result, it helps to assure that both the performance standards and the ACM are used properly.

The Compliance Supplement must describe the specific procedures for using the ACM for compliance with the Building Energy Efficiency Standards. The supplement must provide instructions for preparing the building input, using the correct fixed and restricted inputs, and for using each of the optional capabilities for which the ACM is approved. Also included are procedures for generating the standard reports and documenting the analysis. A sample of a properly documented building analysis must be included.

All Compliance Supplements must be written in a clear and concise manner and with a common organization and format. Variations in format may be approved by the CEC, however, to allow for the differences between ACMs. This will assure consistency between the compliance supplements of different ACMs, simplifying the enforcement task of building officials. Also, vendors of approved ACMs are required to make copies of their compliance supplement available to all building departments in California.

The following sections describe the information that must be included in all compliance supplements. It also presents the required organization for that information.

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### ***8.1 CEC Approval***

This section includes a copy of the official CEC notice of approval of the ACM. The notice may include restrictions or limitations on the use of the ACM. It will also include the date of approval, and may include an expiration date for approval as well. The notice will indicate which optional capabilities the ACM is approved for and other restrictions on its use for compliance. The CEC will provide this notice upon completion of evaluation of the ACM application.

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### ***8.2 Program Capabilities***

This section discusses the program capabilities, with supporting written material explaining, as necessary, how the ACM treats each one. Reference may be made to non-compliance sections of the ACM Users Manual for more complete descriptions, if they exist.

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### ***8.3 Standard Input/Output Report***

This section explains how to use the program to prepare the standard input/output reports.



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### ***8.4 Fixed and Restricted Inputs***

Approved ACMs must automatically use the standard fixed and restricted inputs for the standard design run. It must also default to the standard assumptions for the proposed design run. When the alternative fixed and restricted inputs are used for the proposed design run, the ACM must report this in the *Special Features and Modeling Assumptions* sections of the standard reports.

This section of the Compliance Supplement explains the fixed and restricted inputs and how they are invoked in the ACM. This is especially important if the ACM offers the possibility of non-compliance runs which can deviate from the fixed and restricted inputs.

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### ***8.5 Preparing Basic Input***

This section covers the basic use of the ACM for compliance. Optional capabilities are described in greater detail. Reference may be made to the users manual, but this section should include a complete summary of all inputs and/or commands necessary for compliance.

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### ***8.6 Optional Capabilities***

This section explains the procedures for using each of the optional capabilities of the ACM. It is a parallel section to the basic inputs section above. The section for each optional capability should explain how to prepare inputs, how to document assumptions, and what the limitations are of each analysis capability.

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### ***8.7 Special Features and Modeling Assumptions***

This section explains the use of the Special Features and Modeling Assumptions listing to highlight the importance of verifying the special features and the aspects of those features that were modeled to achieve compliance.

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### ***8.8 HERS Required Verification***

This section explains the use of the HERS Required Verification listing to highlight the special features that require diagnostic testing by a certified home energy rater under the supervision of a CEC approved HERS provider to assure proper installation and verification. This section may rely on the information provided in Chapter 7, other sections of this manual, or may refer to other Commission documents.

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### ***8.9 Checklist for Compliance Submittal***

This section should contain a concise checklist of all items that must be included in a compliance submittal to a building official using the ACM.



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### ***8.10 Sample Compliance Documentation***

This section should include a complete set of compliance documentation for a sample building. The building need not be overly complex, nor need it include every program capability. The example should, however, include all documentation and standard reports that would normally be submitted. This example will serve as a model to ACM users and building officials of what a proper compliance submittal should look like.

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### ***8.11 Compliance Statement***

The following statement must appear within the first several pages of the Supplement:

[ACM Name] may be used to show compliance with California's Residential Building Energy Efficiency Standards.

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### ***8.12 Related Publications***

The Compliance Supplement should refer users to the following related CEC publications and where to obtain them:

- *1998 Building Energy Efficiency Standards* (P400-98-001)
- *1998 Residential Manual* (P400-98-002)

Both publications are available from:

California Energy Commission  
Publications Unit  
1516 Ninth Street  
Sacramento CA 95814  
(916) 654-5200







<b>8. COMPLIANCE SUPPLEMENT</b>	<b>8-1</b>
8.1 CEC Approval	8-1
8.2 Program Capabilities	8-1
8.3 Standard Input/Output Report	8-1
8.4 Fixed and Restricted Inputs	8-2
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8.9 Checklist for Compliance Submittal	8-2
8.10 Sample Compliance Documentation	8-3
8.11 Compliance Statement	8-3
8.12 Related Publications	8-3







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## **9. Vendor Requirements**

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### ***9.1 Availability to CEC***

All ACM vendors are required to submit at least one version of the ACM to the California Energy Commission. An updated copy or access to the approved version of the ACM must be kept by the CEC to maintain approval for compliance usage of the ACM. The CEC agrees not to duplicate the ACM except for the purpose of analyzing it, for verifying building compliance with the ACM, or to verify that only approved versions of the ACM are used for compliance.

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### ***9.2 Building Department Support***

ACM vendors must provide a copy of the ACM Compliance Supplement to all local building enforcement agencies who request one in writing.

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### ***9.3 User Support***

It is expected that ACM vendors will offer support to their users with regard to the use of the ACM for compliance purposes. Vendors may charge a fee for user support.

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### ***9.4 ACM Vendor Demonstration***

The CEC may request ACM vendors to physically demonstrate their program's capabilities. One or more demonstrations may be requested before approval is granted.







<b>9. VENDOR REQUIREMENTS</b>	<b>9-1</b>
9.1 Availability to CEC	9-1
9.2 Building Department Support	9-1
9.3 User Support	9-1
9.4 ACM Vendor Demonstration	9-1



# APPENDIX A







**Certification of Alternative Calculation Method***Energy Efficiency Standards for Residential Buildings, Sections 2-150 to 152*

I, \_\_\_\_\_ (name), certify that this alternative calculation method (ACM),  
\_\_\_\_\_, (name of ACM), version number \_\_\_\_\_, dated  
\_\_\_\_\_, developed by, \_\_\_\_\_ (personnel or company),  
\_\_\_\_\_ (address) \_\_\_\_\_ (city, state) \_\_\_\_\_ (zip),

passes all of the ACM tests and gives results that are reliable and accurate when used for calculating custom budgets and annual energy use estimates to comply with CEC (California Energy Commission) regulations, subject to the fixed and restricted assumptions specified in the *Alternative Calculation Method (ACM) Approval Manual for the 1998 Energy Efficiency Standards for Residential Buildings*, and the fixed and restricted inputs specified in the manuals describing the use of this method (Users Manual and Compliance Supplement thereto). I certify that the calculation of energy use in buildings, following the instructions in the manuals, and using accurate and complete plans and specifications for a building will achieve reliable and accurate energy analysis results with this ACM. Moreover, the calculations are verifiable when modeling the same building and accurately applying the fixed and restricted assumptions and inputs mentioned above. I further certify that all variables used by the program that are not subject to ready verification in the plans and specifications or that are subject to occupant use are either fixed, carefully restricted, or defaulted in this ACM.

I also certify that the inputs, default values, and assumptions specified for compliance runs in the manuals, and used in the accompanying application for the CEC residential ACM approval, are consistent with the inputs, default values, and assumptions specified by the CEC in the *Alternative Calculation Method (ACM) Approval Manual for the 1998 Energy Efficiency Standards for Residential Buildings* for use when generating standard design budgets and annual energy use estimates. I also certify that all specific inputs, variables, and assumptions needed to achieve the accuracy required to pass the capability tests in the *ACM Approval Manual* are either not subject to user variation, are defaulted to the values used for compliance, or are clearly specified as restricted or required inputs in the manuals for the ACM. In addition, the manuals clearly indicates that an easily verified list of the actual values of any such variables used for performance approach compliance which are subject to programmatic or user variation are to be included with the compliance documentation supplied by a building permit applicant to the enforcement agency. In summary, I also certify that the results of this alternative calculation method as specified in the manuals for the ACM in conjunction with an accurate and adequate set of plans and specifications for a building are not subject to significant variation by the manipulation of unrestricted user specified inputs that are difficult or impossible to verify.

In certifying the reliability and accuracy of this ACM, I certify that the results of this ACM's calculations, algorithms and assumptions are open to inspection by any individual or State entity, that this ACM may be challenged for its validity and accuracy as specified by the ACM Approval Manual, and that if challenged, I will prepare an adequate response or face possible withdrawal of ACM approval.

This certification is based upon the tests and requirements specified in the *Alternative Calculation Method (ACM) Approval Manual for the 1998 Energy Efficiency Standards for Residential Buildings*, and upon personal knowledge and experience with the use of this alternative calculation method.

Signed \_\_\_\_\_

Date \_\_\_\_\_ Title \_\_\_\_\_







**Space Conditioning Test 1**

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
01A00				01A01			
02A00				02A01			
03A00				03A01			
04A00				04A01			
05A00				05A01			
06A00				06A01			
07A00				07A01			
08A00				08A01			
09A00				09A01			
10A00				10A01			
11A00				11A01			
12A00				12A01			
13A00				13A01			
14A00				14A01			
15A00				15A01			
16A00				16A01			
03B00				03B01			
09B00				09B01			
12B00				12B01			
14B00				14B01			
16B00				16B01			

**Space Conditioning Test 2**

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
01A00				01A02			
02A00				02A02			
03A00				03A02			
04A00				04A02			
05A00				05A02			
06A00				06A02			
07A00				07A02			
08A00				08A02			
09A00				09A02			
10A00				10A02			
11A00				11A02			
12A00				12A02			
13A00				13A02			
14A00				14A02			
15A00				15A02			
16A00				16A02			
03B00				03B02			
09B00				09B02			
12B00				12B02			
14B00				14B02			
16B00				16B02			



**Space Conditioning Test 3**

Reduce ceiling U-value and increase south glass

Basecase Building			Prototype Variation				
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A03	_____	_____	_____
09A00	_____	_____	_____	09A03	_____	_____	_____
12A00	_____	_____	_____	12A03	_____	_____	_____
14A00	_____	_____	_____	14A03	_____	_____	_____
16A00	_____	_____	_____	16A03	_____	_____	_____

**Space Conditioning Test 4**

Reduce wall U-value and increase west glass

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A04	_____	_____	_____
09A00	_____	_____	_____	09A04	_____	_____	_____
12A00	_____	_____	_____	12A04	_____	_____	_____
14A00	_____	_____	_____	14A04	_____	_____	_____
16A00	_____	_____	_____	16A04	_____	_____	_____

**Space Conditioning Test 5**

Add slab insulation and increase north glass

Basecase Building			Prototype Variation				
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A05	_____	_____	_____
09A00	_____	_____	_____	09A05	_____	_____	_____
12A00	_____	_____	_____	12A05	_____	_____	_____
14A00	_____	_____	_____	14A05	_____	_____	_____
16A00	_____	_____	_____	16A05	_____	_____	_____



**Space Conditioning Test 6**

Reduce glazing U-value and add north glass

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A06	_____	_____	_____
09A00	_____	_____	_____	09A06	_____	_____	_____
12A00	_____	_____	_____	12A06	_____	_____	_____
14A00	_____	_____	_____	14A06	_____	_____	_____
16A00	_____	_____	_____	16A06	_____	_____	_____

**Space Conditioning Test 7**

Increase glazing U-value and reduce glass area on all orientations

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A06	_____	_____	_____
09A00	_____	_____	_____	09A07	_____	_____	_____
12A00	_____	_____	_____	12A07	_____	_____	_____
14A00	_____	_____	_____	14A07	_____	_____	_____
16A00	_____	_____	_____	16A07	_____	_____	_____

**Space Conditioning Test 8**

Increase exposed mass and increase south glass area

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A08	_____	_____	_____
09A00	_____	_____	_____	09A08	_____	_____	_____
12A00	_____	_____	_____	12A08	_____	_____	_____
14A00	_____	_____	_____	14A08	_____	_____	_____
16A00	_____	_____	_____	16A08	_____	_____	_____



**Space Conditioning Test 9**

Increase exposed mass and increase west glass area

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A09	_____	_____	_____
09A00	_____	_____	_____	09A09	_____	_____	_____
12A00	_____	_____	_____	12A09	_____	_____	_____
14A00	_____	_____	_____	14A09	_____	_____	_____
16A00	_____	_____	_____	16A09	_____	_____	_____

**Space Conditioning Test 10**

Increase exposed mass and increase north glass area

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A10	_____	_____	_____
09A00	_____	_____	_____	09A10	_____	_____	_____
12A00	_____	_____	_____	12A10	_____	_____	_____
14A00	_____	_____	_____	14A10	_____	_____	_____
16A00	_____	_____	_____	16A10	_____	_____	_____

**Space Conditioning Test 11**

Increase exposed mass and increase east glass area

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A06	_____	_____	_____
09A00	_____	_____	_____	09A11	_____	_____	_____
12A00	_____	_____	_____	12A11	_____	_____	_____
14A00	_____	_____	_____	14A11	_____	_____	_____
16A00	_____	_____	_____	16A11	_____	_____	_____



**Space Conditioning Test 12**

Reduce exposed thermal mass, add exterior shading and increase west glass

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A12	_____	_____	_____
09A00	_____	_____	_____	09A12	_____	_____	_____
12A00	_____	_____	_____	12A12	_____	_____	_____
14A00	_____	_____	_____	14A12	_____	_____	_____
16A00	_____	_____	_____	16A12	_____	_____	_____

**Space Conditioning Test 13**

Increase exposed thermal mass, add better interior shading and increase south glass

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A13	_____	_____	_____
09A00	_____	_____	_____	09A13	_____	_____	_____
12A00	_____	_____	_____	12A13	_____	_____	_____
14A00	_____	_____	_____	14A13	_____	_____	_____
16A00	_____	_____	_____	16A13	_____	_____	_____

**Space Conditioning Test 14**

Add south overhang and increase south glass

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A14	_____	_____	_____
09A00	_____	_____	_____	09A14	_____	_____	_____
12A00	_____	_____	_____	12A14	_____	_____	_____
14A00	_____	_____	_____	14A14	_____	_____	_____
16A00	_____	_____	_____	16A14	_____	_____	_____



**Space Conditioning Test 15**

Move ducts to conditioned space and increase glass on all orientations

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A15	_____	_____	_____
09A00	_____	_____	_____	09A15	_____	_____	_____
12A00	_____	_____	_____	12A15	_____	_____	_____
14A00	_____	_____	_____	14A15	_____	_____	_____
16A00	_____	_____	_____	16A15	_____	_____	_____

**Water Heating Tests**

Enter the calculated values

Climate Zone	D	E	F	G	H	I	J
Energy Budget	_____	_____	_____	_____	_____	_____	_____
Standard	_____	_____	_____	_____	_____	_____	_____
POU/HWR	_____	_____	_____	_____	_____	_____	_____
Pipe Insulation	_____	_____	_____	_____	_____	_____	_____
Recirc/NoControl	_____	_____	_____	_____	_____	_____	_____
Recirc/Timer	_____	_____	_____	_____	_____	_____	_____
Recirc/Demand	_____	_____	_____	_____	_____	_____	_____
Recirc/Time+Temp	_____	_____	_____	_____	_____	_____	_____
Recirc/Temp	_____	_____	_____	_____	_____	_____	_____
Parallel Piping	_____	_____	_____	_____	_____	_____	_____



**Custom Budget Space Conditioning 31**

Gas heated slab floor building

Label	Basecase Building (from custom budget column)			Label	Standard Design Equivalent (from proposed design column)		
	Heating	Cooling	Total		Heating	Cooling	Total
01C31	_____	_____	_____	01C31C	_____	_____	_____
02C31	_____	_____	_____	02C31C	_____	_____	_____
03C31	_____	_____	_____	03C31C	_____	_____	_____
04C31	_____	_____	_____	04C31C	_____	_____	_____
05C31	_____	_____	_____	05C31C	_____	_____	_____
06C31	_____	_____	_____	06C31C	_____	_____	_____
07C31	_____	_____	_____	07C31C	_____	_____	_____
08C31	_____	_____	_____	08C31C	_____	_____	_____
09C31	_____	_____	_____	09C31C	_____	_____	_____
10C31	_____	_____	_____	10C31C	_____	_____	_____
11C31	_____	_____	_____	11C31C	_____	_____	_____
12C31	_____	_____	_____	12C31C	_____	_____	_____
13C31	_____	_____	_____	13C31C	_____	_____	_____
14C31	_____	_____	_____	14C31C	_____	_____	_____
15C31	_____	_____	_____	15C31C	_____	_____	_____
16C31	_____	_____	_____	16C31C	_____	_____	_____

**Custom Budget Space Conditioning 32**

Gas heated raised floor building

Label	Basecase Building (from custom budget column)			Label	Standard Design Equivalent (from proposed design column)		
	Heating	Cooling	Total		Heating	Cooling	Total
01C32	_____	_____	_____	01C32C	_____	_____	_____
02C32	_____	_____	_____	02C32C	_____	_____	_____
03C32	_____	_____	_____	03C32C	_____	_____	_____
04C32	_____	_____	_____	04C32C	_____	_____	_____
05C32	_____	_____	_____	05C32C	_____	_____	_____
06C32	_____	_____	_____	06C32C	_____	_____	_____
07C32	_____	_____	_____	07C32C	_____	_____	_____
08C32	_____	_____	_____	08C32C	_____	_____	_____
09C32	_____	_____	_____	09C32C	_____	_____	_____
10C32	_____	_____	_____	10C32C	_____	_____	_____
11C32	_____	_____	_____	11C32C	_____	_____	_____
12C32	_____	_____	_____	12C32C	_____	_____	_____
13C32	_____	_____	_____	13C32C	_____	_____	_____
14C32	_____	_____	_____	14C32C	_____	_____	_____
15C32	_____	_____	_____	15C32C	_____	_____	_____
16C32	_____	_____	_____	16C32C	_____	_____	_____



**Custom Budget Space Conditioning 33**

Electric heated slab floor building

Label	Basecase Building (from custom budget column)			Label	Standard Design Equivalent (from proposed design column)		
	Heating	Cooling	Total		Heating	Cooling	Total
01C33	_____	_____	_____	01C33C	_____	_____	_____
02C33	_____	_____	_____	02C33C	_____	_____	_____
03C33	_____	_____	_____	03C33C	_____	_____	_____
04C33	_____	_____	_____	04C33C	_____	_____	_____
05C33	_____	_____	_____	05C33C	_____	_____	_____
06C33	_____	_____	_____	06C33C	_____	_____	_____
07C33	_____	_____	_____	07C33C	_____	_____	_____
08C33	_____	_____	_____	08C33C	_____	_____	_____
09C33	_____	_____	_____	09C33C	_____	_____	_____
10C33	_____	_____	_____	10C33C	_____	_____	_____
11C33	_____	_____	_____	11C33C	_____	_____	_____
12C33	_____	_____	_____	12C33C	_____	_____	_____
13C33	_____	_____	_____	13C33C	_____	_____	_____
14C33	_____	_____	_____	14C33C	_____	_____	_____
15C33	_____	_____	_____	15C33C	_____	_____	_____
16C33	_____	_____	_____	16C33C	_____	_____	_____

**Optional Capability Test 51**

Controlled ventilation crawlspaces

Label	Basecase Building			Label	Prototype Variation		
	Heating	Cooling	Total		Heating	Cooling	Total
03B00	_____	_____	_____	03B51	_____	_____	_____
09B00	_____	_____	_____	09B51	_____	_____	_____
12B00	_____	_____	_____	12B51	_____	_____	_____
14B00	_____	_____	_____	14B51	_____	_____	_____
16B00	_____	_____	_____	16B51	_____	_____	_____
Custom Budget Test							
12B51	_____	_____	_____	12B51C	_____	_____	_____



**Optional Capability Test 52**

Zonal Control

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A52	_____	_____	_____
09A00	_____	_____	_____	09A52	_____	_____	_____
12A00	_____	_____	_____	12A52	_____	_____	_____
14A00	_____	_____	_____	14A52	_____	_____	_____
16A00	_____	_____	_____	16A52	_____	_____	_____
Custom Budget Test							
12A52	_____	_____	_____	12A52C	_____	_____	_____

**Optional Capability Test 53**

Sunscreens

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A53	_____	_____	_____
09A00	_____	_____	_____	09A53	_____	_____	_____
12A00	_____	_____	_____	12A53	_____	_____	_____
14A00	_____	_____	_____	14A53	_____	_____	_____
16A00	_____	_____	_____	16A53	_____	_____	_____
Custom Budget Test							
12A53	_____	_____	_____	12A53C	_____	_____	_____

**Optional Capability Test 54**

Side Fin Shading

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A54	_____	_____	_____
09A00	_____	_____	_____	09A54	_____	_____	_____
12A00	_____	_____	_____	12A54	_____	_____	_____
14A00	_____	_____	_____	14A54	_____	_____	_____
16A00	_____	_____	_____	16A54	_____	_____	_____
Custom Budget Test							
12A54	_____	_____	_____	12A54C	_____	_____	_____



**Optional Capability Test 55**

Exterior Mass Walls

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A55	_____	_____	_____
09A00	_____	_____	_____	09A55	_____	_____	_____
12A00	_____	_____	_____	12A55	_____	_____	_____
14A00	_____	_____	_____	14A55	_____	_____	_____
16A00	_____	_____	_____	16A55	_____	_____	_____
Custom Budget Test							
12A55	_____	_____	_____	12A55C	_____	_____	_____

**Optional Capability Test 56**

Combined Hydronic Space and Water Heating

Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A56K	_____	_____	_____
09A00	_____	_____	_____	09A56K	_____	_____	_____
12A00	_____	_____	_____	12A56K	_____	_____	_____
14A00	_____	_____	_____	14A56K	_____	_____	_____
16A00	_____	_____	_____	16A56K	_____	_____	_____
Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A56L	_____	_____	_____
09A00	_____	_____	_____	09A56L	_____	_____	_____
12A00	_____	_____	_____	12A56L	_____	_____	_____
14A00	_____	_____	_____	14A56L	_____	_____	_____
16A00	_____	_____	_____	16A56L	_____	_____	_____
Basecase Building				Prototype Variation			
Label	Heating	Cooling	Total	Label	Heating	Cooling	Total
03A00	_____	_____	_____	03A56M	_____	_____	_____
09A00	_____	_____	_____	09A56M	_____	_____	_____
12A00	_____	_____	_____	12A56M	_____	_____	_____
14A00	_____	_____	_____	14A56M	_____	_____	_____
16A00	_____	_____	_____	16A56M	_____	_____	_____
Custom Budget Test							
12A56	_____	_____	_____	12A56C	_____	_____	_____



---

**Optional Capability Test 57**

Form 3 Generator

Label	U-value	R-value
W.19.EQ2	_____	_____
FC.30.2x10.16	_____	_____
FX.30.2x10.16	_____	_____
R.22.2x6.24	_____	_____
RP.22.2x6.48	_____	_____
R.38.2x4.24	_____	_____







# APPENDIX B

The Contents of Appendix B Have Been Deleted.  
Appendix B is  
Reserved for Future Use for Sample CALRES Test  
Run Files and Input Descriptions for Tests 00 to 15.

These sample files will be added for information  
purposes only, and will not be adopted as regulations.







# APPENDIX C

Pages C-4 through C-60 have been deleted but are reserved for future use for final versions of the sample CALRES input descriptions of the C prototype building and the Custom Budget tests.

These sample files will be added for information purposes only, and will not be adopted as regulations.

Pages C-1 to C-3 are available upon request by calling Debbie Friese at (916) 654-4067.



# **APPENDIX D**

The Contents of Appendix D Have Been Deleted.  
Appendix D is  
Reserved for Future Use for Sample CALRES Test  
Run Files and Input Descriptions for the Optional  
Capabilities Tests

These sample files will be added for information  
purposes only, and will not be adopted as regulations.



# APPENDIX E







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**Table E-1      FRAMING CALCULATION APPROACHES/TABLES**







## **FRAMING CALCULATION APPROACHES/TABLES**

When showing compliance with the *Energy Efficiency Standards*, the envelope assemblies U-value must meet the *Standard's* requirements. For wood framed, metal framed and for light and heavy mass walls the tabulated default values of calculation methods presented in this section to determine the U-value of an assembly can be used in compliance.

- **TABLE E-2: FRAMED WALL ASSEMBLY U-VALUES**

If the wall assembly is generic or there is no need to take advantage or evaluate specific components of a construction assembly, the default U-values in Table E-2 can be used. Use of Table E-2 will significantly simplify compliance and save considerable time, however, the assumption used to develop these default tables are very conservative.

- **TABLE E-3: METAL FRAMING FACTORS**

This table includes values referenced in Chapter 3 to be used to adjust U-values calculations using a parallel method when metal framing is used.

- **TABLE E-4 through E-6: PROPERTIES OF MASONRY WALLS**

These tables list the U-value and Heat Capacity of basic types of masonry block construction. They also include the effects of insulation placed on block walls.

- **TABLE E-7: FRAMED WALL/FLOOR/CEILING ASSEMBLIES U-VALUES**

This table includes diagrams and assembly U-value calculations for some basic ceiling and floor assemblies.

- **TABLE E-8: DEFAULT FENESTRATION PRODUCT U-VALUES**

This table includes default fenestration product U-values for many common generic fenestration product types.

- **TABLE E-9: DEFAULT FENESTRATION PRODUCT SOLAR HEAT GAIN COEFFICIENTS**

This table includes default fenestration product Solar Heat Gain coefficients (SHGCs) for many common generic fenestration product types.

- **COMPUTER MODELING OF FRAMED ASSEMBLIES**

The Commission has developed the EZFRAME program to automate ASHRAE procedures in order to help the building community calculate the U-values of wood and metal framed assemblies with a higher degree of accuracy and speed. The output forms of this program can be used as part of a residential or nonresidential submittal.

- **U-VALUE CALCULATION PROCEDURES**

This section includes sample calculations for metal framed assemblies and all of the ASHRAE methods, including the parallel path, zonal method, and isothermal plane method. To calculate the U-value of more complex assemblies, or develop a better understanding of heat transfer through different types of construction assemblies, users may reference this section.







**Table E-2      FRAMED WALL ASSEMBLY U-VALUES**







**Table E-2: Framed Wall Assembly U-values**

<u>Framing Type and Spacing</u>	<u>Framing Cavity R-Value</u>	<u>Insulated Sheathing R-Value</u>	<u>Wood Wall U-Value</u>	<u>Metal Wall U-Value</u>	<u>Framing Type and Spacing</u>	<u>Framing Cavity R-Value</u>	<u>Insulated Sheathing R-Value</u>	<u>Wood Wall U-Value</u>	<u>Metal Wall U-Value</u>
2x4 @ 16" O.C.	11	0	0.098	0.202	2x6 @ 16" O.C.	19	0	0.065	0.120
	(compressed)	4	0.068	0.112		(compressed)	4	0.058	0.098
		5	0.064	0.101			5	0.048	0.089
		7	0.056	0.084			7	0.043	0.075
		8.7	0.051	0.073			8.7	0.040	0.067
	13	0	0.088	0.195		21	0	0.059	0.157
		4	0.063	0.109			4	0.046	0.096
		5	0.059	0.099			5	0.044	0.088
		7	0.052	0.082			7	0.041	0.075
		8.7	0.048	0.072			8.7	0.037	0.066
	15	0	0.081	0.189		22	0	0.062	0.158
		4	0.059	0.108		(compressed)	4	0.048	0.097
2x4 @ 24" O.C.		5	0.055	0.097	2x6 @ 24" O.C.		5	0.045	0.088
		7	0.049	0.077			7	0.041	0.075
		8.7	0.045	0.071			8.7	0.038	0.067
	11	0	0.094	0.173		19	0	0.062	0.135
		4	0.066	0.102		(compressed)	4	0.048	0.088
		5	0.062	0.093			5	0.045	0.081
		7	0.055	0.078			7	0.042	0.070
		8.7	0.050	0.069			8.7	0.039	0.062
	13	0	0.085	0.165		21	0	0.056	0.130
		4	0.061	0.099			4	0.044	0.086
		5	0.057	0.090			5	0.042	0.079
		7	0.051	0.077			7	0.039	0.068
		8.7	0.047	0.068			8.7	0.036	0.061
	15	0	0.077	0.158		22	0	0.058	0.132
		4	0.056	0.097		(compressed)	4	0.046	0.086
		5	0.053	0.088			5	0.043	0.079
		7	0.047	0.071			7	0.040	0.068
		8.7	0.044	0.067			8.7	0.037	0.061



Table E-2 (cont'd): Framed Wall Assembly U-values

Framing Type and Spacing	Framing Cavity R-Value	Insulated Sheathing R-Value	Wood Wall U-Value	Metal Wall U-Value	Framing Type and Spacing	Framing Cavity R-Value	Insulated Sheathing R-Value	Wood Wall U-Value	Metal Wall U-Value
2x8 @ 16" O.C.	19	0	0.059	0.145	2x10 @ 16" O.C.	30	0	0.041	0.120
		4	0.047	0.092			4	0.035	0.081
		5	0.044	0.084			5	0.033	0.075
		7	0.041	0.072			7	0.031	0.065
		8.7	0.038	0.064			8.7	0.029	0.059
	22	0	0.054	0.140		38 (compressed)	0	0.040	0.119
		4	0.043	0.090			4	0.033	0.080
		5	0.041	0.082			5	0.032	0.074
		7	0.038	0.071			7	0.030	0.065
		8.7	0.035	0.063			8.7	0.028	0.058
	25	0	0.050	0.136	2x10 @ 24" O.C.	30 (compressed)	0	0.039	0.099
		4	0.040	0.088			4	0.033	0.071
		5	0.038	0.081			5	0.032	0.066
		7	0.035	0.070			7	0.030	0.058
		8.7	0.033	0.062			8.7	0.028	0.053
	30 (compressed)	0	0.048	0.135		38	0	0.038	0.097
		4	0.039	0.088			4	0.032	0.070
		5	0.037	0.081			5	0.031	0.066
		7	0.035	0.070			7	0.029	0.058
		8.7	0.032	0.062			8.7	0.027	0.053
2x8 @ 24" O.C.	19	0	0.056	0.122					
		4	0.045	0.082					
		5	0.043	0.076					
		7	0.040	0.066					
		8.7	0.037	0.059					
	22	0	0.051	0.117					
		4	0.041	0.080					
		5	0.040	0.074					
		7	0.036	0.064					
		8.7	0.034	0.058					
	25	0	0.047	0.113					
		4	0.038	0.078					
		5	0.037	0.072					
		7	0.034	0.063					
		8.7	0.032	0.057					
	30 (compressed)	0	0.046	0.112					
		4	0.037	0.077					
		5	0.036	0.072					
		7	0.034	0.063					
		8.7	0.031	0.057					



**Table E-3: Metal Framing Factor**

METAL FRAMING FACTORS*			
Stud Spacing	Stud Depth	Insulation R-Value	Framing Factor
16" o.c.	4"	R-7	0.522
		R-11	0.403
		R-13	0.362
		R-15	0.328
	6"	R-19	0.325
		R-21	0.300
		R-22	0.287
		R-25	0.263
24" o.c.	4"	R-7	0.577
		R-11	0.458
		R-13	0.415
		R-15	0.379
	6"	R-19	0.375
		R-21	0.348
		R-22	0.335
		R-25	0.308
R-value calculation for Exterior Wall Assemblies with Metal Studs, July 19, 1990, Staff Draft Docket 90-CON-1.			
*Correction to metal framing factors applies to the entire assembly including: interior air films, interior surfaces, cavity/insulation, exterior surfaces, and exterior air films.			



**Table E-4: Properties of Hollow Unit Masonry Walls**

Type			Core Treatment		
			Solid Grout	Partly Grouted with UngROUTED Cells	
				Empty	Insulated
12"	LW CMU	U	0.51	0.43	0.30
		Rw	2.0	2.3	3.3
		HC	23	14.8	14.8
	MW CMU	U	0.54	0.46	0.33
		Rw	1.9	2.2	3.0
		HC	23.9	15.6	15.6
	NW CMU	U	0.57	0.49	0.36
		Rw	1.8	2.0	2.8
		HC	24.8	16.5	16.5
10"	LW CMU	U	0.55	0.46	0.34
		Rw	1.8	2.2	2.9
		HC	18.9	12.6	12.6
	MW CMU	U	0.59	0.49	0.37
		Rw	1.7	2.1	2.7
		HC	19.7	13.4	13.4
	NW CMU	U	0.62	0.52	0.41
		Rw	1.6	1.9	2.4
		HC	20.5	14.2	14.2
8"	LW CMU	U	0.62	0.50	0.37
		Rw	1.6	2.0	2.7
		HC	15.1	9.9	9.9
	MW CMU	U	0.65	0.53	0.41
		Rw	1.5	1.9	2.4
		HC	15.7	10.5	10.5
	NW CMU	U	0.69	0.56	0.44
		Rw	1.4	1.8	2.3
		HC	16.3	11.1	11.1
6"	LW CMU	U	0.57	0.47	0.39
		Rw	1.8	2.1	2.6
		HC	15.1	11.4	11.4
	MW CMU	U	0.68	0.54	0.44
		Rw	1.5	1.9	2.3
		HC	10.9	7.9	7.9
	MW CMU	U	0.72	0.58	0.48
		Rw	1.4	1.7	2.1
		HC	11.4	8.4	8.4
	NW CMU	U	0.76	0.61	0.52
		Rw	1.3	1.6	1.9
		HC	11.9	8.9	8.9
	Clay Unit	U	0.65	0.52	0.45
		Rw	1.5	1.9	2.2
		HC	11.1	8.6	8.6

**Notes:**

LW CMU is a Light Weight Concrete Masonry Unit per ASTM C 90, Calculated at 105 PCF density  
 MW CMU is a Medium Weight Concrete Masonry Unit per ASTM C 90, Calculated at 115 PCF density  
 NW CMU is a Normal Weight Concrete Masonry Unit per ASTM C 90, Calculated at 125 PCF density  
 Clay Unit is a Hollow Clay Unit per ASTM C 652, Calculated at 130 PCF density  
 Values include air films on inner and outer surfaces.

Calculations based on Energy Calculations and Data, CMAACN, 1986

Grouted Cells at 32" X 48" in Partly Grouted Walls

Source: Berkeley Solar Group; Concrete Masonry Association of California and Nevada



**Table E-5: Properties of Solid Unit Masonry and Solid Concrete Walls**

Type		Layer Thickness, inches									
		3	4	5	6	7	8	9	10	11	12
LW CMU	U	na	0.71	0.64	na	na	na	na	na	na	na
	Rw	na	1.4	1.6	na	na	na	na	na	na	na
	HC	na	7.00	8.75	na	na	na	na	na	na	na
MW CMU	U	na	0.76	0.70	na	na	na	na	na	na	na
	Rw	na	1.3	1.4	na	na	na	na	na	na	na
	HC	na	7.67	9.58	na	na	na	na	na	na	na
NW CMU	U	0.89	0.82	0.76	na	na	na	na	na	na	na
	Rw	1.1	1.2	1.3	na	na	na	na	na	na	na
	HC	6.25	8.33	10.42	na	na	na	na	na	na	na
Clay Brick	U	0.80	0.72	0.66	na	na	na	na	na	na	na
	Rw	1.3	1.4	1.5	na	na	na	na	na	na	na
	HC	6.30	8.40	10.43	na	na	na	na	na	na	na
Concrete	U	0.96	0.91	0.86	0.82	0.78	0.74	0.71	0.68	0.65	0.63
	Rw	1.0	1.1	1.2	1.2	1.3	1.4	1.4	1.5	1.5	1.6
	HC	7.20	9.60	12.00	14.40	16.80	19.20	21.60	24.00	26.40	28.80

## Notes:

LW CMU is a Light Weight Concrete Masonry Unit per ASTM C 90 or 55, Calculated at 105 PCF density

MW CMU is a Medium Weight Concrete Masonry Unit per ASTM C 90 or 55, Calculated at 115 PCF density

NW CMU is a Normal Weight Concrete Masonry Unit per ASTM C 90 or 55, Calculated at 125 PCF density

Clay Brick is a Clay Unit per ASTM C 62, Calculated at 130 PCF density

Concrete is structural poured or precast concrete, Calculated at 144 PCF density

Calculations based on Energy Calculations and Data, CMACN, 1986

Values include air films on inner and outer surfaces.

Source: Berkeley Solar Group; Concrete Masonry Association of California and Nevada



**Table E-6: Effective R-Values for Interior Insulation Layers on Structural Mass Walls**

Type		Furring space R-value without framing effects																					
Actual	Frame	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Thick																							
Any	None	0.5	1.5	2.5	3.5	4.5	5.5	6.5	7.5	8.5	9.5	10	11.5	12.5	13.5	14.5	15.5	16.5	17.5	18.5	19.5	20.5	21.5
0.5"	Wood	1.3	1.3	1.9	2.4	2.7	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na
	Metal	0.9	0.9	1.1	1.1	1.2	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na
0.75"	Wood	1.4	1.4	2.1	2.7	3.1	3.5	3.8	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na
	Metal	1.0	1.0	1.3	1.4	1.5	1.5	1.6	na	na	na	na	na	na	na	na	na	na	na	na	na	na	na
1.0"	Wood	1.3	1.5	2.2	2.9	3.4	3.9	4.3	4.6	4.9	na	na	na	na	na	na	na	na	na	na	na	na	na
	Metal	1.0	1.1	1.4	1.6	1.7	1.8	1.8	1.9	1.9	na	na	na	na	na	na	na	na	na	na	na	na	na
1.5"	Wood	1.3	1.5	2.4	3.1	3.8	4.4	4.9	5.4	5.8	6.2	6.5	6.8	7.1	na	na	na	na	na	na	na	na	na
	Metal	1.1	1.2	1.6	1.9	2.1	2.2	2.3	2.4	2.5	2.5	2.6	2.6	2.7	na	na	na	na	na	na	na	na	na
2"	Wood	1.4	1.5	2.5	3.3	4.0	4.7	5.3	5.9	6.4	6.9	7.3	7.7	8.1	8.4	8.7	9.0	9.3	na	na	na	na	na
	Metal	1.1	1.2	1.7	2.1	2.3	2.5	2.7	2.8	2.9	3.0	3.1	3.2	3.2	3.3	3.3	3.4	3.4	na	na	na	na	na
2.5"	Wood	1.4	1.5	2.5	3.4	4.2	4.9	5.6	6.3	6.8	7.4	7.9	8.4	8.8	9.2	9.6	10.0	10.3	10.6	10.9	11.2	11.5	na
	Metal	1.2	1.3	1.8	2.3	2.6	2.8	3.0	3.2	3.3	3.5	3.6	3.6	3.7	3.8	3.9	3.9	4.0	4.0	4.1	4.1	4.1	na
3"	Wood	1.4	1.5	2.5	3.5	4.3	5.1	5.8	6.5	7.2	7.8	8.3	8.9	9.4	9.9	10.3	10.7	11.1	11.5	11.9	12.2	12.5	12.9
	Metal	1.2	1.3	1.9	2.4	2.8	3.1	3.3	3.5	3.7	3.8	4.0	4.1	4.2	4.3	4.4	4.4	4.5	4.6	4.6	4.7	4.7	4.8
3.5"	Wood	1.4	1.5	2.6	3.5	4.4	5.2	6.0	6.7	7.4	8.1	8.7	9.3	9.8	10.4	10.9	11.3	11.8	12.2	12.6	13.0	13.4	13.8
	Metal	1.2	1.3	2.0	2.5	2.9	3.2	3.5	3.8	4.0	4.2	4.3	4.5	4.6	4.7	4.8	4.9	5.0	5.1	5.1	5.2	5.2	5.3
4"	Wood	1.4	1.6	2.6	3.6	4.5	5.3	6.1	6.9	7.6	8.3	9.0	9.6	10.2	10.8	11.3	11.9	12.4	12.8	13.3	13.7	14.2	14.6
	Metal	1.2	1.3	2.0	2.6	3.0	3.4	3.7	4.0	4.2	4.5	4.6	4.8	5.0	5.1	5.2	5.3	5.4	5.5	5.6	5.7	5.8	5.8
4.5"	Wood	1.4	1.6	2.6	3.6	4.5	5.4	6.2	7.1	7.8	8.5	9.2	9.9	10.5	11.2	11.7	12.3	12.8	13.3	13.8	14.3	14.8	15.2
	Metal	1.2	1.3	2.1	2.6	3.1	3.5	3.9	4.2	4.5	4.7	4.9	5.1	5.3	5.4	5.6	5.7	5.8	5.9	6.0	6.1	6.2	6.3
5"	Wood	1.4	1.6	2.6	3.6	4.6	5.5	6.3	7.2	8	8.7	9.4	10.1	10.8	11.5	12.1	12.7	13.2	13.8	14.3	14.8	15.3	15.8
	Metal	1.2	1.4	2.1	2.7	3.2	3.7	4.1	4.4	4.7	5.0	5.2	5.4	5.6	5.8	5.9	6.1	6.2	6.3	6.5	6.6	6.7	6.8
5.5"	Wood	1.4	1.6	2.6	3.6	4.6	5.5	6.4	7.3	8.1	8.9	9.6	10.3	11.0	11.7	12.4	13.0	13.6	14.2	14.7	15.3	15.8	16.3
	Metal	1.3	1.4	2.1	2.8	3.3	3.8	4.2	4.6	4.9	5.2	5.4	5.7	5.9	6.1	6.3	6.4	6.6	6.7	6.8	7.0	7.1	7.2

All furring thickness values given are actual dimensions

All values include .5" gypbd. on the inner surface, interior surface resistances not included

24" OC Furring      24 Gage, Z-type Metal Furring

Douglas-Fir Larch Wood Furring, density = 34.9 lb/cu.ft.

Insulation assumed to fill the furring space

[Source: Berkeley Solar Group; Concrete Masonry Association of California and Nevada]

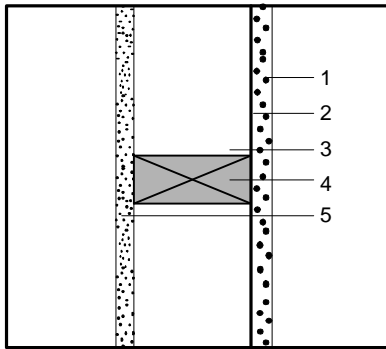


**Table E-7: Framed Wall/Floor/Ceiling Assembly U-values**







**Reference Name: W.0.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**
**Framing Size:**
**Framing Spacing:**
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

<input type="checkbox"/>	Floor
<input checked="" type="checkbox"/>	Wall
<input type="checkbox"/>	Ceiling/Roof
<b>Wood</b>	
<u>2</u>	× <u>4</u>
<u>16</u>	"o.c.
Wall:	<input checked="" type="checkbox"/> 15% (16"o.c.)
	<input type="checkbox"/> 12% (24"o.c.)
	<input type="checkbox"/> 9% (48"o.c.)
Floor/Ceiling:	<input type="checkbox"/> 10% (16"o.c.)
	<input type="checkbox"/> 7% (24"o.c.)
	<input type="checkbox"/> 4% (48"o.c.)
NA	

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	3.5" & greater air space; heat sideways
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

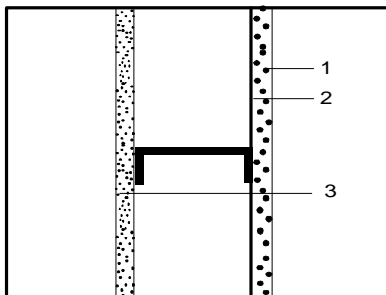
$$\left[ \left( \frac{1/2.385}{1+R_c} \right) \times \left( \frac{1-15/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \left( \frac{1/5.00}{1+R_f} \right) \times \left( \frac{15/100}{Fr.\% + 100} \right) \right] =$$

$$\frac{1/0.385}{1+Total\ U-Value} =$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.175	0.175
0.060	0.600
0.850	-----
-----	3.465
0.450	0.450
0.680	0.680
2.385	5.000
$R_c$	$R_f$

**0.385****Total U-Value**

2.591

**Total R-Value****Reference Name: W.0.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**
**Framing Spacing:**
**Framing Size:**
**Cavity Insulation:**
**Insulation Tape R-value:**

<input type="checkbox"/>	Floor
<input checked="" type="checkbox"/>	Wall
<input type="checkbox"/>	Ceiling/Roof
<b>Metal</b>	
<u>16</u>	"o.c.
Actual Depth	3.625
Actual Width	1.625
R-value	0.850
Knock-out (%)	15.00
Web Thickness	0.060
Interior Flange	0.0
Exterior Flange	0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.50 in gypsum or plaster board
4.	
5.	
6.	
7.	
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.449}{1+Total\ U-Value} =$$

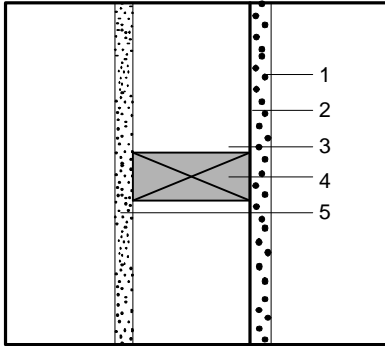
R-Value	
	0.170
	0.175
	0.060
	0.450
	0.680

**0.449****Total U-Value**

2.23

**Total R-Value**



**Reference Name: W.0.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof  
**Wood**  
2 X 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	3.5" & greater air space; heat sideways
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

Total Unadjusted R-Values:

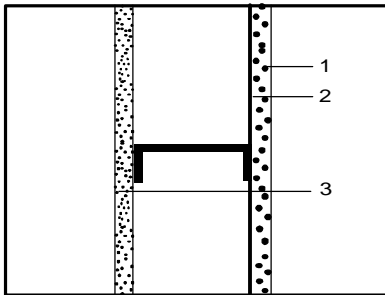
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/2.385}{1+R_c} \right) \times \left( \frac{1-12/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/5.000}{1+R_f} \right) \times \left( \frac{12/100}{Fr.\% +100} \right) \right] = \frac{1/0.393}{1+Total\ U-Value}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.175	0.175
0.060	0.600
0.850	-----
-----	3.465
0.450	0.450
-----	-----
0.680	0.680
2.385	5.000
$R_c$	$R_f$

**0.393****Total U-Value**

2.546  
**Total R-Value**

**Reference Name: W.0.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 0.850  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange 0.0  
Exterior Flange 0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.50 in gypsum or plaster board
4.	
5.	
6.	
7.	Inside Surface Air Film

**Calculation:**

From EZFRAME

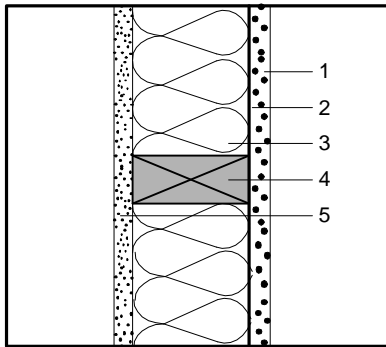
$$\frac{1/0.443}{1+Total\ U-Value}$$

R-Value	
0.170	
0.175	
0.060	
0.450	
-----	
-----	
-----	
0.680	

**0.443****Total U-Value**

2.260  
**Total R-Value**



**Reference Name: W.7.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof  
**Wood**  
2 × 4  
16 "o.c."  
Wall: ☒ 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-7 fiberglass insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

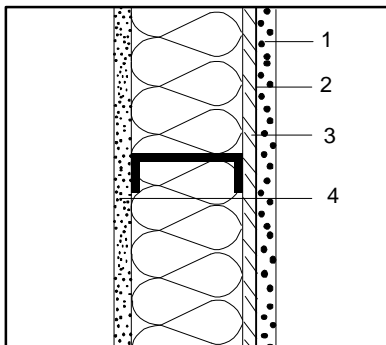
$$\left[ \left( \frac{1/8.535}{1+R_c} \right) \times \left( \frac{1-15/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/5.00}{1+R_f} \right) \times \left( \frac{15/100}{Fr.\% +100} \right) \right] =$$

$$\frac{1/0.130}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.600
7.000	-----
-----	3.465
0.450	0.450
0.680	0.680
8.535	5.000
R <sub>c</sub>	R <sub>f</sub>

**0.130****Total U-Value**

7.69

**Total R-Value****Reference Name: W.7.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 7.00  
Knock-out (%) 15.00  
Web Thickness 0.0600  
Interior Flange 0.0  
Exterior Flange 0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.50 in polyisocyanurate
4.	0.50 in gypsum or plaster board
5.	
6.	
7.	
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.125}{1+Total\ U-Value}$$

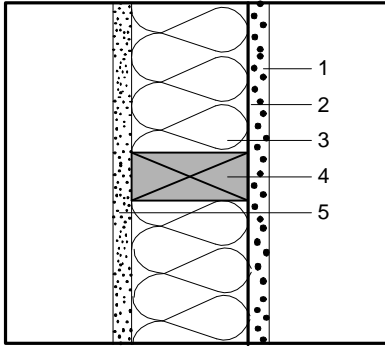
R-Value	
	0.170
	0.175
	0.060
	3.500
	0.450
	0.680

**0.125****Total U-Value**

7.990

**Total R-Value**



**Reference Name: W.7.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof  
**Wood**  
2 × 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-7 Fiberglass Insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

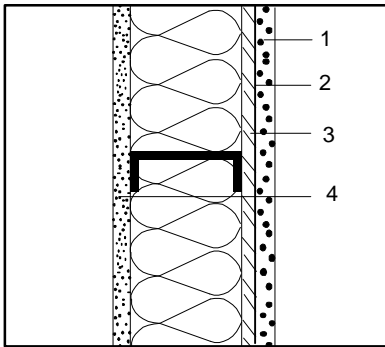
$$\left[ \left( \frac{1/8.535}{1+R_c} \right) \times \left( \frac{1-15/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/5.00}{1+R_f} \right) \times \left( \frac{15/100}{Fr.\% +100} \right) \right] =$$

$$\frac{1/0.127}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.600
7.000	-----
-----	3.465
0.450	0.450
0.680	0.680
8.535	5.000
R <sub>c</sub>	R <sub>f</sub>

**0.127****Total U-Value**

7.874

**Total R-Value****Reference Name: W.7.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 7.00  
Knock-out (%) 15.00  
Web Thickness 0.0600  
Interior Flange 0.0  
Exterior Flange 0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.50 in polyisocyanurate
4.	0.50 in gypsum or plaster board
5.	
6.	
7.	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.117}{1+Total\ U-Value}$$

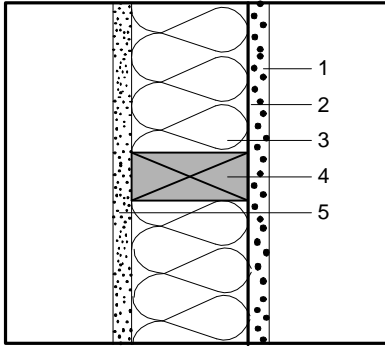
R-Value	
	0.170
	0.175
	0.060
	3.500
	0.450
	0.680

**0.117****Total U-Value**

8.530

**Total R-Value**



**Reference Name: W.11.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof  
**Wood**  
2 × 4  
16 "o.c."  
Wall: ☒ 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-11 fiberglass insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

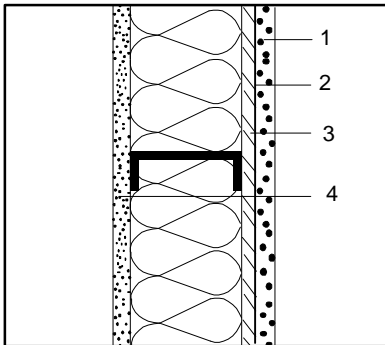
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{12.535} \right) \times \left( \frac{1-15/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \left( \frac{1}{5.00} \right) \times \left( \frac{15/100}{Fr.\% + 100} \right) \right] = \frac{1/0.098}{1 + \text{Total U-Value}}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.060
11.000	-----
-----	3.465
0.450	0.450
0.680	0.680
12.535	5.00
R <sub>c</sub>	R <sub>f</sub>

**0.098****Total U-Value**

10.204

**Total R-Value****Reference Name: W.11.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 11.00  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange 0.0  
Exterior Flange 0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.75 in polyisocyanurate
4.	0.50 in gypsum or plaster board
5.	
6.	
7.	
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.096}{1 + \text{Total U-Value}}$$

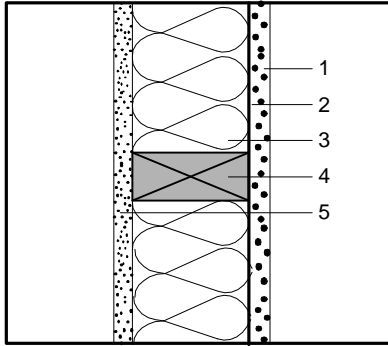
R-Value	
	0.170
	0.175
	0.060
	5.250
	0.450
	0.680

**0.096****Total U-Value**

10.360

**Total R-Value**



**Reference Name: W.11.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof  
**Wood**  
2 × 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-11 fiberglass insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

**Total Unadjusted R-Values:**

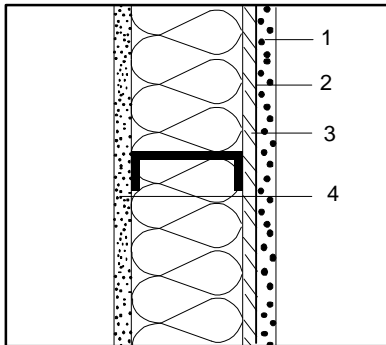
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{12.535} \right) \times \left( \frac{1-12/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1}{5.00} \right) \times \left( \frac{12/100}{Fr.\% \div 100} \right) \right] = \frac{1/0.094}{1 + \text{Total U-Value}}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.600
11.00	-----
-----	3.465
0.450	0.450
0.680	0.680
12.535	5.00
R <sub>c</sub>	R <sub>f</sub>

**0.094****Total U-Value**

10.638

**Total R-Value****Reference Name: W.11.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 11.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange 0.0  
Exterior Flange 0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.75 in polyisocyanurate
4.	0.50 in gypsum or plaster board
5.	
6.	
7.	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.090}{1 + \text{Total U-Value}}$$

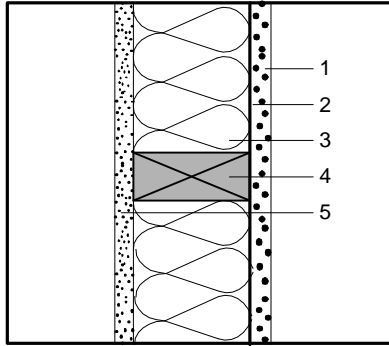
R-Value	
	0.170
	0.175
	0.060
	5.250
	0.450
	0.680

**0.090****Total U-Value**

11.140

**Total R-Value**



**Reference Name: W.13.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof  
**Wood**  
2 × 4  
16 "o.c."  
Wall: ☒ 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

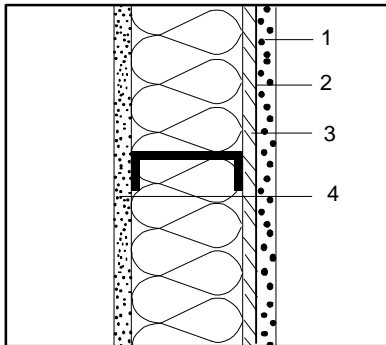
**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-13 fiberglass insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{14.535} \right) \times \left( \frac{1-15/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1}{5.00} \right) \times \left( \frac{15/100}{Fr.\% \div 100} \right) \right] = \frac{1/0.088}{1 + \text{Total U-Value}} = \frac{11.364}{\text{Total R-Value}}$$

**Reference Name: W.13.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 13.000  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange 0.0  
Exterior Flange 0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	1.00 in Polyisocyanurate
4.	0.50 in gypsum or plaster board
5.	
6.	
7.	
	Inside Surface Air Film

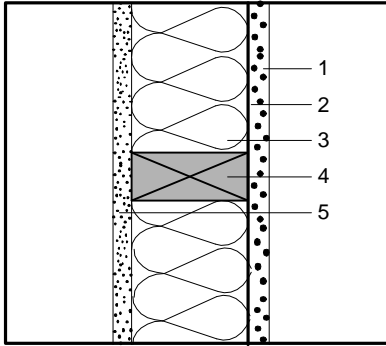
**Calculation:**

From EZFRAME

$$\frac{1/0.081}{1 + \text{Total U-Value}}$$

R-Value	
	0.170
	0.175
	0.060
	7.000
	0.450
	0.680
<b>0.081</b>	
<b>Total U-Value</b>	
	12.330
<b>Total R-Value</b>	



Reference Name: **W.13.2x4.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)Framing Material:  
Framing Size:  
Framing Spacing:  
Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)

Floor  
☒ Wall  
 Ceiling/Roof

**Wood**

2 × 4  
 24 "o.c."

Wall: 15% (16"o.c.)  
 12% (24"o.c.)  
☒ 9% (48"o.c.)  
 Floor/Ceiling: 10% (16"o.c.)  
 7% (24"o.c.)  
 4% (48"o.c.)

NA

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-13 fiberglass insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

## Framing Adjustment Calculation:

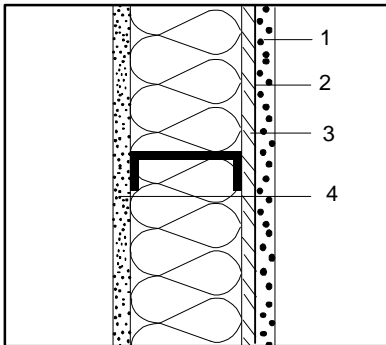
$$\left[ \left( \frac{1}{14.535} \right) \times \left( \frac{1-12/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \left( \frac{1}{5.00} \right) \times \left( \frac{12/100}{Fr.\% + 100} \right) \right] = \frac{1/0.085}{1 + \text{Total U-Value}}$$

## R-Value

Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.600
13.000	-----
-----	3.465
0.450	0.450
0.680	0.680
14.535	5.00
R <sub>c</sub>	R <sub>f</sub>

**0.085****Total U-Value**

10.620

**Total R-Value**Reference Name: **W.13.2x4.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)Framing Material:  
Framing Spacing:  
Framing Size:

Cavity Insulation:

Insulation Tape R-value:

Floor  
☒ Wall  
 Ceiling/Roof

**Metal**

24 "o.c."

Actual Depth 3.625  
 Actual Width 1.625  
 R-value 13.00  
 Knock-out (%) 15.00  
 Web Thickness 0.060  
 Interior Flange 0.0  
 Exterior Flange 0.0

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.75 in polyisocyanurate
4.	0.50 in gypsum or plaster board
5.	
6.	
7.	
	Inside Surface Air Film

## Calculation:

From EZFRAME

$$\frac{1/0.087}{1 + \text{Total U-Value}}$$

## R-Value

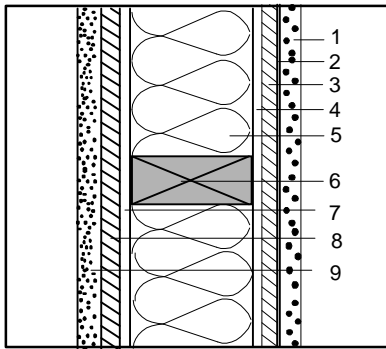
0.170
0.175
0.060
5.250
0.450
0.680

**0.087****Total U-Value**

11.460

**Total R-Value**



**Reference Name: WP.14.2x4.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof  
**Wood**  
2 X 4  
48 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.375 in plywood
4.	0.875 in Furring Channel
5.	3 5/8 in EPS foam insulation @ R-3.85/in
6.	2X4 in fir framing
7.	0.875 in Furring Channel
8.	0.375 in plywood
9.	0.50 in gypsum or plaster board
	Inside Surface Air Film

Total Unadjusted R-Values:

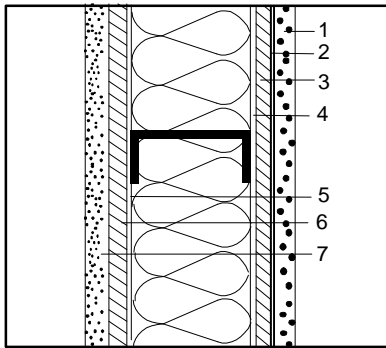
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{18.031} \right) \times \left( \frac{1-9/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1}{7.540} \right) \times \left( \frac{9/100}{Fr.\% \div 100} \right) \right] = \frac{1/0.062}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.060
0.470	0.470
0.800	0.800
13.956	-----
-----	3.465
0.800	0.800
0.470	0.470
0.450	0.450
0.680	0.680
18.031	7.540
R <sub>c</sub>	R <sub>f</sub>

**0.062****Total U-Value**

16.129  
**Total R-Value**

**Reference Name: WP.14.2x4.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof  
**Metal**  
48 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 14.00  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange 0.0  
Exterior Flange 0.0

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	1.00 in polyisocyanurate
4.	0.875 in Furring Channel
5.	0.875 in Furring Channel
6.	0.375 in plywood
7.	0.50 in gypsum or plaster board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

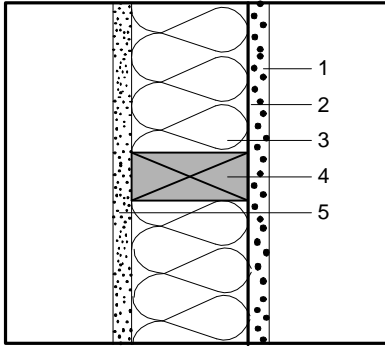
$$\frac{1/0.062}{1+Total\ U-Value}$$

R-Value	
	0.170
	0.175
	0.060
	7.000
	0.800
	0.800
	0.470
	0.450
	0.680

**0.062****Total U-Value**

16.26  
**Total R-Value**



Reference Name: **W.15.2x4.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)Framing Material:  
Framing Size:  
Framing Spacing:  
Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)

Floor  
☒ Wall  
 Ceiling/Roof

**Wood**

2 × 4  
 16 "o.c.

Wall: ☒ 15% (16"o.c.)  
☐ 12% (24"o.c.)  
☐ 9% (48"o.c.)

Floor/Ceiling: ☐ 10% (16"o.c.)  
☐ 7% (24"o.c.)  
☐ 4% (48"o.c.)

NA

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-15 fiberglass insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

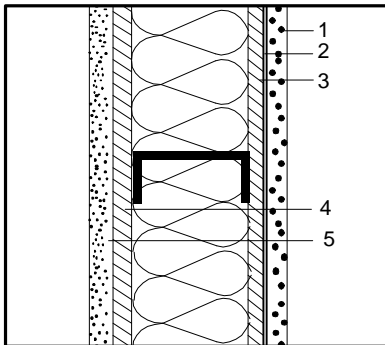
## Framing Adjustment Calculation:

$$\left[ \left( \frac{1}{16.535} \right) \times \left( \frac{1-15/100}{1} \right) \right] + \left[ \left( \frac{1}{5.00} \right) \times \left( \frac{15/100}{1} \right) \right] = \frac{1/0.081}{1 + \text{Total U-Value}}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.060
15.000	-----
-----	3.465
0.450	0.450
0.680	0.680
16.353	5.000
R <sub>c</sub>	R <sub>f</sub>

**0.081****Total U-Value**

12.346

**Total R-Value**Reference Name: **W.15.2x4.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)Framing Material:  
Framing Spacing:  
Framing Size:

Cavity Insulation:

Insulation Tape R-value:

Floor  
☒ Wall  
 Ceiling/Roof

**Metal**

16 "o.c.

Actual Depth 3.625  
 Actual Width 1.625  
 R-value 15.00  
 Knock-out (%) 15.00  
 Web Thickness 0.060  
 Interior Flange  
 Exterior Flange

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.50 in Polyisocyanurate
4.	0.50 in Polyisocyanurate
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

## Calculation:

From EZFRAME

$$\frac{1/0.080}{1 + \text{Total U-Value}}$$

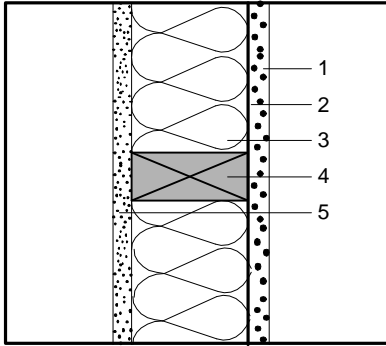
R-Value	
	0.170
	0.175
	0.060
	3.500
	3.500
	0.450
	0.680

**0.080****Total U-Value**

12.510

**Total R-Value**



Reference Name: **W.15.2x4.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)
 Framing Material:  
 Framing Size:  
 Framing Spacing:  
 Framing Percentage:  
 (check one)
Wall Weight / sf:  
(Packages only)
 Floor  
☒ Wall  
 Ceiling/Roof  
**Wood**  
 2 × 4  
 24 "o.c."  
 Wall:  
☐ 15% (16"o.c.)  
☒ 12% (24"o.c.)  
☐ 9% (48"o.c.)  
 Floor/Ceiling:  
☐ 10% (16"o.c.)  
☐ 7% (24"o.c.)  
☐ 4% (48"o.c.)  
 NA
**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-15 fiberglass insulation
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

Total Unadjusted R-Values:

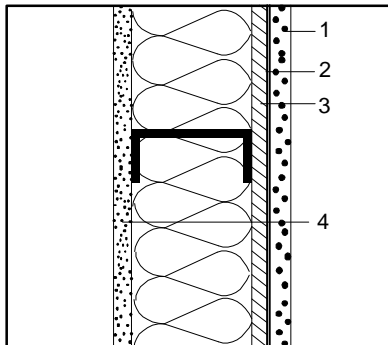
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{16.535} \right) \times \left( \frac{1-12/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1}{5.00} \right) \times \left( \frac{12/100}{Fr.\% \div 100} \right) \right] = \frac{1/0.077}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.060
15.000	-----
-----	3.465
0.450	0.450
0.680	0.680
16.535	5.00
R <sub>c</sub>	R <sub>f</sub>

**0.077****Total U-Value**

12.987

**Total R-Value**Reference Name: **W.15.2x4.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)
 Framing Material:  
 Framing Spacing:  
 Framing Size:

Cavity Insulation:

Insulation Tape R-value:

 Floor  
☒ Wall  
 Ceiling/Roof  
**Metal**  
 24 "o.c."  
 Actual Depth 3.625  
 Actual Width 1.625  
 R-value 15.00  
 Knock-out (%) 15.00  
 Web Thickness 0.060  
 Interior Flange  
 Exterior Flange
**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	1 in Polyisocyanurate
4.	0.50 in gypsum or plaster board
5.	
6.	
7.	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.074}{1+Total\ U-Value}$$

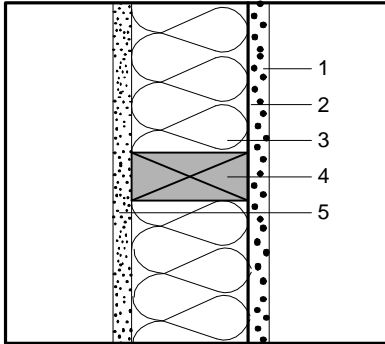
R-Value	
	0.170
	0.175
	0.060
	7.000
	0.450
	0.680

**0.074****Total U-Value**

13.470

**Total R-Value**



Reference Name: **W.19.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Size:

Framing Spacing:

Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)

Floor  
☒ Wall  
 Ceiling/Roof

**Wood**

2 × 6  
 16 "o.c.

Wall: ☒ 15% (16"o.c.)  
☐ 12% (24"o.c.)  
☐ 9% (48"o.c.)

Floor/Ceiling: ☐ 10% (16"o.c.)  
☐ 7% (24"o.c.)  
☐ 4% (48"o.c.)

NA

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-19 fiberglass insulation
4.	2x6 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

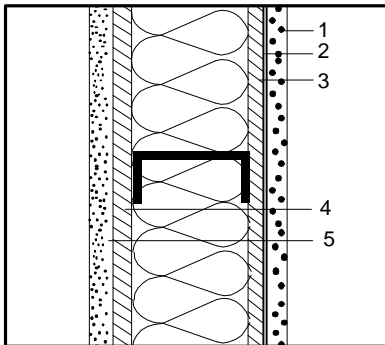
## Framing Adjustment Calculation:

$$\left[ \left( \frac{1}{19.335} \right) \times \left( \frac{1-15}{100} \right) \right] + \left[ \left( \frac{1}{6.98} \right) \times \left( \frac{15}{100} \right) \right] = \frac{1}{0.065}$$

$$\frac{1}{0.065} = 15.385$$

**0.065****Total U-Value**

15.385  
**Total R-Value**

Reference Name: **W.19.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Spacing:

Framing Size:

Cavity Insulation:

Insulation Tape R-value:

Floor  
☒ Wall  
 Ceiling/Roof

**Metal**

16 "o.c.

Actual Depth 6.000  
 Actual Width 1.625  
 R-value 19.00  
 Knock-out (%) 15.00  
 Web Thickness 0.060  
 Interior Flange  
 Exterior Flange

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.75 in polyisocyanurate
4.	0.50 in polyisocyanurate
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

## Calculation:

From EZFRAME

$$\frac{1}{0.064} = 15.530$$

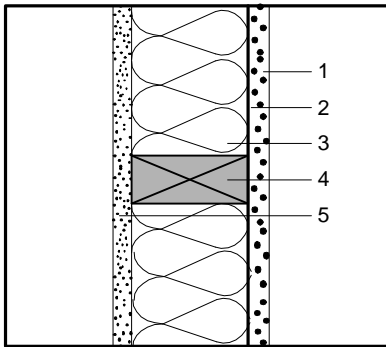
## R-Value

0.170
0.175
0.060
5.250
3.500
0.450
0.680

**0.064****Total U-Value**

15.530  
**Total R-Value**



Reference Name: **W.19.2x6.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Size:

Framing Spacing:

Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)

Floor  
☒ Wall  
☐ Ceiling/Roof

**Wood**

2 × 6  
 24 "o.c.

Wall: ☐ 15% (16"o.c.)  
☒ 12% (24"o.c.)  
☐ 9% (48"o.c.)

Floor/Ceiling: ☐ 10% (16"o.c.)  
☐ 7% (24"o.c.)  
☐ 4% (48"o.c.)

NA

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-19 fiberglass insulation
4.	2x6 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

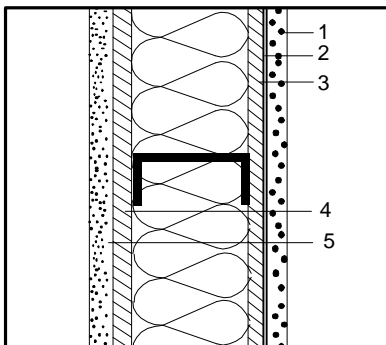
## Framing Adjustment Calculation:

$$\left[ \left( \frac{1}{19.335} \right) \times \left( \frac{1-12/100}{1-(12/100)} \right) \right] + \left[ \left( \frac{1}{6.980} \right) \times \left( \frac{12/100}{1-(12/100)} \right) \right] = \frac{1/0.063}{1+0.063}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.060
17.800	-----
-----	5.445
0.450	0.450
0.680	0.680
19.335	6.980
R <sub>c</sub>	R <sub>f</sub>

**0.063****Total U-Value**

15.873

**Total R-Value**Reference Name: **W.19.2x6.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Spacing:

Framing Size:

Cavity Insulation:

Insulation Tape R-value:

Floor  
☒ Wall  
☐ Ceiling/Roof

**Metal**

24 "o.c.

Actual Depth 6.000  
 Actual Width 1.625  
 R-value 19.00  
 Knock-out (%) 15.00  
 Web Thickness 0.060  
 Interior Flange  
 Exterior Flange

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.75 in polyisocyanurate
4.	0.50 in polyisocyanurate
5.	0.50 in gypsum board
6.	
7.	
	Inside Surface Air Film

## Calculation:

From EZFRAME

$$\frac{1/0.060}{1+0.060}$$

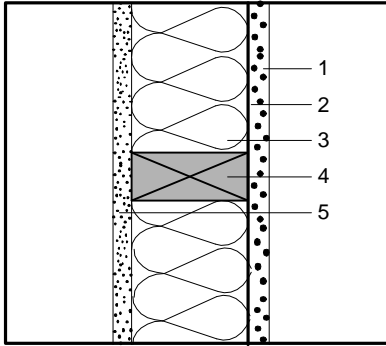
R-Value	
	0.170
	0.175
	0.060
	5.250
	3.500
	0.450
	0.680

**0.060****Total U-Value**

16.750

**Total R-Value**



Reference Name: **W.21.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Size:

Framing Spacing:

Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)

Floor  
☒ Wall  
 Ceiling/Roof

**Wood**

2 × 6  
 16 "o.c.

Wall: 15% (16"o.c.)  
 12% (24"o.c.)  
☒ 9% (48"o.c.)  
 Floor/Ceiling: 10% (16"o.c.)  
 7% (24"o.c.)  
 4% (48"o.c.)

NA

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-21 fiberglass insulation
4.	2x6 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

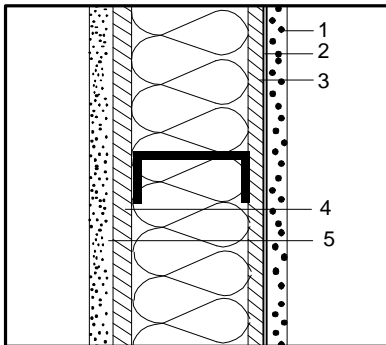
Total Unadjusted R-Values:

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.060
21.000	-----
-----	5.445
0.450	0.450
0.680	0.680
22.535	6.980
R <sub>c</sub>	R <sub>f</sub>

Framing Adjustment Calculation:

$$\left[ \left( \frac{1/22.535}{1+R_c} \right) \times \left( \frac{1-15/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \left( \frac{1/6.980}{1+R_f} \right) \times \left( \frac{15/100}{Fr.\% + 100} \right) \right] = \boxed{0.059}$$

$$\frac{1/0.059}{1+Total\ U-Value} = \frac{16.949}{Total\ R-Value}$$

Reference Name: **W.21.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Spacing:

Framing Size:

Cavity Insulation:

Insulation Tape R-value:

Floor  
☒ Wall  
 Ceiling/Roof

**Metal**

16 "o.c.

Actual Depth 6.000  
 Actual Width 1.625  
 R-value 21.00  
 Knock-out (%) 15.00  
 Web Thickness 0.060  
 Interior Flange  
 Exterior Flange

## List of Construction Components

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	1.0 in polyisocyanurate
4.	0.5 in polyisocyanurate
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

Calculation:

From EZFRAME

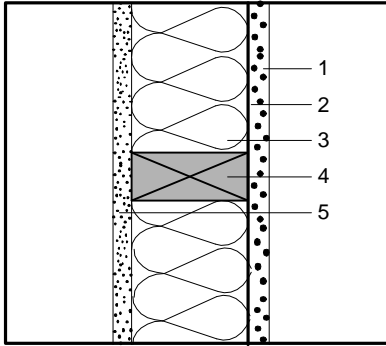
$$\frac{1/0.057}{1+Total\ U-Value}$$

R-Value	
	0.170
	0.175
	0.060
	7.000
	3.500
	0.450
	0.680

$$= \boxed{0.057}$$

$$= \frac{17.440}{Total\ R-Value}$$



Reference Name: **W.21.2x6.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Size:

Framing Spacing:

Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)

<input type="checkbox"/>	Floor
<input checked="" type="checkbox"/>	Wall
<input type="checkbox"/>	Ceiling/Roof
<b>Wood</b>	
<u>2</u>	× <u>6</u>
<u>24</u>	"o.c.
Wall:	15% (16"o.c.)
<input checked="" type="checkbox"/>	12% (24"o.c.)
<input type="checkbox"/>	9% (48"o.c.)
Floor/Ceiling:	10% (16"o.c.)
<input type="checkbox"/>	7% (24"o.c.)
<input type="checkbox"/>	4% (48"o.c.)
NA	

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	R-21 fiberglass insulation
4.	2x6 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

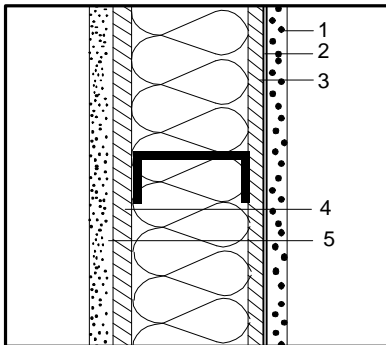
$$\left[ \left( \frac{1}{22.535} \right) \times \left( \frac{1-12/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/6.98}{1+R_f} \right) \times \left( \frac{12/100}{Fr.\% +100} \right) \right] =$$

$$\frac{1/0.056}{1+Total\ U-Value} =$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.175	0.175
0.060	0.060
21.000	-----
-----	3.465
0.450	0.450
0.680	0.680
22.535	6.980
R <sub>c</sub>	R <sub>f</sub>

**0.056****Total U-Value**

17.857

**Total R-Value**Reference Name: **W.21.2x6.24**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Spacing:

Framing Size:

Cavity Insulation:

Insulation Tape R-value:

<input type="checkbox"/>	Floor
<input checked="" type="checkbox"/>	Wall
<input type="checkbox"/>	Ceiling/Roof
<b>Metal</b>	
<u>24</u>	"o.c.
Actual Depth	6.000
Actual Width	1.625
R-value	21.00
Knock-out (%)	15.00
Web Thickness	0.060
Interior Flange	
Exterior Flange	

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	1.0 in polyisocyanurate
4.	0.5 in polyisocyanurate
5.	0.50 in gypsum or plaster board
6.	
7.	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.053}{1+Total\ U-Value} =$$

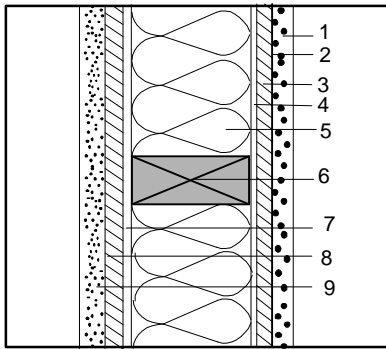
R-Value	
	0.170
	0.175
	0.060
	7.000
	3.500
	0.450
	0.680

**0.053****Total U-Value**

18.720

**Total R-Value**



**Reference Name: WP.22.2x6.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
☒ Wall  
Ceiling/Roof

**Wood**

2 × 6  
48 "o.c.

Wall: 15% (16" o.c.)  
12% (24" o.c.)  
9% (48" o.c.)  
Floor/Ceiling: 10% (16" o.c.)  
7% (24" o.c.)  
4% (48" o.c.)

NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.375 in plywood
4.	0.875 in Furring Channel
5.	R-21.656 EPS foam insulation
6.	2X6 in fir framing
7.	0.875 in Furring Channel
8.	0.375 in plywood
9.	0.50 in gypsum or plaster board
	Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/25.731}{1+R_c} \right) \times \left( \frac{1-9/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1/9.52}{1+R_f} \right) \times \left( \frac{9/100}{Fr.\% \div 100} \right) \right] = \frac{1/0.044}{1+Total\ U-Value}$$

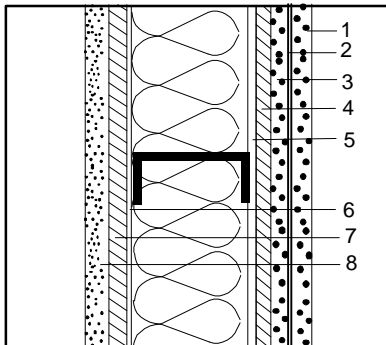
R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.175	0.175
0.060	0.060
0.470	0.470
0.800	0.800
21.656	-----
-----	5.445
0.800	0.800
0.470	0.470
0.450	0.450
0.680	0.680
25.731	9.520
$R_c$	$R_f$

**0.044**

**Total U-Value**

22.727

**Total R-Value**

**Reference Name: WP.22.2x6.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Spacing:**

**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
☒ Wall  
Ceiling/Roof

**Metal**

48 "o.c.

Actual Depth 6.000  
Actual Width 1.625  
R-value 21.700  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	1.50 in polyisocyanurate
4.	0.50 in plywood
5.	0.875 in Furring channel
6.	0.875 in Furring channel
7.	0.50 in plywood
8.	0.50 in gypsum or plaster board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.044}{1+Total\ U-Value}$$

=

**0.044**

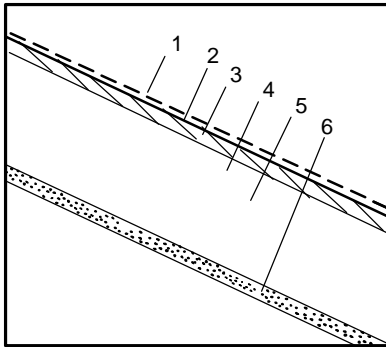
**Total U-Value**

=

22.83

**Total R-Value**



**Reference Name: R.0.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof

**Wood**

2 × 6  
16 "o.c.

Wall: \_\_\_\_\_ 15% (16" o.c.)  
\_\_\_\_\_ 12% (24" o.c.)  
\_\_\_\_\_ 9% (48" o.c.)  
Floor/Ceiling: ☒ 10% (16" o.c.)  
\_\_\_\_\_ 7% (24" o.c.)  
\_\_\_\_\_ 4% (48" o.c.)

NA

**List of Construction Components**

- |    |  |
|----|--|
|    | Outside Surface Air Film                 |
| 1. | Asphalt shingle roofing                  |
| 2. | Building paper (felt)                    |
| 3. | 0.50 in plywood                          |
| 4. | 3.5 in & greater air space; heat flow up |
| 5. | 2x6 in fir framing                       |
| 6. | 0.50 in gypsum or plaster board          |
| 7. | Inside Surface Air Film                  |

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/3.150}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \left( \frac{1/7.795}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% + 100} \right) \right] =$$

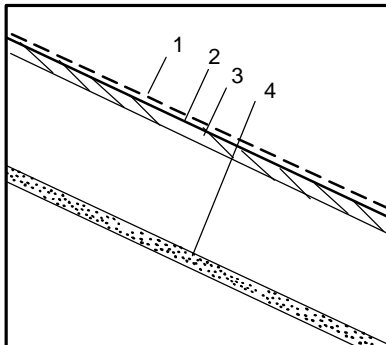
$$\frac{1/0.298}{1+Total\ U-Value}$$

**R-Value**

Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
<b>0.800</b>	----
----	5.445
0.450	0.450
0.610	0.610
3.150	7.795
R <sub>c</sub>	R <sub>f</sub>

**0.298****Total U-Value**

3.356  
**Total R-Value**

**Reference Name: R.0.2X6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof

**Metal**

16 "o.c.  
Actual Depth 6.000  
Actual Width 1.625  
R-value 0.800  
Knock-out (%) 15.00  
Web Thickness 0.06  
Interior Flange  
Exterior Flange

**List of Construction Components**

- |    |                                 |
|----|---------------------------------|
|    | Outside Surface Air Film        |
| 1. | Asphalt shingle                 |
| 2. | Building paper (felt)           |
| 3. | 0.50 in plywood                 |
| 4. | 0.50 in gypsum or plaster board |
| 5. |                                 |
| 6. |                                 |
| 7. | Inside Surface Air Film         |

**Calculation:**

From EZFRAME

$$\frac{1/0.323}{1+Total\ U-Value}$$

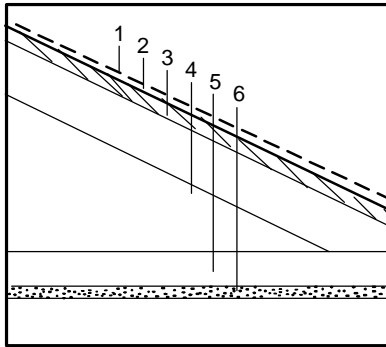
**R-Value**

0.170
0.440
0.060
0.630
0.450
0.620

**0.323****Total U-Value**

3.090  
**Total R-Value**



**Reference Name: R.0.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
2. Building paper (felt)
3. 0.50 in plywood
4. 3.5" & greater air space; heat sideways
5. 2x4 in fir framing
6. 0.50 in gypsum or plaster board
7. Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

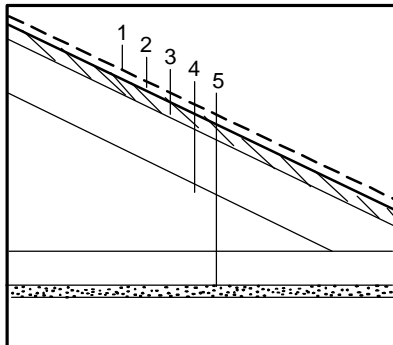
$$\left[ \left( \frac{1/3.150}{1+R_c} \right) \times \left( \frac{1-7/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1/6.615}{1+R_f} \right) \times \left( \frac{7/100}{Fr.\% \div 100} \right) \right] =$$

$$\frac{1/0.306}{1+Total\ U-Value}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
-----	3.465
0.450	0.450
0.610	0.610
3.150	6.615
$R_c$	$R_f$

**0.306****Total U-Value**

3.268  
**Total R-Value**

**Reference Name: R.0.2X4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 0.800  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle
2. Building paper (felt)
3. 0.50 in plywood
4. 3.5" & greater air space; heat sideways
5. 0.50 in gypsum or plaster board
- 6.
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

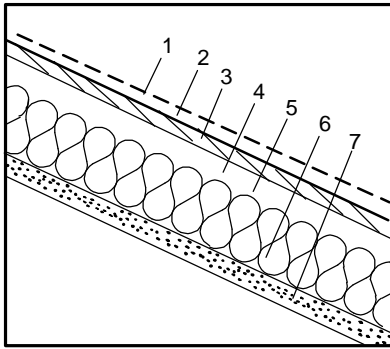
$$\frac{1/0.316}{1+Total\ U-Value}$$

R-Value	
	0.170
	0.440
	0.060
	0.630
	0.800
	0.450
	0.610

**0.316****Total U-Value**

3.160  
**Total R-Value**



**Reference Name: R.11.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof

**Wood**

2 × 6  
16 "o.c.

Wall: \_\_\_\_\_ 15% (16"o.c.)  
\_\_\_\_\_ 12% (24"o.c.)  
\_\_\_\_\_ 9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
\_\_\_\_\_ 7% (24"o.c.)  
\_\_\_\_\_ 4% (48"o.c.)

NA

**List of Construction Components**

- |    |                                 |
|----|---------------------------------|
|    | Outside Surface Air Film        |
| 1. | Asphalt shingle roofing         |
| 2. | Building paper (felt)           |
| 3. | 0.50 in plywood                 |
| 4. | 2.0 in air space; heat flow up  |
| 5. | 2X6 in fir framing              |
| 6. | R-11 fiberglass insulation      |
| 7. | 0.50 in gypsum or plaster board |
|    | Inside Surface Air Film         |

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/14.130}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/7.795}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% +100} \right) \right] =$$

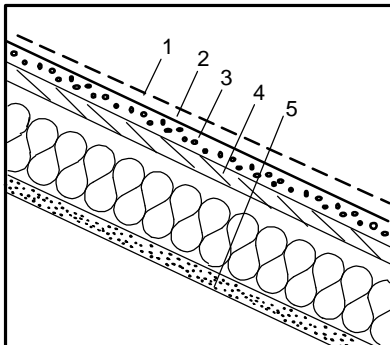
$$\frac{1/0.077}{1+Total\ U-Value}$$

**R-Value**

Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.780	-----
-----	5.445
11.000	-----
0.450	0.450
0.610	0.610
14.130	7.795
R <sub>c</sub>	R <sub>f</sub>

**0.077****Total U-Value**

12.987

**Total R-Value****Reference Name: R.11.2X6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof

**Metal**

16 "o.c.  
Actual Depth 6.000  
Actual Width 1.625  
R-value 11.800  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- |    |                                 |
|----|---------------------------------|
|    | Outside Surface Air Film        |
| 1. | Asphalt shingle                 |
| 2. | Building paper (felt)           |
| 3. | 0.75 in Polyisocyanurate        |
| 4. | 0.625 in Plywood                |
| 5. | 0.50 in gypsum or plaster board |
| 6. |                                 |
| 7. |                                 |
|    | Inside Surface Air Film         |

**Calculation:**

From EZFRAME

$$\frac{1/0.071}{1+Total\ U-Value}$$

**R-Value**

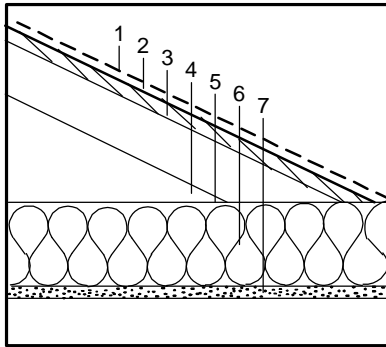
0.170
0.440
0.060
5.250
0.780
0.450
-----
-----
0.620

**0.071****Total U-Value**

14.060

**Total R-Value**



**Reference Name: R.11.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 X 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
2. Building paper (felt)
3. 0.50 in plywood
4. 3.50 in & greater air space; heat flow up
5. R-11 fiberglass insulation
6. 2X4 in fir framing
7. 0.50 in gypsum or plaster board
- Inside Surface Air Film

**Total Unadjusted R-Values:**

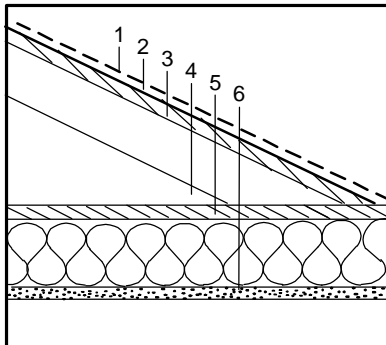
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{14.150} \right) \times \left( \frac{1-7/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{6.615} \right) \times \left( \frac{7/100}{1+R_f} \right) \right] = \frac{1/0.077}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
11.000	-----
-----	3.465
0.450	0.450
0.610	0.610
14.150	6.615
R <sub>c</sub>	R <sub>f</sub>

**0.077****Total U-Value**

12.987

**Total R-Value****Reference Name: R.11.2X4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 11.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle
2. Building paper (felt)
3. 0.50 in plywood
4. 3.50 in & greater air space; heat flow up
5. 0.75 in Polyisocyanurate
6. 0.50 in gypsum or plaster board
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.069}{1+Total\ U-Value}$$

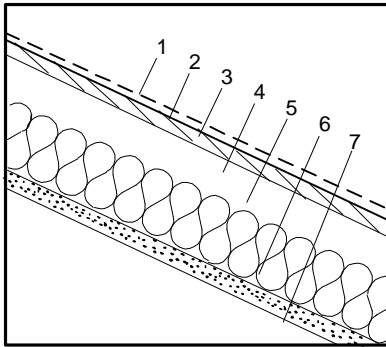
R-Value	
	0.170
	0.440
	0.060
	0.630
	0.800
	5.250
	0.450
	-----
	0.610

**0.069****Total U-Value**

14.500

**Total R-Value**



**Reference Name: R.13.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 6  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- |    |                                 |
|----|---------------------------------|
|    | Outside Surface Air Film        |
| 1. | Asphalt shingle roofing         |
| 2. | Building paper (felt)           |
| 3. | 0.50 in plywood                 |
| 4. | 2.0 in air space; heat flow up  |
| 5. | 2X6 in fir framing              |
| 6. | R-13 fiberglass insulation      |
| 7. | 0.50 in gypsum or plaster board |
|    | Inside Surface Air Film         |

Total Unadjusted R-Values:

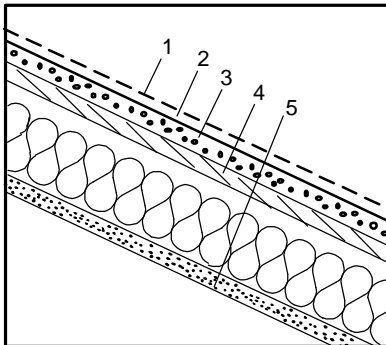
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{16.130} \right) \times \left( \frac{1-10/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{7.795} \right) \times \left( \frac{10/100}{1+R_f} \right) \right] = \frac{1/0.069}{1+\text{Total U-Value}}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.780	-----
-----	5.445
13.000	-----
0.450	0.450
0.610	0.610
16.130	7.795
R <sub>c</sub>	R <sub>f</sub>

**0.069****Total U-Value**

14.493

**Total R-Value****Reference Name: R.13.2X6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 6.00  
Actual Width 1.625  
R-value 13.800  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- |    |                                 |
|----|---------------------------------|
|    | Outside Surface Air Film        |
| 1. | Asphalt shingle                 |
| 2. | Building paper (felt)           |
| 3. | 1.00 in polyisocyanurate        |
| 4. | 0.50 in plywood                 |
| 5. | 0.50 in gypsum or plaster board |
| 6. |                                 |
| 7. |                                 |
|    | Inside Surface Air Film         |

**Calculation:**

From EZFRAME

$$\frac{1/0.062}{1+\text{Total U-Value}}$$

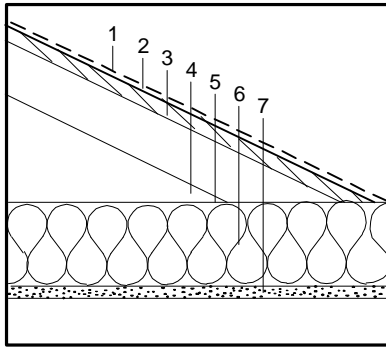
R-Value	
0.170	
0.440	
0.060	
7.000	
0.630	
0.450	
0.620	

**0.062****Total U-Value**

16.130

**Total R-Value**



**Reference Name: R.13.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 X 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- |    |   |
|----|---|
|    | Outside Surface Air Film                  |
| 1. | Asphalt shingle roofing                   |
| 2. | Building paper (felt)                     |
| 3. | 0.50 in plywood                           |
| 4. | 3.50 in & greater air space; heat flow up |
| 5. | R-13 fiberglass insulation                |
| 6. | 2X4 in fir framing                        |
| 7. | 0.50 in gypsum or plaster board           |
|    | Inside Surface Air Film                   |

Total Unadjusted R-Values:

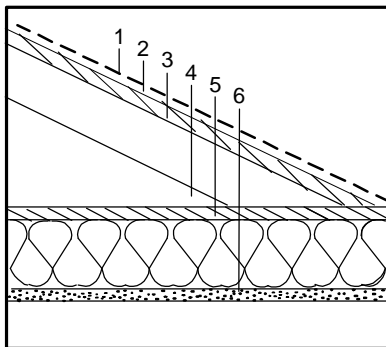
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{16.150} \right) \times \left( \frac{1-7/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{6.615} \right) \times \left( \frac{7/100}{1+R_f} \right) \right] = \frac{1/0.069}{1+\text{Total U-Value}}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
13.000	-----
-----	3.465
0.450	0.450
0.610	0.610
16.150	6.615
R <sub>c</sub>	R <sub>f</sub>

**0.069****Total U-Value**

14.492  
**Total R-Value**

**Reference Name: R.13.2X4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 13.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- |    |   |
|----|---|
|    | Outside Surface Air Film                  |
| 1. | Asphalt shingle                           |
| 2. | Building paper (felt)                     |
| 3. | 0.50 in plywood                           |
| 4. | 3.50 in & greater air space; heat flow up |
| 5. | 0.75 in Polyisocyanurate                  |
| 6. | 0.50 in gypsum or plaster board           |
| 7. |   |
|    | Inside Surface Air Film                   |

**Calculation:**

From EZFRAME

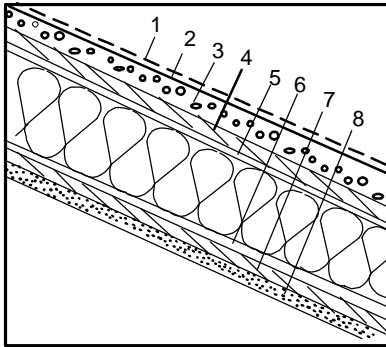
$$\frac{1/0.066}{1+\text{Total U-Value}}$$

R-Value	
0.170	
0.440	
0.060	
0.630	
0.800	
5.250	
0.450	
0.610	

**0.066****Total U-Value**

15.100  
**Total R-Value**



**Reference Name: RP.14.2x4.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 4  
48 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
2. Building paper (felt)
3. 0.375 in plywood
4. 7/8 in furring channel
5. 2X4 in fir framing
6. 3 5/8 in EPS foam insulation
7. 7/8 in furring channel
8. 0.375 in plywood
9. 0.50 in gypsum or plaster board
- Inside Surface Air Film

Total Unadjusted R-Values:

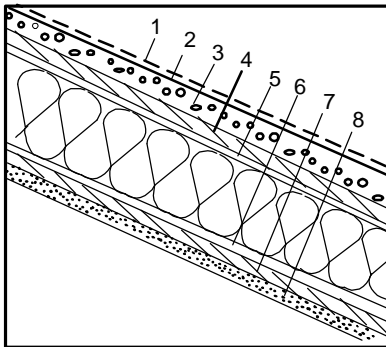
**Framing Adjustment Calculation:**

$$\left[ \frac{1}{1+R_c} \times \left( \frac{1-4/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \frac{1}{1+R_f} \times \left( \frac{4/100}{Fr.\% + 100} \right) \right] = \frac{1/0.058}{1+Total\ U-Value}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.470	0.470
0.800	0.800
-----	3.465
13.956	-----
0.800	0.800
0.470	0.470
0.450	0.450
0.610	0.610
18.226	7.735
$R_c$	$R_f$

**0.058****Total U-Value**

17.288  
**Total R-Value**

**Reference Name: RP.14.2x4.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
48 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 14.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle
2. Building paper
3. 3/4 in polyisocyanurate
4. 3/8 in plywood
5. 7/8 in furring channel
6. 7/8 in furring channel
7. 3/8 in plywood
8. 1/2 in gypsum or plaster board
- Inside Surface Air Film

**Calculation:**

From EZFRAME

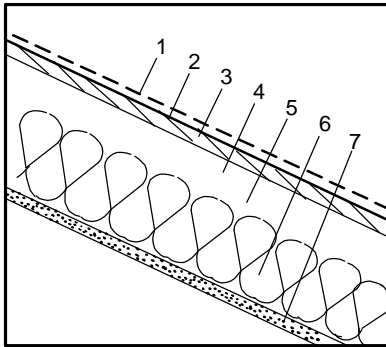
$$\frac{1/0.055}{1+Total\ U-Value}$$

R-Value	
0.170	
0.440	
0.060	
5.250	
0.470	
0.800	
0.800	
0.800	
0.470	
0.620	
<b>0.055</b>	

**Total U-Value**

18.130  
**Total R-Value**



**Reference Name: R.19.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 X 8  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
2. Building paper (felt)
3. 0.50 in plywood
4. 1.0 in air space; heat flow up
5. 2X8 in fir framing
6. R-19 fiberglass insulation
7. 0.50 in gypsum or plaster board
- Inside Surface Air Film

**Total Unadjusted R-Values:**

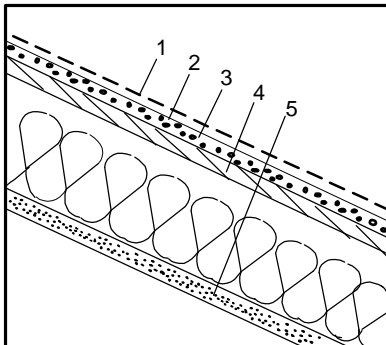
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/22.110}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/9.528}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% +100} \right) \right] = \frac{1/0.051}{1+Total\ U-Value}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.760	-----
-----	7.175
19.000	-----
0.450	0.450
0.610	0.610
22.110	9.528
$R_c$	$R_f$

**0.051****Total U-Value**

19.608

**Total R-Value****Reference Name: R.19.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 8.000  
Actual Width 1.625  
R-value 19.800  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt Shingle
2. Building Paper
3. 1.25 in Polyisocyanurate
4. 0.5 in plywood
5. 0.50 in Gypsum board
- 6.
- 7.
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.051}{1+Total\ U-Value}$$

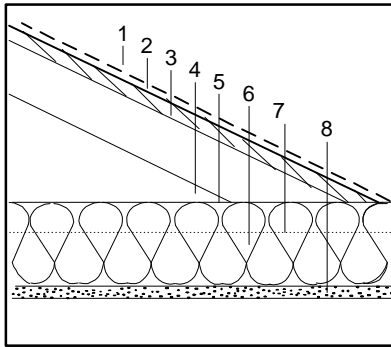
R-Value	
	0.170
	0.440
	0.060
	8.750
	0.630
	0.450
	-----
	-----
	0.620

**0.051****Total U-Value**

19.760

**Total R-Value**



**Reference Name: R.19.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	0.50 in plywood
4.	3.50 in & greater air space; heat flow up
5.	R-8 fiberglass insulation
6.	R-11 fiberglass insulation
7.	2X4 in fir framing
8.	0.50 in gypsum or plaster board
	Inside Surface Air Film

Total Unadjusted R-Values:

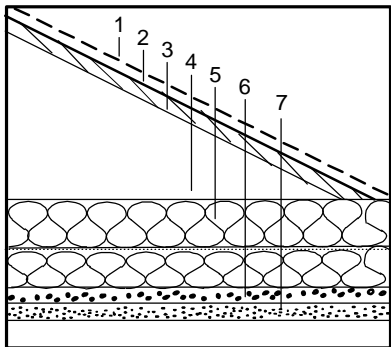
**Framing Adjustment Calculation:**

$$\left[ \frac{1/22.15}{1+R_c} \times \frac{1-7/100}{1-(Fr.\% \div 100)} \right] + \left[ \frac{1/14.615}{1+R_f} \times \frac{7/100}{Fr.\% \div 100} \right] = \frac{1/0.047}{1+Total\ U-Value}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
8.000	8.000
11.000	-----
-----	3.465
0.450	0.450
0.610	0.610
22.150	14.615
$R_c$	$R_f$

**0.047****Total U-Value**

21.277

**Total R-Value****Reference Name: R.19.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 11.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt Roofing
2.	Building paper (felt)
3.	0.625 in Plywood
4.	3.5 in Air, Ceiling
5.	R-8 fiberglass insulation
6.	3/4 in polyisocyanurate
7.	0.50 in Gypsum board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.044}{1+Total\ U-Value}$$

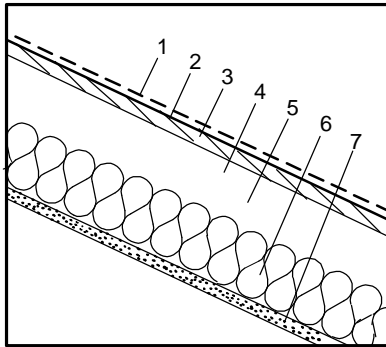
R-Value	
	0.170
	0.150
	0.060
	0.780
	0.800
	8.000
	5.250
	0.450
	0.610

**0.044****Total U-Value**

22.670

**Total R-Value**



**Reference Name: R.22.2x10.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 10  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	0.875 in stucco
2.	Building paper (felt)
3.	3.5" & greater air space; heat sideways
4.	2x4 in fir framing
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

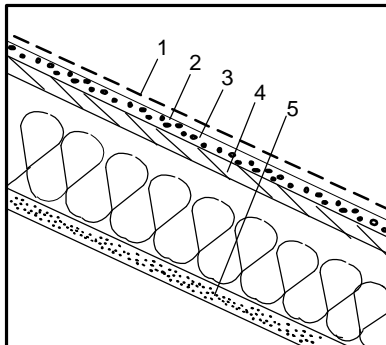
$$\left[ \left( \frac{1/25.14}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \left( \frac{1/11.058}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% + 100} \right) \right] =$$

$$\frac{1/0.045}{1+Total\ U-Value}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.790	-----
-----	9.158
22.000	-----
0.450	0.450
0.610	0.610
25.140	11.058
$R_c$	$R_f$

**0.045****Total U-Value**

22.22  
**Total R-Value**

**Reference Name: R.22.2x10.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 10.000  
Actual Width 1.625  
R-value 22.800  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt Paper
2.	Building paper (felt)
3.	1.50 in polyisocyanurate
4.	0.50 in Plywood
5.	0.50 in gypsum or plaster board
6.	
7.	
	Inside Surface Air Film

**Calculation:**

From EZFRAME

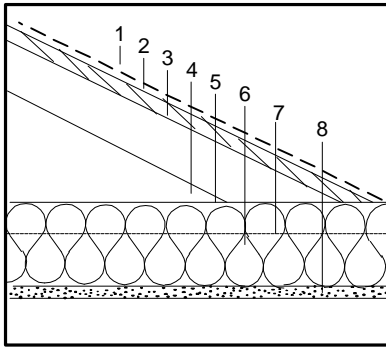
$$\frac{1/0.044}{1+Total\ U-Value}$$

R-Value	
	0.170
	0.440
	0.060
	10.500
	0.630
	0.450
	0.620

**0.044****Total U-Value**

22.660  
**Total R-Value**



**Reference Name: R.22.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 X 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt shingle roofing
2.	Building paper (felt)
3.	0.50 in plywood
4.	3.50 in & greater air space
5.	R-11 fiberglass insulation
6.	R-11 fiberglass insulation
7.	2X4 in fir framing
8.	0.50 in gypsum or plaster board
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

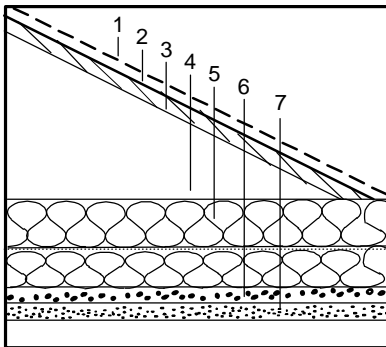
$$\left[ \left( \frac{1/25.15}{1+R_c} \right) \times \left( \frac{1-7/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1/17.615}{1+R_f} \right) \times \left( \frac{7/100}{Fr.\% \div 100} \right) \right] =$$

$$\frac{1/0.041}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
11.000	11.000
11.000	-----
-----	3.465
0.450	0.450
0.610	0.610
25.150	17.615
R <sub>c</sub>	R <sub>f</sub>

**0.041****Total U-Value**

24.390

**Total R-Value****Reference Name: R.22.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 11.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt shingle roofing
2.	Building paper (felt)
3.	0.50 in plywood
4.	3.50 in & greater air space
5.	R-11 fiberglass insulation
6.	0.75 in Polyisocyanurate
7.	0.50 in Gypsum Board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.039}{1+Total\ U-Value}$$

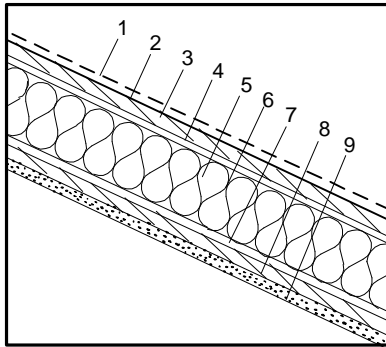
R-Value	
0.170	
0.440	
0.060	
0.630	
0.800	
11.000	
5.250	
0.450	
0.610	

**0.039****Total U-Value**

25.500

**Total R-Value**



**Reference Name: RP.22.2x6.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 6  
48 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt shingle roofing
2.	Building paper (felt)
3.	0.375 in plywood
4.	0.875 in furring channel
5.	5 5/8 in EPS foam insulation
6.	2X6 in fir framing
7.	0.875 in furring channel
8.	0.375 in plywood
9.	0.50 in gypsum or plaster board
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

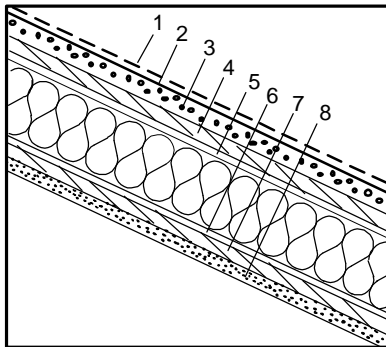
$$\left[ \left( \frac{1/25.926}{1+R_c} \right) \times \left( \frac{1-4/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/10.045}{1+R_f} \right) \times \left( \frac{4/100}{Fr.\% +100} \right) \right]$$

$$\frac{1/0.041}{1+Total\ U-Value}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.470	0.800
0.800	0.800
21.656	-----
-----	5.445
0.800	0.800
0.470	0.470
0.450	0.450
0.610	0.610
25.926	10.045
$R_c$	$R_f$

**0.041****Total U-Value**

24.384  
**Total R-Value**

**Reference Name: RP.22.2x6.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
48 "o.c."  
Actual Depth 6.000  
Actual Width 1.625  
R-value 22.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt Shingle
2.	Building paper (felt)
3.	1.00 in polyisocyanurate
4.	0.375 in Plywood
5.	0.875 in furring channel
6.	0.875 in furring channel
7.	0.375 in Plywood
8.	0.50 in gypsum or plaster board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

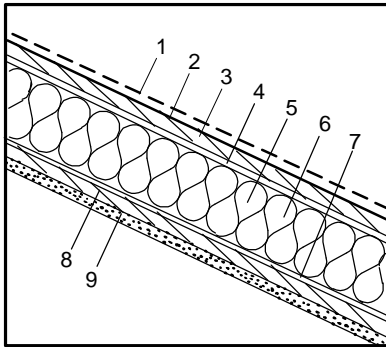
$$\frac{1/0.039}{1+Total\ U-Value}$$

R-Value	
	0.170
	0.440
	0.060
	7.000
	0.470
	0.800
	0.800
	0.470
	0.450
	0.620
	<b>0.039</b>

**Total U-Value**

25.460  
**Total R-Value**



**Reference Name: RP.28.2x8.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 8  
48 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
☒  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt shingle roofing
2.	Building paper (felt)
3.	0.375 in plywood
4.	0.875 in furring channel
5.	7 3/8 in EPS foam insulation @ R-3.85/in
6.	2X8 in fir framing
7.	0.875 in furring channel
8.	0.375 in plywood
9.	0.50 in gypsum or plaster board
	Inside Surface Air Film

Total Unadjusted R-Values:

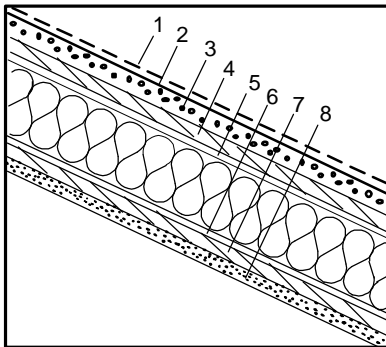
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/32.664}{1+R_c} \right) \times \left( \frac{1-4/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/11.448}{1+R_f} \right) \times \left( \frac{4/100}{Fr.\% +100} \right) \right] = \frac{1/0.033}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.470	0.470
0.800	0.800
28.394	-----
-----	7.178
0.800	0.800
0.470	0.470
0.450	0.450
0.610	0.610
32.664	11.448
R <sub>c</sub>	R <sub>f</sub>

**0.033****Total U-Value**

30.410  
**Total R-Value**

**Reference Name: RP.28.2x8.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
48 "o.c."  
Actual Depth 8.000  
Actual Width 1.625  
R-value 28.394  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt Shingle
2.	Building paper (felt)
3.	1.75 in polyisocyanurate
4.	0.375 in Plywood
5.	0.875 in furring channel
6.	0.875 in furring channel
7.	0.375 in Plywood
8.	0.50 in gypsum or plaster board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

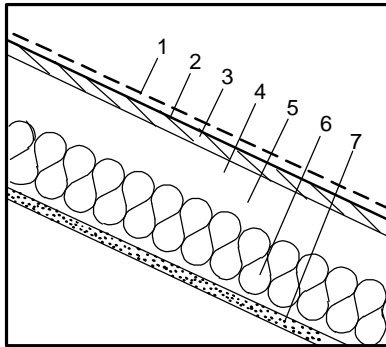
$$\frac{1/0.031}{1+Total\ U-Value}$$

R-Value	
	0.170
	0.440
	0.060
	12.250
	0.470
	0.800
	0.800
	0.470
	0.450
	0.620
	<b>0.031</b>

**Total U-Value**

31.940  
**Total R-Value**



**Reference Name: R.30.2x12.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof

**Wood**

2 × 12  
16 "o.c.

Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)

NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
2. Building paper (felt)
3. 0.50 in plywood
4. 1.75 in air space; heat flow up
5. 2X12 in fir framing
6. R-30 fiberglass insulation
7. 0.50 in gypsum or plaster board
- Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{33.130} \right) \times \left( \frac{1-10/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{13.488} \right) \times \left( \frac{10/100}{1+R_f} \right) \right] = \frac{1/0.034}{1 + \text{Total U-Value}}$$

**R-Value**

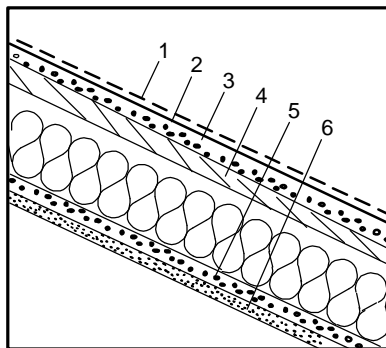
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.780	-----
-----	11.138
30.000	-----
0.450	0.450
0.610	0.610
33.130	13.488
$R_c$	$R_f$

**0.034**

**Total U-Value**

29.412

**Total R-Value**

**Reference Name: R.30.2x12.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof

**Metal**

16 "o.c.  
Actual Depth 12.00  
Actual Width 1.625  
R-value 30.8  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle
2. Building Paper
3. 1.50 in Polyisocyanurate
4. 0.50 in plywood
5. 1.00 in Polyisocyanurate
6. 0.50 in gypsum or plaster board
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.032}{1 + \text{Total U-Value}}$$

**R-Value**

0.170
0.440
0.060
10.50
0.62
7.00
0.45
-----
0.620

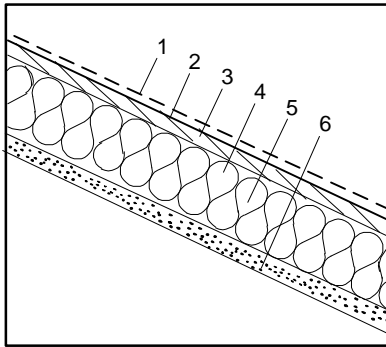
**0.032**

**Total U-Value**

31.64

**Total R-Value**



**Reference Name: R.30.2x10.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 10  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
2. Building paper (felt)
3. 0.50 in plywood
4. 2x10 in fir framing
5. R-30c fiberglass insulation (8.5" thkns)
6. 0.50 in gypsum or plaster board
7. Inside Surface Air Film

Total Unadjusted R-Values:

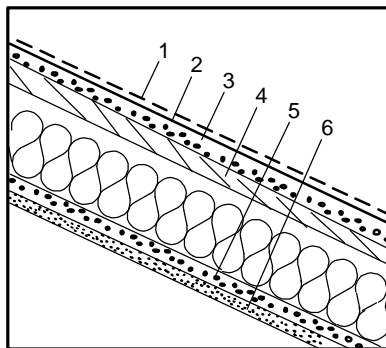
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{32.350} \right) \times \left( \frac{1-10/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{11.508} \right) \times \left( \frac{10/100}{1+R_f} \right) \right] = \frac{1/0.036}{1 + \text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
-----	9.158
30.000	-----
0.450	0.450
0.610	0.610
32.350	11.508
$R_c$	$R_f$

**0.036****Total U-Value**

27.778

**Total R-Value****Reference Name: R.30.2x10.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 10.00  
Actual Width 1.625  
R-value 30.80  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle
2. Building Paper
3. 1.50 in Polyisocyanurate
4. 0.50 in plywood
5. 0.75 in Polyisocyanurate
6. 0.50 in gypsum or plaster board
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.034}{1 + \text{Total U-Value}}$$

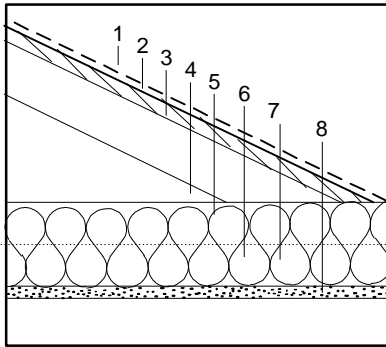
R-Value	
	0.170
	0.440
	0.060
	10.50
	0.62
	5.25
	0.45
	0.620

**0.034****Total U-Value**

29.220

**Total R-Value**



**Reference Name: R.30.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 X 4  
24 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- |    |                                 |
|----|---------------------------------|
|    | Outside Surface Air Film        |
| 1. | Asphalt shingle roofing         |
| 2. | Building paper (felt)           |
| 3. | 0.50 in plywood                 |
| 4. | 3.50 in & greater air space     |
| 5. | R-19 fiberglass insulation      |
| 6. | R-11 fiberglass insulation      |
| 7. | 2X4 in fir framing              |
| 8. | 0.50 in gypsum or plaster board |
|    | Inside Surface Air Film         |

**Total Unadjusted R-Values:**

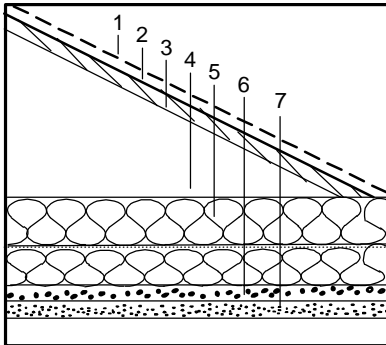
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{33.150} \right) \times \left( \frac{1-7/100}{1-(7\% \div 100)} \right) \right] + \left[ \left( \frac{1}{25.615} \right) \times \left( \frac{7/100}{7\% \div 100} \right) \right] = \frac{1/0.031}{1 \div \text{Total U-Value}}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
19.000	19.000
11.000	-----
-----	3.465
0.450	0.450
0.610	0.610
33.150	25.615
R <sub>c</sub>	R <sub>f</sub>

**0.031****Total U-Value**

32.481

**Total R-Value****Reference Name: R.30.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
24 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 11.00  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- |    |                             |
|----|-----------------------------|
|    | Outside Surface Air Film    |
| 1. | Asphalt shingle roofing     |
| 2. | Building paper (felt)       |
| 3. | 0.50 in plywood             |
| 4. | 3.50 in & greater air space |
| 5. | R-19 fiberglass insulation  |
| 6. | 0.75 in Polyisocyanurate    |
| 7. | 0.50 in Gypsum Board        |
|    | Inside Surface Air Film     |

**Calculation:**

From EZFRAME

$$\frac{1/0.030}{1 \div \text{Total U-Value}}$$

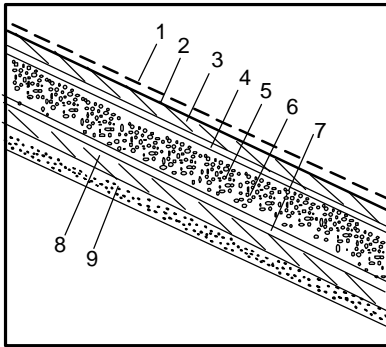
R-Value	
	0.170
	0.440
	0.060
	0.630
	0.800
	19.000
	5.250
	0.450
	0.680

**0.030****Total U-Value**

33.52

**Total R-Value**



**Reference Name: RP.35.2x10.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 10  
48 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt shingle roofing
2.	Building paper (felt)
3.	0.375 in plywood
4.	0.875 furring channel
5.	4 in EPS foam insulation
6.	2x10 in fir framing
7.	0.875 furring channel
8.	0.375 in plywood
9.	0.50 in gypsum or plaster board
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{39.270} \right) \times \left( \frac{1-4/100}{1-R_c} \right) \right] + \left[ \left( \frac{1}{13.426} \right) \times \left( \frac{4/100}{1-R_f} \right) \right]$$

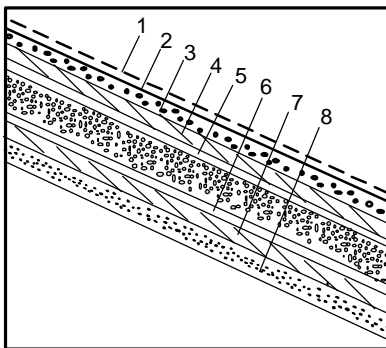
$$\frac{1/0.027}{1+\text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.470	0.470
0.800	0.800
35.000	-----
-----	9.158
0.800	0.800
0.470	0.470
0.450	0.450
0.610	0.610
39.270	13.426
$R_c$	$R_f$

**0.027****Total U-Value**

=

=

$$\frac{37.037}{\text{Total R-Value}}$$
**Reference Name: RP.35.2x10.48**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
48 "o.c."  
Actual Depth 10.000  
Actual Width 1.625  
R-value 35.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt shingle roofing
2.	Building paper (felt)
3.	2.25 in polyisocyanurate
4.	0.375 in plywood
5.	0.875 in furring channel
6.	0.875 in furring channel
7.	0.375 in plywood
8.	0.50 in gypsum or plaster board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.026}{1+\text{Total U-Value}}$$

R-Value	
	0.170
	0.440
	0.060
	15.750
	0.470
	0.800
	0.800
	0.470
	0.450
	0.680
	<b>0.026</b>

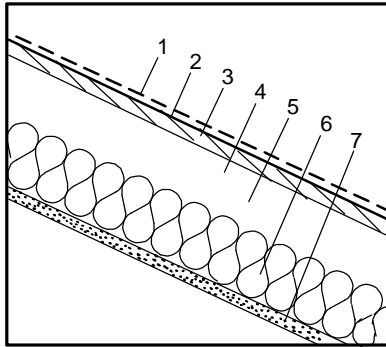
**Total U-Value**

=

=

$$\frac{38.44}{\text{Total R-Value}}$$



**Reference Name: R.38.2x14.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 14  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
2. Building paper (felt)
3. 0.50 in plywood
4. 1.25 in air space; heat flow up
5. 2X14 in fir framing
6. R-38 fiberglass insulation
7. 0.50 in gypsum or plaster board
- Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

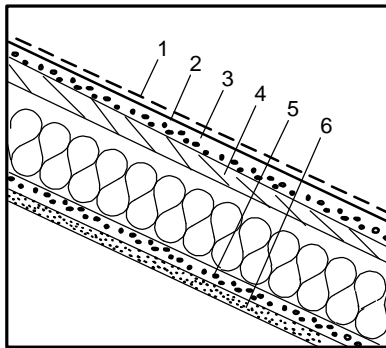
$$\left[ \left( \frac{1}{41.110} \right) \times \left( \frac{1-10/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{15.468} \right) \times \left( \frac{10/100}{1+R_f} \right) \right]$$

$$\frac{1/0.028}{1 + \text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.760	-----
-----	13.118
38.000	-----
0.450	0.450
0.610	0.610
41.110	15.468
$R_c$	$R_f$

**0.028****Total U-Value**

35.714

**Total R-Value****Reference Name: R.38.2x14.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 14.000  
Actual Width 1.625  
R-value 38.800  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt Shingle
2. Building paper (felt)
3. 1.50 in Polyisocyanurate
4. 0.50 in Plywood
5. 1.50 in Polyisocyanurate
6. 0.50 in gypsum or plaster board
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.027}{1 + \text{Total U-Value}}$$

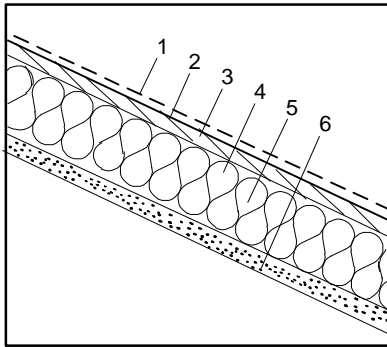
R-Value	
0.170	
0.440	
0.060	
10.500	
0.630	
10.500	
0.450	
-----	
0.620	

**0.027****Total U-Value**

36.95

**Total R-Value**



**Reference Name: R.38.2x12.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof  
**Wood**  
2 × 12  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt shingle roofing
  2. Building paper (felt)
  3. 0.50 in plywood
  4. 2X12 in fir framing
  5. R-38 fiberglass insulation
  6. 0.50 in gypsum or plaster board
  7. Inside Surface Air Film

Total Unadjusted R-Values:

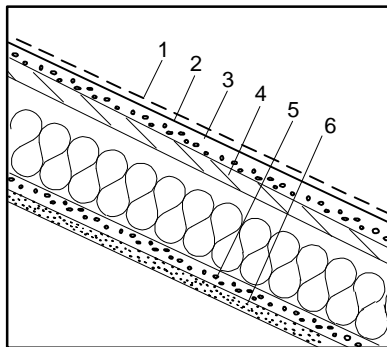
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{39.350} \right) \times \left( \frac{1-10/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{13.488} \right) \times \left( \frac{10/100}{1+R_f} \right) \right] = \frac{1/0.030}{1+\text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
-----	11.138
37.000	-----
0.450	0.450
0.610	0.610
39.350	13.488
$R_c$	$R_f$

**0.030****Total U-Value**

33.333

**Total R-Value****Reference Name: R.38.2x12.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 12.000  
Actual Width 1.625  
R-value 38.800  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Asphalt Shingle
  2. Building paper (felt)
  3. 1.50 in polyisocyanurate
  4. 0.625 in plywood
  5. 1.00 in polyisocyanurate
  6. 0.625 in gypsum or plaster board
  7. Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.030}{1+\text{Total U-Value}}$$

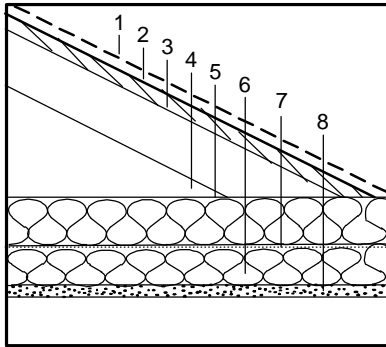
R-Value	
0.170	
0.440	
0.060	
10.50	
0.780	
7.00	
0.560	
0.620	

**0.030****Total U-Value**

33.38

**Total R-Value**



**Reference Name: R.38.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
 Wall  
☒ Ceiling/Roof  
**Wood**  
 2 × 4  
 24 "o.c.  
 Wall: 15% (16"o.c.)  
 12% (24"o.c.)  
 9% (48"o.c.)  
 Floor/Ceiling: 10% (16"o.c.)  
 7% (24"o.c.)  
 4% (48"o.c.)  
 NA

**List of Construction Components**

- Outside Surface Air Film
- Asphalt shingle roofing
  - Building paper (felt)
  - 0.50 in plywood
  - 3.50 in & greater air space; heat flow up
  - R-27 fiberglass insulation
  - R-11 fiberglass insulation
  - 2X4 in fir framing
  - 0.50 in gypsum or plaster board
- Inside Surface Air Film

Total Unadjusted R-Values:

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
27.000	27.000
11.000	-----
-----	3.465
0.450	0.450
0.610	0.610
41.150	33.615
$R_c$	$R_f$

**Framing Adjustment Calculation:**

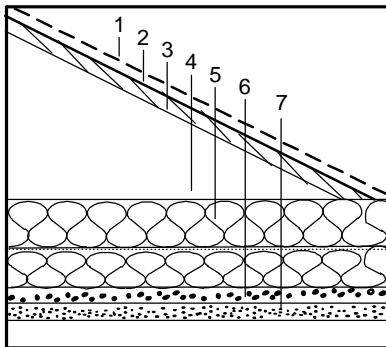
$$\left[ \left( \frac{1}{41.150} \right) \times \left( \frac{1-7/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1}{33.615} \right) \times \left( \frac{7/100}{Fr.\% \div 100} \right) \right] =$$

$$\frac{1/0.024}{1 \div \text{Total U-Value}} =$$

$$= \frac{0.024}{41.667} =$$

**Total U-Value**

**Total R-Value**

**Reference Name: R.38.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**
**Cavity Insulation:****Insulation Tape R-value:**

Floor  
 Wall  
☒ Ceiling/Roof  
**Metal**  
 24 "o.c.  
 Actual Depth 3.625  
 Actual Width 1.625  
 R-value 11.00  
 Knock-out (%) 15.000  
 Web Thickness 0.060  
 Interior Flange  
 Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
- Asphalt Shingle
  - Building paper (felt)
  - 0.50 in Plywood
  - 3.50 in & greater air space; heat flow up
  - R-27 fiberglass insulation
  - 1.00 in polyisocyanurate
  - 0.50 in gypsum or plaster board
- Inside Surface Air Film

R-Value	
	0.170
	0.440
	0.060
	0.630
	0.800
	27.00
	7.00
	0.450
	0.610

**Calculation:**

From EZFRAME

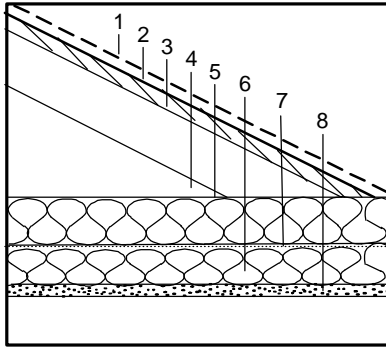
$$\frac{1/0.023}{1 \div \text{Total U-Value}} =$$

$$= \frac{0.023}{43.25} =$$

**Total U-Value**

**Total R-Value**



**Reference Name: R.49.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

Floor  
Wall  
☒ Ceiling/Roof

**Wood**  
2 X 4  
16 "o.c."

Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)

NA

**List of Construction Components**

- |    |   |
|----|---|
|    | Outside Surface Air Film                  |
| 1. | Asphalt shingle roofing                   |
| 2. | Building paper (felt)                     |
| 3. | 0.50 in plywood                           |
| 4. | 3.50 in & greater air space; heat flow up |
| 5. | R-38 fiberglass insulation                |
| 6. | R-11 fiberglass insulation                |
| 7. | 2X4 in fir framing                        |
| 8. | 0.50 in gypsum or plaster board           |
|    | Inside Surface Air Film                   |

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{52.150} \right) \times \left( \frac{1-10/100}{1} \right) \right] + \left[ \left( \frac{1}{44.615} \right) \times \left( \frac{10/100}{1} \right) \right] = \frac{1/0.019}{1 + \text{Total U-Value}}$$

**R-Value**

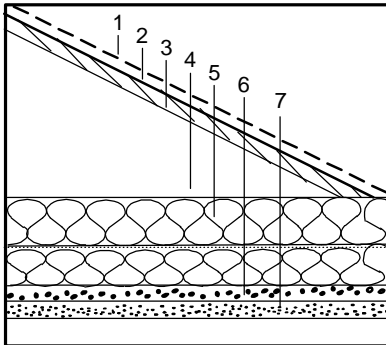
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
38.000	38.000
11.000	-----
-----	3.465
0.450	0.450
0.610	0.610
52.150	44.615
R <sub>c</sub>	R <sub>f</sub>

**0.019**

**Total U-Value**

52.632

**Total R-Value**

**Reference Name: R.49.2x4.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

Floor  
Wall  
☒ Ceiling/Roof

**Metal**  
16 "o.c."  
Actual Depth 3.625  
Actual Width 1.625  
R-value 11.00  
Knock-out (%) 15.00  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- |    |                                 |
|----|---------------------------------|
|    | Outside Surface Air Film        |
| 1. | Asphalt shingle                 |
| 2. | 0.50 in plywood                 |
| 3. | 3.50 in air space               |
| 4. | R-38 fiberglass insulation      |
| 5. | 1.00 in polyisocyanurate        |
| 6. | 0.50 in gypsum or plaster board |
| 7. | Inside Surface Air Film         |

**Calculation:**

From EZFRAME

$$\frac{1/0.019}{1 + \text{Total U-Value}}$$

**R-Value**

0.170
0.440
0.630
0.800
38.00
7.000
0.450
0.610

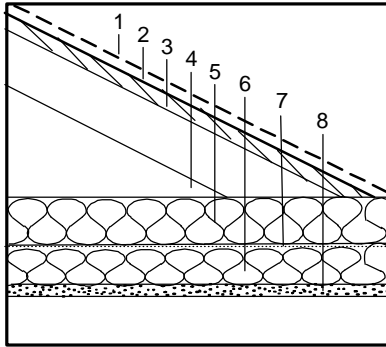
**0.019**

**Total U-Value**

53.02

**Total R-Value**



**Reference Name: R.49.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

☐ Floor  
☐ Wall  
☒ Ceiling/Roof

**Framing Material:**
**Wood**
**Framing Size:**
 2  ×  4

**Framing Spacing:**
 24  "o.c.

**Framing Percentage:**  
(check one)

Wall:  15% (16"o.c.)  
 12% (24"o.c.)  
 9% (48"o.c.)  
 Floor/Ceiling:  10% (16"o.c.)  
☒ 7% (24"o.c.)  
 4% (48"o.c.)

**Wall Weight / sf:**  
(Packages only)

NA

**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt shingle roofing
2.	Building paper (felt)
3.	0.50 in plywood
4.	3.50 in & greater air space; heat flow up
5.	R-38 fiberglass insulation
6.	R-11 fiberglass insulation
7.	2X4 in fir framing
8.	0.50 in gypsum or plaster board
	Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

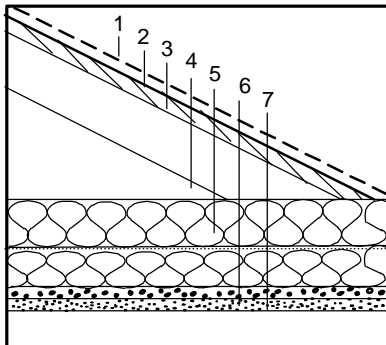
$$\left[ \left( \frac{1}{52.15} \right) \times \left( \frac{1-7/100}{1-(7\%+100)} \right) \right] + \left[ \left( \frac{1}{44.615} \right) \times \left( \frac{7/100}{7\%+100} \right) \right] =$$

$$\frac{1/0.019}{1+\text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
0.440	0.440
0.060	0.060
0.620	0.620
0.800	0.800
38.000	38.000
11.000	-----
-----	3.465
0.450	0.450
0.610	0.610
52.150	44.615
$R_c$	$R_f$

**0.019****Total U-Value**

52.632

**Total R-Value****Reference Name: R.49.2x4.24**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

☐ Floor  
☐ Wall  
☒ Ceiling/Roof

**Framing Material:**
**Metal**
**Framing Spacing:**
 24  "o.c.

**Framing Size:**
 Actual Depth  3.625

 Actual Width  1.625

**Cavity Insulation:**
 R-value  11.00

 Knock-out (%)  15.00

 Web Thickness  0.060

**Insulation Tape R-value:**
 Interior Flange

 Exterior Flange
**List of Construction Components**

	Outside Surface Air Film
1.	Asphalt Shingle
2.	Building paper (felt)
3.	0.50 in Plywood
4.	3.50 in & greater air space; heat flow up
5.	R-38 fiberglass insulation
6.	0.25 in Polyisocyanurate
7.	0.75 in gypsum or plaster board
	Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.018}{1+\text{Total U-Value}}$$

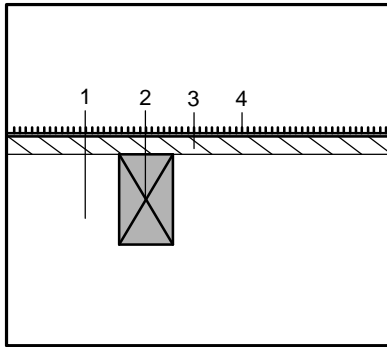
R-Value	
	0.170
	0.440
	0.060
	0.630
	0.800
	38.000
	1.750
	0.680
	0.610

**0.018****Total U-Value**

54.250

**Total R-Value**



Reference Name: **FC.0.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Size:

Framing Spacing:

Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)
☒ Floor  
☐ Wall  
☐ Ceiling/Roof
**Wood**

2 × 6

16 "o.c.

Wall: 15% (16" o.c.)

12% (24" o.c.)

9% (48" o.c.)

Floor/Ceiling: ☒ 10% (16" o.c.)

7% (24" o.c.)

4% (48" o.c.)

NA

**List of Construction Components**

1. Outside Surface Air Film
2. Effective R-value of vented crawlspace
3. 2X6 in fir framing
4. 0.625 in plywood
5. Carpet & Pad
- 6.
- 7.

Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

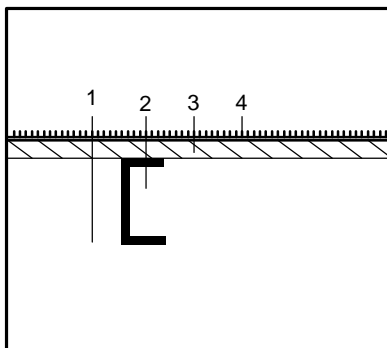
$$\left[ \left( \frac{1/9.940}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/15.385}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% +100} \right) \right]$$

$$\frac{1/0.097}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
6.000	6.000
-----	5.445
0.770	0.770
2.080	2.080
0.920	0.920
3.940	9.385
R <sub>c</sub>	R <sub>f</sub>

**0.097****Total U-Value**

10.309

**Total R-Value**Reference Name: **FC.0.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Spacing:

Framing Size:

Cavity Insulation:

Insulation Tape R-value:

☒ Floor  
☐ Wall  
☐ Ceiling/Roof
**Metal**

16 "o.c.

Actual Depth 6.000

Actual Width 1.625

R-value 0.800

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**List of Construction Components**

1. Outside Surface Air Film
2. Effective R-value of vented crawlspace
3. 0.625 in plywood
4. Carpet & Pad
- 5.
- 6.
- 7.

Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.094}{1+Total\ U-Value}$$

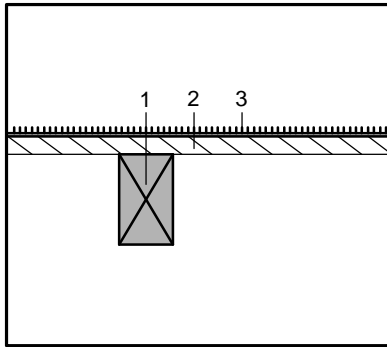
R-Value	
0.170	
6.000	
0.780	
2.080	
0.920	

**0.094****Total U-Value**

10.680

**Total R-Value**



Reference Name: **FX.0.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)
☒ Floor  
☐ Wall  
☐ Ceiling/Roof

Framing Material:

**Wood**

Framing Size:

2 × 6

Framing Spacing:

16 "o.c."

Framing Percentage:  
(check one)

Wall: ☐ 15% (16"o.c.)  
☐ 12% (24"o.c.)  
☐ 9% (48"o.c.)  
 Floor/Ceiling: ☒ 10% (16"o.c.)  
☐ 7% (24"o.c.)  
☐ 4% (48"o.c.)

Wall Weight / sf:  
(Packages only)

NA

**List of Construction Components**

- Outside Surface Air Film
1. 2X6 in fir framing
  2. 0.625 in plywood
  3. Carpet & Pad
  4. \_\_\_\_\_
  5. \_\_\_\_\_
  6. \_\_\_\_\_
  7. \_\_\_\_\_
- Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

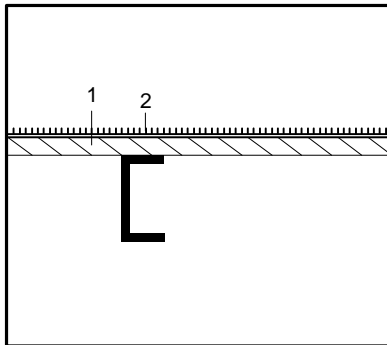
$$\left[ \left( \frac{1/3.940}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\%+100)} \right) \right] + \left[ \left( \frac{1/9.385}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\%+100} \right) \right] =$$

$$\frac{1/0.241}{1+Total\ U-Value} =$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
-----	5.445
0.770	0.770
2.080	2.080
_____	_____
_____	_____
_____	_____
0.920	0.920
3.940	9.385
$R_c$	$R_f$

**0.241****Total U-Value**

4.150

**Total R-Value**Reference Name: **FX.0.2x6.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)
☒ Floor  
☐ Wall  
☐ Ceiling/Roof

Framing Material:

**Metal**

Framing Spacing:

16 "o.c."

Framing Size:

Actual Depth 6.000

Actual Width 1.625

R-value 0.800

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange \_\_\_\_\_

Exterior Flange \_\_\_\_\_

Insulation Tape R-value:

**List of Construction Components**

- Outside Surface Air Film
1. 0.625 in plywood
  2. Carpet & pad
  3. \_\_\_\_\_
  4. \_\_\_\_\_
  5. \_\_\_\_\_
  6. \_\_\_\_\_
  7. \_\_\_\_\_
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.253}{1+Total\ U-Value} =$$

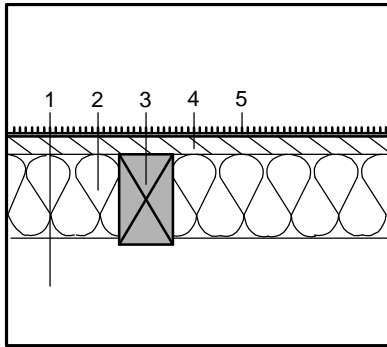
R-Value	
0.170	
0.780	
2.08	
_____	
_____	
_____	
0.920	

**0.253****Total U-Value**

3.950

**Total R-Value**



**Reference Name: FC.11.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Wood**

2 X 6

16 "o.c.

Wall: 15% (16" o.c.)

12% (24" o.c.)

9% (48" o.c.)

Floor/Ceiling: ☒ 10% (16" o.c.)

7% (24" o.c.)

4% (48" o.c.)

NA

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. R-11 fiberglass insulation
3. 2X6 in fir framing
4. 0.625 in plywood
5. Carpet & pad
- 6.
- 7.
- Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/20.940}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1/15.385}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% \div 100} \right) \right] =$$

$$\frac{1/0.050}{1+Total\ U-Value}$$

**R-Value**

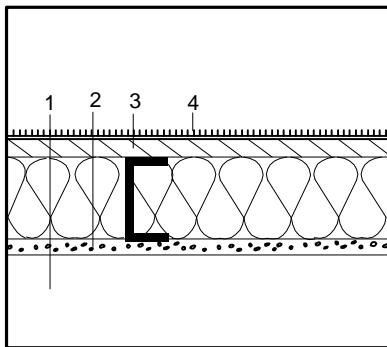
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
6.000	6.000
11.000	-----
-----	5.445
0.770	0.770
2.080	2.080
-----	-----
0.920	0.920
20.940	15.385
$R_c$	$R_f$

**0.050**

**Total U-Value**

20.00

**Total R-Value**

**Reference Name: FC.11.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Spacing:**

**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Metal**

16 "o.c.

Actual Depth 6.000

Actual Width 1.625

R-value 11.000

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. 0.75 in polyisocyanurate
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
- 7.
- Inside Surface Air Film

**Calculation:**

From EZFRAME

**R-Value**

0.170

6.000

5.250

0.780

2.080

-----

-----

0.920

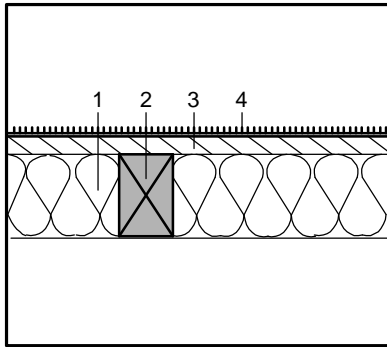
**0.048**

**Total U-Value**

21.030

**Total R-Value**



**Reference Name: FX.11.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Wood**

2 X 6

16 "o.c."

Wall: 15% (16" o.c.)

12% (24" o.c.)

9% (48" o.c.)

Floor/Ceiling: ☒ 10% (16" o.c.)

7% (24" o.c.)

4% (48" o.c.)

NA

**List of Construction Components**

1. Outside Surface Air Film
2. R-11 fiberglass insulation
3. 2X6 in fir framing
4. 0.625 in Plywood
5. Carpet & pad
- 6.
7. Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{14.940} \right) \times \left( \frac{1-10}{100} \right) \right] + \left[ \left( \frac{1}{9.385} \right) \times \left( \frac{10}{100} \right) \right] = \frac{1}{0.071}$$

1+Total U-Value

**R-Value**

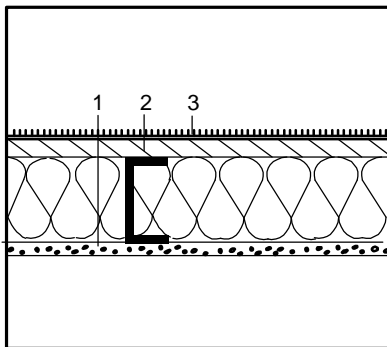
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
11.000	-----
-----	5.445
0.770	0.770
2.080	2.080
-----	-----
-----	-----
0.920	0.920
14.940	9.385
R <sub>c</sub>	R <sub>f</sub>

**0.071**

**Total U-Value**

14.085

**Total R-Value**

**Reference Name: FX.11.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Spacing:**

**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Metal**

16 "o.c."

Actual Depth 6.000

Actual Width 1.625

R-value 11.000

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**List of Construction Components**

1. Outside Surface Air Film
2. 0.75 in polyisocyanurate
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1}{0.071} = \frac{1}{1+Total U-Value}$$

**R-Value**

0.170

5.250

0.780

2.080

-----

-----

-----

0.920

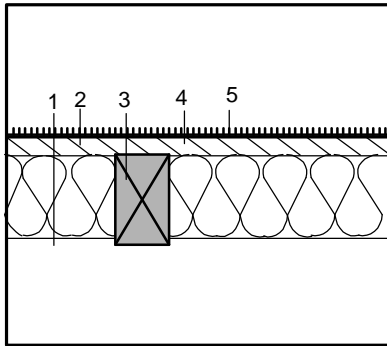
**0.071**

**Total U-Value**

14.16

**Total R-Value**



**Reference Name: FC.13.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

✓ Floor  
Wall  
Ceiling/Roof  
**Wood**  
2 × 6  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ✓ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-Value of vented crawlspace
2. R-13 fiberglass insulation
3. 2X6 in fir framing
4. 0.625 in plywood
5. Carpet & pad
- 6.
- 7.
- Inside Surface Air Film

Total Unadjusted R-Values:

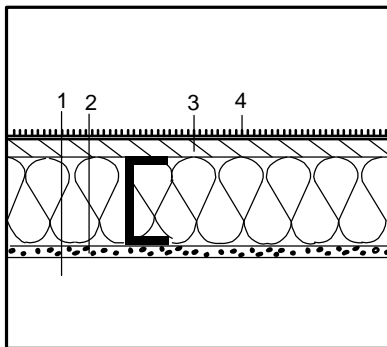
**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{22.94} \right) \times \left( \frac{1-10/100}{1-R_c} \right) \right] + \left[ \left( \frac{1}{15.385} \right) \times \left( \frac{10/100}{1-R_f} \right) \right] = \frac{1/0.046}{1+\text{Total U-Value}}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
6.000	6.000
13.000	-----
-----	5.445
0.770	0.770
2.080	2.080
-----	-----
0.920	0.920
22.940	15.385
R <sub>c</sub>	R <sub>f</sub>

**0.046****Total U-Value**

21.740

**Total R-Value****Reference Name: FC.13.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

✓ Floor  
Wall  
Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 6.000  
Actual Width 1.625  
R-value 13.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-Value of vented crawlspace
2. 1.00 in polyisocyanurate
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
- 7.
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.043}{1+\text{Total U-Value}}$$

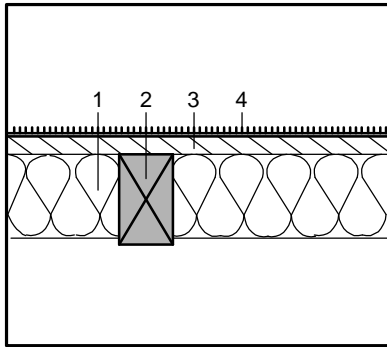
R-Value	
0.170	
6.000	
7.000	
0.780	
2.080	
-----	
0.920	

**0.043****Total U-Value**

23.340

**Total R-Value**



**Reference Name: FX.13.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

✓ Floor  
Wall  
Ceiling/Roof  
**Wood**  
2 × 6  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ✓ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. R-13 fiberglass insulation
2. 2X6 in fir framing
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
7. Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

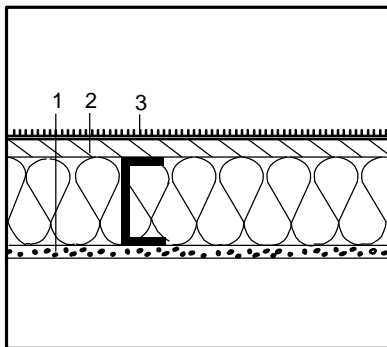
$$\left[ \left( \frac{1/16.940}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/9.385}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% +100} \right) \right] =$$

$$\frac{1/0.064}{1+Total\ U-Value}$$

R-Value	
Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
13.000	-----
-----	5.445
0.770	0.770
2.080	2.080
-----	-----
0.920	0.920
16.940	9.385
R <sub>c</sub>	R <sub>f</sub>

**0.064****Total U-Value**

15.625  
**Total R-Value**

**Reference Name: FX.13.2x6.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

✓ Floor  
Wall  
Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 6.000  
Actual Width 1.625  
R-value 13.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. 1.00 in polyisocyanurate
2. 0.625 in plywood
3. Carpet & pad
- 4.
- 5.
- 6.
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

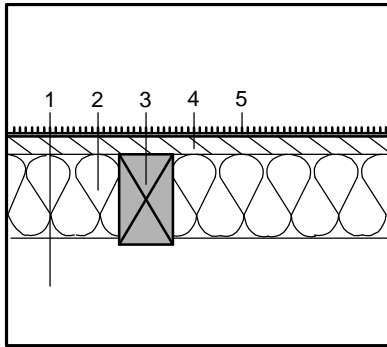
$$\frac{1/0.058}{1+Total\ U-Value}$$

R-Value	
0.170	
7.000	
0.780	
2.080	
-----	
0.920	

**0.058****Total U-Value**

17.340  
**Total R-Value**



**Reference Name:** **FC.19.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)
☒ Floor  
☐ Wall  
☐ Ceiling/Roof
**Framing Material:****Wood****Framing Size:**

2 × 8

**Framing Spacing:**

16 "o.c."

**Framing Percentage:**  
(check one)

Wall: ☐ 15% (16"o.c.)  
☐ 12% (24"o.c.)  
☐ 9% (48"o.c.)  
Floor/Ceiling: ☒ 10% (16"o.c.)  
☐ 7% (24"o.c.)  
☐ 4% (48"o.c.)

**Wall Weight / sf:**  
(Packages only)

NA

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. R-19 fiberglass insulation
3. 7.25 in fir framing
4. 0.625 in plywood
5. Carpet & pad
- 6.
- 7.
- Inside Surface Air Film

**Total Unadjusted R-Values:****Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/14.535}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1/17.118}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% \div 100} \right) \right] =$$

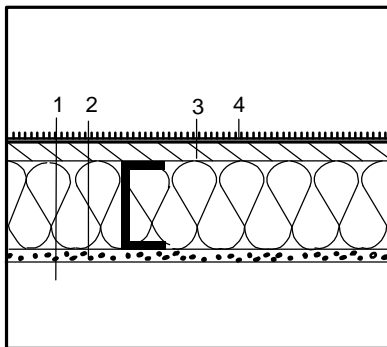
$$\frac{1/0.037}{1+Total\ U-Value}$$

**R-Value**

Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
6.000	6.000
19.000	-----
-----	7.178
0.770	0.770
2.080	2.080
-----	-----
0.920	0.920
28.940	17.118
$R_c$	$R_f$

**0.037****Total U-Value**

27.027

**Total R-Value****Reference Name:** **FC.19.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)
☒ Floor  
☐ Wall  
☐ Ceiling/Roof
**Framing Material:****Metal****Framing Spacing:**

16 "o.c."

**Framing Size:**

Actual Depth 8.00

Actual Width 1.625

R-value 19.000

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**Insulation Tape R-value:****List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. 1.50 in polyisocyanurate
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
- 7.
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.035}{1+Total\ U-Value}$$

**R-Value**

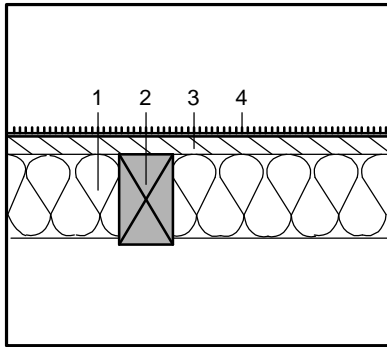
0.170
6.000
10.500
0.780
2.080
-----
-----
0.920

**0.035****Total U-Value**

28.700

**Total R-Value**



**Reference Name: FX.19.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Size:**  
**Framing Spacing:**  
**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

✓ Floor  
Wall  
Ceiling/Roof  
**Wood**  
2 × 8  
16 "o.c."  
Wall: 15% (16"o.c.)  
12% (24"o.c.)  
9% (48"o.c.)  
Floor/Ceiling: ✓ 10% (16"o.c.)  
7% (24"o.c.)  
4% (48"o.c.)  
NA

**List of Construction Components**

- Outside Surface Air Film
1. R-19 fiberglass insulation
2. 7.25 in fir framing
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
7. Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/22.940}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% \div 100)} \right) \right] + \left[ \left( \frac{1/11.118}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% \div 100} \right) \right] =$$

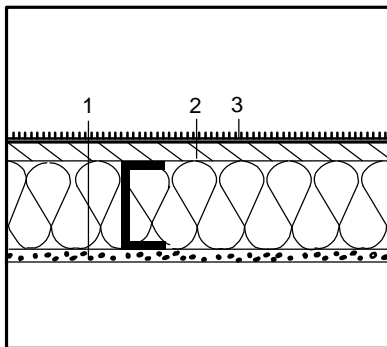
$$\frac{1/0.049}{1+Total\ U-Value}$$

**R-Value**

Cavity (R <sub>c</sub> )	Frame (R <sub>f</sub> )
0.170	0.170
19.000	-----
-----	7.178
0.770	0.770
2.080	2.080
-----	-----
-----	-----
0.920	0.920
22.940	11.118
R <sub>c</sub>	R <sub>f</sub>

**0.049****Total U-Value**

20.408

**Total R-Value****Reference Name: FX.19.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**  
**Framing Spacing:**  
**Framing Size:**

**Cavity Insulation:****Insulation Tape R-value:**

✓ Floor  
Wall  
Ceiling/Roof  
**Metal**  
16 "o.c."  
Actual Depth 8.00  
Actual Width 1.625  
R-value 19.000  
Knock-out (%) 15.000  
Web Thickness 0.060  
Interior Flange  
Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. 1.25 in polyisocyanurate
2. 0.625 in plywood
3. Carpet & pad
- 4.
- 5.
- 6.
7. Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.048}{1+Total\ U-Value}$$

**R-Value**

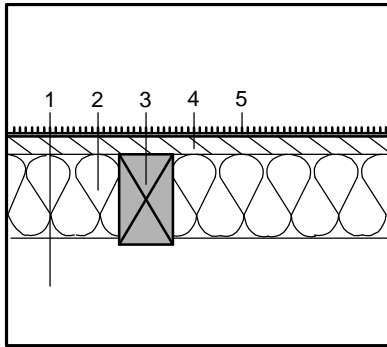
0.170
8.750
0.780
2.080
-----
-----
-----
0.920

**0.048****Total U-Value**

20.950

**Total R-Value**



**Reference Name: FC.21.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Wood**

2 × 8

16 "o.c.

Wall: 15% (16" o.c.)

12% (24" o.c.)

9% (48" o.c.)

Floor/Ceiling: ☒ 10% (16" o.c.)

7% (24" o.c.)

4% (48" o.c.)

NA

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. R-21 fiberglass insulation
3. 7.25 in fir framing
4. 0.625 in plywood
5. Carpet & pad
- 6.
- 7.
- Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/30.940}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% +100)} \right) \right] + \left[ \left( \frac{1/17.118}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% +100} \right) \right]$$

$$\frac{1/0.035}{1+\text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
6.000	6.000
21.000	-----
-----	7.178
0.770	0.770
2.080	2.080
-----	-----
0.920	0.920
30.940	17.118
$R_c$	$R_f$

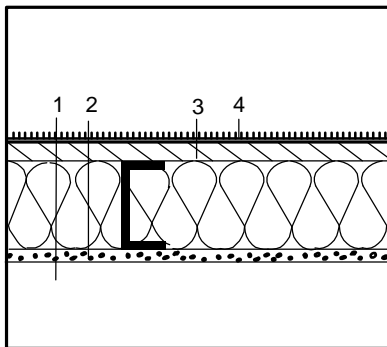
**0.035**

**Total U-Value**

=

=

**28.571**  
**Total R-Value**

**Reference Name: FC.21.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Spacing:**

**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Metal**

16 "o.c.

Actual Depth 8.00

Actual Width 1.625

R-value 21.000

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. 1.50 in polyisocyanurate
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
- 7.
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.034}{1+\text{Total U-Value}}$$

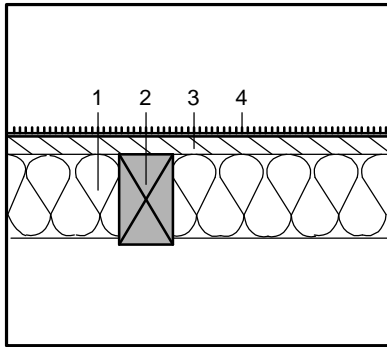
=

=

**0.034**  
**Total U-Value**

**29.080**  
**Total R-Value**



**Reference Name: FX.21.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Wood**

2 × 8

16 "o.c.

Wall: 15% (16" o.c.)

12% (24" o.c.)

9% (48" o.c.)

Floor/Ceiling: ☒ 10% (16" o.c.)

7% (24" o.c.)

4% (48" o.c.)

NA

**List of Construction Components**

- Outside Surface Air Film
1. R-19 fiberglass insulation
2. 7.25 in fir framing
3. 0.625 in plywood
4. Carpet & pad
5. \_\_\_\_\_
6. \_\_\_\_\_
7. \_\_\_\_\_
- Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1}{24.950} \right) \times \left( \frac{1-10/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{11.128} \right) \times \left( \frac{10/100}{1+R_f} \right) \right]$$

$$\frac{1/0.045}{1+\text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
21.000	-----
-----	7.178
0.780	0.780
2.080	2.080
-----	-----
-----	-----
0.920	0.920
22.950	11.128
$R_c$	$R_f$

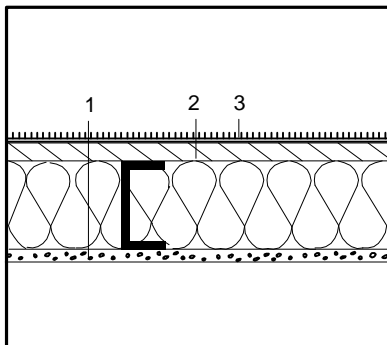
**0.045**

**Total U-Value**

=

=

**22.220**  
**Total R-Value**

**Reference Name: FX.21.2x8.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Spacing:**

**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Metal**

16 "o.c.

Actual Depth 8.00

Actual Width 1.625

R-value 21.000

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. 1.50 in polyisocyanurate
2. 0.625 in plywood
3. Carpet & pad
4. \_\_\_\_\_
5. \_\_\_\_\_
6. \_\_\_\_\_
7. \_\_\_\_\_
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.043}{1+\text{Total U-Value}}$$

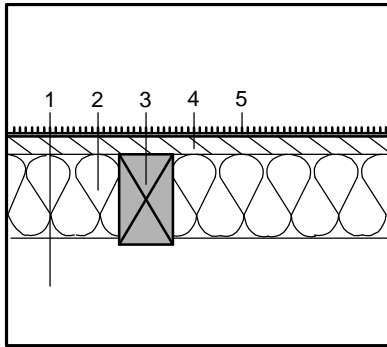
=

=

**0.043**  
**Total U-Value**

**23.080**  
**Total R-Value**



**Reference Name: FC.30.2x10.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Size:**

**Framing Spacing:**

**Framing Percentage:**  
(check one)

**Wall Weight / sf:**  
(Packages only)

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Wood**

2 × 8

16 "o.c.

Wall: 15% (16" o.c.)

12% (24" o.c.)

9% (48" o.c.)

Floor/Ceiling: ☒ 10% (16" o.c.)

7% (24" o.c.)

4% (48" o.c.)

NA

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. R-30 fiberglass insulation
3. 9.25 in fir framing
4. 0.625 in plywood
5. Carpet & pad
- 6.
- 7.
- Inside Surface Air Film

**Total Unadjusted R-Values:**

**Framing Adjustment Calculation:**

$$\left[ \left( \frac{1/39.940}{1+R_c} \right) \times \left( \frac{1-10/100}{1-(Fr.\% + 100)} \right) \right] + \left[ \left( \frac{1/19.098}{1+R_f} \right) \times \left( \frac{10/100}{Fr.\% + 100} \right) \right]$$

$$\frac{1/0.028}{1 + \text{Total U-Value}}$$

**R-Value**

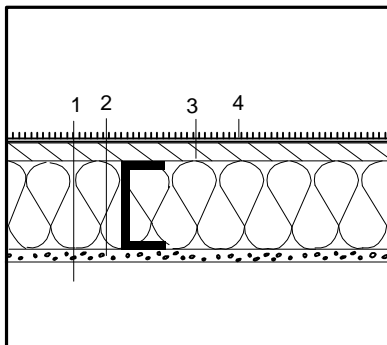
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
6.000	6.000
30.000	-----
-----	9.158
0.770	0.770
2.080	2.080
-----	-----
0.920	0.920
39.940	19.098
$R_c$	$R_f$

**0.028**

**Total U-Value**

35.714

**Total R-Value**

**Reference Name: FC.30.2x10.16**

Sketch of Construction Assembly

**Assembly Type:**  
(check one)

**Framing Material:**

**Framing Spacing:**

**Framing Size:**

**Cavity Insulation:**

**Insulation Tape R-value:**

☒ Floor  
☐ Wall  
☐ Ceiling/Roof

**Metal**

16 "o.c.

Actual Depth 10.000

Actual Width 1.625

R-value 30.000

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. Effective R-value of vented crawlspace
2. 2.50 in polyisocyanurate
3. 0.625 in plywood
4. Carpet & pad
- 5.
- 6.
- 7.
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.026}{1 + \text{Total U-Value}}$$

**R-Value**

0.170
6.000
17.50
0.780
2.080
-----
-----
0.920

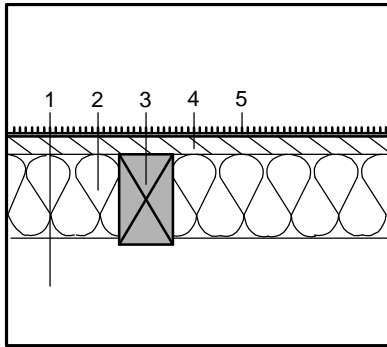
**0.026**

**Total U-Value**

38.110

**Total R-Value**



Reference Name: **FX.30.2x10.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Size:

Framing Spacing:

Framing Percentage:  
(check one)Wall Weight / sf:  
(Packages only)
☒ Floor  
☐ Wall  
☐ Ceiling/Roof
**Wood**

2 × 8

16 "o.c.

Wall: 15% (16" o.c.)

12% (24" o.c.)

9% (48" o.c.)

Floor/Ceiling: ☒ 10% (16" o.c.)

7% (24" o.c.)

4% (48" o.c.)

NA

**List of Construction Components**

- Outside Surface Air Film
1. R-30 fiberglass insulation
2. 9.25 in fir framing
3. 0.625 in plywood
4. Carpet & pad
5. \_\_\_\_\_
6. \_\_\_\_\_
7. \_\_\_\_\_
- Inside Surface Air Film

Total Unadjusted R-Values:

**Framing Adjustment Calculation:**

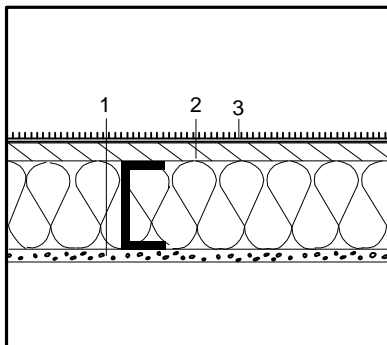
$$\left[ \left( \frac{1}{33.940} \right) \times \left( \frac{1-10/100}{1+R_c} \right) \right] + \left[ \left( \frac{1}{13.098} \right) \times \left( \frac{10/100}{1+R_f} \right) \right]$$

$$\frac{1/0.034}{1+\text{Total U-Value}}$$

R-Value	
Cavity ( $R_c$ )	Frame ( $R_f$ )
0.170	0.170
30.000	-----
-----	9.158
0.770	0.770
2.080	2.080
-----	-----
-----	-----
0.920	0.920
39.940	19.098
$R_c$	$R_f$

**0.034****Total U-Value**

29.412

**Total R-Value**Reference Name: **FX.30.2x10.16**

Sketch of Construction Assembly

Assembly Type:  
(check one)

Framing Material:

Framing Spacing:

Framing Size:

Cavity Insulation:

Insulation Tape R-value:

☒ Floor  
☐ Wall  
☐ Ceiling/Roof
**Metal**

16 "o.c.

Actual Depth 10.000

Actual Width 1.625

R-value 38.000

Knock-out (%) 15.000

Web Thickness 0.060

Interior Flange

Exterior Flange

**List of Construction Components**

- Outside Surface Air Film
1. 2.50 in polyisocyanurate
2. 0.625 in plywood
3. Carpet & pad
4. \_\_\_\_\_
5. \_\_\_\_\_
6. \_\_\_\_\_
7. \_\_\_\_\_
- Inside Surface Air Film

**Calculation:**

From EZFRAME

$$\frac{1/0.031}{1+\text{Total U-Value}}$$

R-Value	
0.170	
17.50	
0.780	
2.080	
-----	
-----	
-----	
0.920	

**0.031****Total U-Value**

32.110

**Total R-Value**



Table E-8

## DEFAULT FENESTRATION PRODUCT U-VALUES

<u>Frame Type</u> <sup>1</sup>	<u>Product Type</u>	<u>Single Pane U-value</u>	<u>Double Pane U-value</u> <sup>2</sup>
Metal	Operable	1.28	0.87
Metal	Fixed	1.19	0.72
Metal	Greenhouse/Garden window	2.26	1.40
Metal	Doors	1.25	0.85
Metal	Skylight	1.72	0.94
Metal, Thermal Break	Operable		0.71
Metal, Thermal Break	Fixed		0.60
Metal, Thermal Break	Greenhouse/Garden window		1.12
Metal, Thermal Break	Doors		0.64
Metal, Thermal Break	Skylight		0.80
Non-Metal	Operable	0.99	0.60
Non-Metal	Fixed	1.04	0.57
Non-Metal	Doors	0.99	0.55
Non-Metal	Greenhouse/Garden windows	1.94	1.06
Non-Metal	Skylight	1.47	0.68

<sup>1</sup> Metal includes any field-fabricated product with metal cladding. Non-metal framed manufactured fenestration products with metal cladding must add 0.04 to the listed U-value. Non-Metal frame types can include metal fasteners, hardware, and door thresholds. Thermal break product design characteristics are:

- a. The material used as the thermal break must have a thermal conductivity of not more than 3.6 Btu-inch/hr/ft<sup>2</sup>/°F,
- b. The thermal break must produce a gap of not less than 0.210", and
- c. All metal members of the fenestration product exposed to interior and exterior air must incorporate a thermal break meeting the criteria in (a) and (b) above.

In addition, the fenestration product must be clearly labeled by the manufacturer that it qualifies as a thermally broken product in accordance with this standard.

<sup>2</sup>For all dual glazed fenestration products, adjust the listed U-values as follows:

- a. Subtract 0.05 for spacers of 7/16" or wider.
- b. Subtract 0.05 for products certified by the manufacturer as low-E glazing.
- c. Add 0.05 for products with dividers between panes if spacer is less than 7/16" wide.
- d. Add 0.05 to any product with true divided lite (dividers through the panes).



Table E-9

**DEFAULT FENESTRATION PRODUCT  
SOLAR HEAT GAIN COEFFICIENTS**

<u>Frame Type</u>	<u>Product</u>	<u>Glazing</u>	<b>Total Window SHGC</b>	
			<b><u>Single Pane</u></b>	<b><u>Double Pane</u></b>
Metal	Operable	Uncoated	0.80	0.70
Metal	Fixed	Uncoated	0.83	0.73
Metal	Operable	Tinted	0.67	0.59
Metal	Fixed	Tinted	0.68	0.60
Metal, Thermal Break	Operable	Uncoated	0.72	0.63
Metal, Thermal Break	Fixed	Uncoated	0.78	0.69
Metal, Thermal Break	Operable	Tinted	0.60	0.53
Metal, Thermal Break	Fixed	Tinted	0.65	0.57
Non-Metal	Operable	Uncoated	0.74	0.65
Non-Metal	Fixed	Uncoated	0.76	0.67
Non-Metal	Operable	Tinted	0.60	0.53
Non-Metal	Fixed	Tinted	0.63	0.55

SC = Shading Coefficient

SHGC = Solar Heat Gain Coefficient



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### ASHRAE's U-value Calculation Procedures

ASHRAE's procedures for calculating U-Values are documented in the *1997 ASHRAE Handbook of Fundamentals*, Chapter 24. Parts or all of this chapter may later be reproduced in this section when the Commission gets ASHRAE's approval to reproduce their copyrighted information.

Special care must be taken to properly calculate the U-values of walls containing metals, e.g. steel or aluminum framing, since metals short-circuit the flow of heat and allow heat flows to bypass insulation. Various methods in the *ASHRAE Handbook of Fundamentals* account for these effects but care must be taken to be certain that the assumptions of the simpler calculation methods for metal-framed walls are valid since large errors may result if they are not.











# APPENDIX F



## Appendix F

### Standard Procedure for Determining the Seasonal Energy Efficiencies of Residential Air Distribution Systems

#### 1.0 Introduction

This appendix describes the measurement and calculation methods for determining air distribution system efficiency.

#### 2.0 Definitions

**aerosol sealant closure system:** A method of sealing leaks by blowing aerosolized sealant particles into the duct system and which must include minute-by-minute documentation of the sealing process.

**floor area :** The floor area of enclosed conditioned space on all floors of a building, as measured at the floor level of the exterior surfaces enclosing the conditioned space.

**delivery effectiveness :** The ratio of the thermal energy delivered to the conditioned space and the thermal energy entering the distribution system at the equipment heat exchanger.

**distribution system efficiency :** The ratio of the thermal energy consumed by the equipment with the distribution system to the energy consumed if the distribution system had no losses or impact on the equipment or building loads.

**equipment efficiency :** The ratio between the thermal energy entering the distribution system at the equipment heat exchanger and the energy being consumed by the equipment.

**equipment factor :**  $F_{\text{equip}}$  is the ratio of the equipment efficiency including the effects of the distribution system to the equipment efficiency of the equipment in isolation.

**fan flowmeter device:** A device used to measure air flow rates under a range of test pressure differences.

**flowhood:** A device used to capture and measure the airflow at a register.

**load factor :**  $F_{\text{load}}$  is the ratio of the building energy load without including distribution effects to the load including distribution system effects.

**pressure pan :** a device used to seal individual forced air system registers and to measure the static pressure from the register.

**radiant barrier :** a surface of low emissivity (less than 0.05) placed inside an attic or roof space to reduce radiant heat transfer.



**recovery factor** :  $F_{\text{recovery}}$  is the fraction of energy lost from the distribution system that enters the conditioned space.

**thermal regain**: The fraction of delivery system losses that are returned to the building.

### 3.0 Nomenclature

$a_r$  = duct leakage factor (1-return eakage) for return ducts  
 $a_s$  = duct leakage factor (1-supply leakage)p for supply ducts  
 $A_{\text{floor}}$  = conditioned floor area of building , ft<sup>2</sup>  
 $A_{r,\text{out}}$  = surface area of return duct outside conditioned space ,ft<sup>2</sup>  
 $A_{r,\text{attic}}$  = return duct area in attic , ft<sup>2</sup>  
 $A_{r,\text{base}}$  = return duct area in basement , ft<sup>2</sup>  
 $A_{r,\text{crawl}}$  = return duct area in crawlspace, ft<sup>2</sup>  
 $A_{r,\text{gar}}$  = return duct area inside garage, ft<sup>2</sup>  
 $A_{s,\text{out}}$  = surface area of supply duct outside conditioned space,ft<sup>2</sup>  
 $A_{s,\text{attic}}$  = supply duct area in attic , ft<sup>2</sup>  
 $A_{s,\text{base}}$  = supply duct area in basement , ft<sup>2</sup>  
 $A_{s,\text{crawl}}$  = supply duct area in crawlspace,ft<sup>2</sup>  
 $A_{s,\text{gar}}$  = supply duct area inside garage, ft<sup>2</sup>  
 $A_{s,\text{in}}$  = supply duct area inside conditioned space, ft<sup>2</sup>  
 $B_r$  = conduction fraction for return  
 $B_s$  = conduction fraction for supply  
 $DE$  = delivery effectiveness\_  
 $DE_{\text{design}}$  = design delivery effectiveness  
 $DE_{\text{seasonal}}$  = seasonal delivery effectiveness  
 $E_{\text{equip}}$  = rate of energy exchanged between equipment and delivery system,  
 Btu/hour  
 $F_{\text{cycloss}}$  = cyclic loss factor  
 $F_{\text{equip}}$  = load factor for equipment  
 $F_{\text{flow}}$  = load factor for fan flow effect on equipment efficiency  
 $F_{\text{leak}}$  = fraction of system fan flow that leaks out of supply or return ducts  
 $F_{\text{load}}$  = load factor for delivery system  
 $F_{\text{recovery}}$  = thermal loss recovery factor  
 $F_{\text{regain}}$  = thermal regain factor  
 $K_r$  = return duct surface area coefficient  
 $K_s$  = supply duct surface area coefficient  
 $N_{\text{story}}$  = number of stories of the building  
 $P_{sp}$  = pressure difference between supply plenum and conditioned space [Pa]  
 $P_{\text{test}}$  = test pressure for duct leakage [Pa]  
 $Q_e$  = Flow through air handler fan at operating conditions, cfm  
 $Q_{\text{total},25}$  = total duct leakage at 25 Pascal, cfm  
 $R_r$  = thermal resistance of return duct, h ft<sup>2</sup> F/Btu  
 $R_s$  = thermal resistance of supply duct, h ft<sup>2</sup> F/Btu  
 $T_{\text{amb},r}$  = ambient temperature for return , F

$T_{\text{amb},s}$  = ambient temperature for supply , F  
 $T_{\text{attic}}$  = attic air temperature , F  
 $T_{\text{base}}$  = return duct temperature in basement, F  
 $T_{\text{crawl}}$  = return duct temperature in crawlspace,F  
 $T_{\text{design}}$  = outdoor air design temperature , F  
 $T_{\text{ground}}$  = ground temperature , F  
 $T_{\text{gar}}$  = temperature of garage air , F  
 $T_{\text{in}}$  = temperature of indoor air , F  
 $T_{\text{rp}}$  = return plenum air temperature , F  
 $T_{\text{seasonal}}$  = outdoor air seasonal temperature, F  
 $T_{\text{sp}}$  = supply plenum air temperature , F  
 $\Delta T_e$  = temperature rise across heat exchanger , F  
 $\Delta T_r$  = temperature difference between indoors and the ambient for the return , F  
 $\Delta T_s$  = temperature difference between indoors and the ambient for the supply,  
 $\eta_{\text{dist,seasonal}}$  = seasonal distribution system efficiency



## **4.0 Air Distribution Diagnostic Measurement and Default Assumptions**

### **4.1 Instrumentation Specifications**

The instrumentation for the air distribution diagnostic measurements shall conform to the following specifications:

#### **4.1.1 Pressure Measurements**

All pressure measurements shall be measured with measurement systems (i.e. sensor plus data acquisition system) having an accuracy of  $\pm 0.2$  Pa. All pressure measurements within the duct system shall be made with static pressure probes.

#### **4.1.2 Fan Flow Measurements**

All measurements of distribution fan flows shall be made with measurement systems (i.e. sensor plus data acquisition system) having an accuracy of  $\pm 5\%$  reading or  $\pm 5$  cfm whichever is greater.

#### **4.1.3 Duct Leakage Measurements**

The measurement of air flows during duct leakage testing shall have an accuracy of  $\pm 3\%$  of measured flow using digital gauges.

All instrumentation used for fan flow and duct leakage diagnostic measurements shall be calibrated according to the manufacturer's calibration procedure to conform to the above accuracy requirement. All testers performing diagnostic tests shall obtain evidence from the manufacturer that the equipment meets the accuracy specifications. The evidence shall include equipment model, serial number, the name and signature of the person of the test laboratory verifying the accuracy, and the instrument accuracy. All diagnostic testing equipment is subject to re-calibration when the period of the manufacturer's guaranteed accuracy expires.

### **4.2 Apparatus**

#### **4.2.1 System Fan Flows**

HVAC system fan flow shall be measured using one of the following methods.

##### **4.2.1.1 Plenum pressure matching measurement**

The apparatus for measuring the system fan flow shall consist of a duct pressurization and flow measurement device (subsequently referred to as a fan flowmeter [see section 4.3.7.2.2.]) meeting the specifications in 4.1.3, a static pressure transducer meeting the specifications in Section 4.1.1, and an air barrier between the return duct system and the air handler inlet. The measuring device shall be attached at the air handler blower compartment door. All registers shall be in their normal operating condition. The static pressure probe shall be fixed to the supply plenum so that it is not moved during this test.

##### **4.2.1.2 Flow hood measurement**



A flow hood meeting the specifications in section 4.1.2. can be used to verify the fan flow at the return register(s) after the completion of a rough-in duct leakage measurement. All registers shall be in their normal operating position. Measurement(s) shall be taken at the return grill(s).

#### **4.2.2 Duct Leakage**

The apparatus for fan pressurization duct leakage measurements shall consist of a duct pressurization and flow measurement device meeting the specifications in Section 4.1.3.

### **4.3 Procedure**

The following sections identify input values for building and HVAC system (including ducts) using either default or diagnostic information.

#### **4.3.1 Building Information**

The calculation procedure for determining air distribution efficiencies requires the following building information:

1. climate zone for the building,
2. conditioned floor area,
3. number of stories,
4. supply duct location and
5. floor type.

##### **4.3.1.1 Default Input**

Using default values rather than diagnostic procedures produce relatively low air distribution-system efficiencies. Default values shall be obtained from following sections:

1. the location of the duct system in Section 4.3.4,
2. the surface area and insulation level of the ducts in Sections 4.3.3, 4.3.4 and 4.3.6,
3. the system fan flow in Section 4.3.7, and
4. the leakage of the duct system in Section 4.3.8.

##### **4.3.2 Diagnostic Input**

Diagnostic inputs are used for the calculation of improved duct efficiency. The diagnostics include observation of various duct characteristics and measurement of duct leakage and system fan flows as described in Sections 4.3.5 through 4.3.8. These observations and measurements replace those assumed as default values.

The diagnostic procedures include

- measure supply duct surface area as described in Section 4.3.3.2.
- measure total duct system leakage as described in Section 4.3.8.
- measure system fan flow or observe the presence of a thermostatic expansion valve for claiming ACCA manual D design credit as described in Section 4.3.7.
- Observe the insulation level for the supply ( $R_s$ ) and return ( $R_r$ ) ducts outside the conditioned space as described in Section 4.3.6.
- Observe the presence of radiant barriers.



### 4.3.3 Duct Surface Area

The supply-side and return-side duct surface areas shall be calculated separately. If the supply or return duct is located in more than one zone, the area of that duct in each zone shall be calculated separately. The duct surface area shall be determined using the following methods.

#### 4.3.3.1 Default Duct Surface Area

##### 4.3.3.1.1 Duct Surface Area for More Than 12 feet of Duct Outside Conditioned Space

The default duct surface area for supply and return shall be calculated as follows:

For supplies:

$$A_{s,\text{total}} = 0.27 A_{\text{floor}} \quad (4.1)$$

For returns:

$$A_{r,\text{total}} = K_r A_{\text{floor}} \quad (4.2)$$

Where  $K_r$  (return duct surface area coefficient) shall be 0.05 for one story building and 0.1 for two or more stories.

##### 4.3.3.1.1 Duct Surface Area for Less Than 12 feet of Duct Outside Conditioned Space

For HVAC systems with air handlers located outside the conditioned space but with less than 12 feet of duct located outside the conditioned space including air handler and plenum, the duct surface area outside the conditioned space shall be calculated as follows:

$$A_{s,\text{out}} = 0.027 A_{\text{floor}} \quad (4.3)$$

Where  $A_{s,\text{out}}$  is substituted for  $A_{s,\text{attic}}$ ;  $A_{s,\text{crawl}}$ ; or  $A_{s,\text{base}}$  depending on the location of the ducts.

### 4.3.3.2 Diagnostic Duct Surface Area

A well designed duct system can reduce the length of the supply duct. Smaller duct surface area will result in reduced duct conduction losses. Duct surface area shall be calculated from measured duct lengths and nominal outside diameters (for round ducts) or outside perimeters (for rectangular ducts) of each duct run in the building. Improved conduction losses can be claimed for reduced supply duct surface area only (it does not apply to the return duct). Supply plenum surface area shall be included in the supply duct surface area. Diagnostic duct surface area requires measuring duct surface areas separately for each location outside conditioned space ( $A_{s,\text{attic}}$ ;  $A_{s,\text{crawl}}$ ; or  $A_{s,\text{base}}$ ) and the system fan flow to ensure that there is sufficient air flow to deliver the designed heating and cooling loads.



#### 4.3.4 Duct Location

Duct location determines the external temperature for duct conduction losses, the temperature for return leaks, and the thermal regain of duct losses. Default duct surface areas by locations of the supply duct shall be obtained from Table 4.1. The default duct surface area for crawlspace and basement applies only to buildings with all supply ducts installed in the crawlspace or basement. If the supply duct is installed in locations other than crawlspace or basement, the default supply duct location shall be “Other”.

If ducts are installed in multiple locations, air distribution efficiency shall be calculated for each duct location. Total air distribution efficiency for the house shall be the weighted average based on the floor area served by each duct system.

<b>Table 4.1 Default Assumptions for Duct Locations</b>				
Supply or Return Duct Location	<b>Supply Duct Surface Area</b>		<b>Return Duct Surface Area</b>	
	One story	Two or more story	One story	Two or more story
Attic	100% attic	65% attic 35% conditioned space	100% attic	100% attic
Crawlspace	100% crawlspace	65% crawlspace 35% conditioned space	100% attic	100% attic
Basement	100% Basement	65% basement 35% conditioned space	100% Basement	100% Basement
Other	100% attic	65% attic 35% conditioned space	100% attic	100% attic

#### 4.3.5 Climate and Duct Ambient Conditions for Ducts Outside Conditioned Space

Duct ambient temperature for both heating and cooling at different duct locations shall be obtained from Table 4.2. Indoor dry-bulb ( $T_{in}$ ) temperature for cooling is 78°F. The indoor dry-bulb temperature for heating is 70°F. Reduction of attic temperature and the reduction in solar radiation effect due to radiant barriers shall only be applied to cooling calculations. The procedures for the installation of radiant barriers shall be as described in ACM Section 4.23. Attic temperatures for houses with radiant barriers shall be obtained from Table 4.2.

<b>Table 4.2 Default Assumptions for Duct Ambient Temperature</b>								
Climate zone	<b>Duct Ambient Temperature for Heating, <math>T_{heat,amb}</math></b>			<b>Duct Ambient Temperature for Cooling, <math>T_{cool,amb}</math></b>				
	Attic	Crawlspace	Basement	Attic	Attic w/ radiant	Attic w/ radiant	Crawlspace	Basement



					barrier (supply)	barrier (return)		
1	52.0	52.2	48.9	60.0	65.4	61.2	54.0	49.1
2	48.0	48.7	56.5	87.0	84.3	84.2	78.0	64.5
3	55.0	54.9	58.3	80.0	79.4	78.2	71.8	62.8
4	53.0	53.1	56.6	79.0	78.7	77.4	70.9	61.4
5	49.0	49.6	52.3	74.0	75.2	73.1	66.4	56.8
6	57.0	56.7	59.9	81.0	80.1	79.1	72.7	64.1
7	62.0	61.1	60.4	74.0	75.2	73.1	66.4	61.6
8	58.0	57.6	60.1	80.0	79.4	78.2	71.8	63.9
9	53.0	53.1	59.6	87.0	84.3	84.2	78.0	66.4
10	53.0	53.1	61.1	91.0	87.1	87.6	81.6	68.9
11	48.0	48.7	59.5	95.0	89.9	91.0	85.1	69.5
12	50.0	50.4	59.3	91.0	87.1	87.6	81.6	67.8
13	48.0	48.7	58.4	92.0	87.8	88.4	82.4	67.6
14	39.0	40.7	55.4	99.0	92.7	94.4	88.7	68.6
15	50.0	50.4	63.4	102.	94.8	96.9	91.3	74.6
16	32.0	34.4	43.9	80.0	79.4	78.2	71.8	54.1

### 4.3.6 Duct Wall Thermal Resistance

#### 4.3.6.1 Default Duct Insulation R value

Default duct wall thermal resistance is R4.2. An air film resistance of 0.7 [h ft<sup>2</sup> °F/BTU] shall be added to the duct insulation R value to account for external and internal film resistance.

#### 4.3.6.2 Diagnostic Duct Wall Thermal Resistance

Duct wall thermal resistance shall be determined from the manufacturer's specification observed during diagnostic inspection. If ducts with multiple R values are installed, the lowest duct R value shall be used. If a duct with a higher R value than 4.2 is installed, the R-value shall be clearly stated on the building plan and a visual inspection of the ducts must be performed to verify the insulation values. In case the space on top of the duct boot is limited and can not be inspected, the insulation R value within two feet of the boot to which the duct is connected may be excluded from the determination of the overall system R value.

### 4.3.7 System Fan Flow

#### 4.3.7.1 Default Fan Flow

The default cooling fan flow with an air conditioner and for heating with a heat pump for **climate zones 8 through 15** shall be calculated as follows:



$$Q_e = 0.70 A_{\text{floor}} \quad (4.4)$$

The default cooling fan flow with an air conditioner and for heating with a heat pump for **climate zones 1 through 7 and 16** and default heating fan flow for forced air furnaces for all climate zones shall be calculated as follows:

$$Q_e = 0.50 A_{\text{floor}} \quad (4.5)$$

#### **4.3.7.2 Diagnostic Fan Flow**

To obtain duct efficiency credit for duct systems designed according to ACCA Manual D, a diagnostic fan flow measurement must be performed or the installation of a thermostatic expansion valve must be verified. The access panel on the cooling coil shall be removable for the verification of a thermostatic expansion valve. For ACCA Manual D designed duct system, engineering calculations and the building plan for duct sizing and layout shall also be prepared. The diagnostic fan flow measurement shall be measured using one of the following methods:

##### **4.3.7.2.1 Diagnostic Fan Flow Using Flow Hood:**

To measure the system return fan flow, all registers shall be fully open, and the air filter shall be installed. Turn on the system fan and measure the fan flow at the return grille(s) with a calibrated flow hood to determine the total system return fan flow. The system fan flow ( $Q_e$ ) shall be the sum of the measured return flows.

##### **4.3.7.2.2 Diagnostic Fan Flow Using Plenum Pressure Matching:**

The fan flow measurement shall be performed using the following procedures:

1. With the system fan on ( in heating mode with burners on for heating, or in cooling mode with compressor on), measure the pressure difference (in pascal) between the supply plenum and the conditioned space ( $\Delta P_{sp}$ ).  $P_{sp}$  is the target pressure to be maintained during the fan flow tests. If there is no access to the supply plenum, then place the pressure probe in the nearest supply duct. Adjust the probe to achieve the highest pressure and then firmly attach the probe (e.g., with duct tape) to ensure that it does not move during the fan flow test.
2. Block the return duct from the plenum upstream of the air handler fan and the fan flowmeter. Filters are often located in an ideal location for this blockage.
3. Attach the fan flowmeter device to the duct system at the air handler. For many air handlers, there will be a removable section that allows access to the fan that is suitable for this purpose. Assure that there is no significant leakage between the fan flowmeter and the system fan.
4. If the fan flowmeter is connected to the air handler outside the conditioned space, then the door or access panel between the conditioned space and the air handler location shall be opened.
5. Turn on the system fan and the fan flowmeter, adjust the fan flowmeter until the pressure between supply plenum and conditioned space matches  $P_{sp}$ .



6. Record the flow through the flowmeter ( $Q_e$ , cfm) - this is the diagnostic fan flow.

In some systems, typical system fan and fan flowmeter combinations may not be able to produce enough flow to reach  $P_{sp}$ . In this case record the maximum flow ( $Q_{max}$ , cfm) and pressure ( $P_{max}$ ) between the supply plenum and the conditioned space. The following equation shall be used to correct measured system flow and pressure ( $Q_{max}$  and  $P_{max}$ ) to operating condition ( $Q_e$ ) at operating pressure ( $P_{sp}$ ).

$$Q_e = Q_{max} \left( \frac{P_{sp}}{P_{max}} \right)^{\frac{1}{2}} \quad (4.6)$$



### 4.3.8 Duct Leakage

#### 4.3.8.1 Duct Leakage Factor for Delivery Effectiveness Calculations

Default duct leakage factors shall be obtained from Table 4.3, using the “not Tested” values.

Duct leakage factors shown in Table 4.3 shall be used in calculations of delivery effectiveness.

Table 4.3 Duct Leakage Factors		
	Duct Leakage Diagnostic Test Performed using Section 4.3.8.2 Procedures	$a_s = a_r =$
Duct systems in homes built prior to 1999	Not tested	0.86
Duct systems in homes built after 1999	Not tested	0.89
Duct systems in homes of all ages, System with refrigerant based cooling, tested after house and HVAC system completion	( $Q_{25}$ ) Total leakage is less than $0.06 Q_{ecool}$	0.96
Duct systems in homes of all ages, System without refrigerant based cooling, tested after house and HVAC system completion	( $Q_{25}$ ) Total leakage is less than $0.06 Q_{eheat}$	0.96
Duct systems with refrigerant based cooling, in homes built after 1999, System tested with air handler installed, but prior to installation of the interior finishing wall	( $Q_{25}$ ) Total leakage is less than $0.06 Q_{ecool}$ and final duct integrity verified	0.96
Duct systems without refrigerant based cooling, in homes built after 1999, System tested with air handler installed, but prior to installation of the interior finishing wall	( $Q_{25}$ ) Total leakage is less than $0.06 Q_{eheat}$ and final duct integrity verified	0.96
Duct systems with refrigerant based cooling, in homes built after 1999, System tested without air handler installed, but prior to installation of the interior finishing wall	( $Q_{25}$ ) Total leakage is less than $0.04 Q_{ecool}$ and final duct integrity verified	0.96
Duct systems without refrigerant based cooling, in homes built after 1999, System tested without air handler installed, but prior to installation of the interior finishing wall	( $Q_{25}$ ) Total leakage is less than $0.04 Q_{eheat}$ and final duct integrity verified	0.96

#### 4.3.8.2 Diagnostic Duct Leakage



Diagnostic duct leakage measurement is used to quantify total leakage for the calculation of air distribution efficiency. To obtain the improved duct efficiency for sealing the duct system, a diagnostic leakage test as described in section 4.3.8.2.1 or 4.3.8.2.2 must be performed. Houses built after 1/1/1999 shall not be allowed to claim duct leakage credit and diagnostic testing may not be done on any HVAC system that uses building cavities such as plenums or a platform return.

#### **4.3.8.2.1 Diagnostic Duct Leakage from Fan Pressurization of Ducts**

The total duct leakage shall be determined by pressurizing the ducts to 25 Pascals. The following procedure shall be used for the fan pressurization tests:

1. Seal all the supply and return registers, except for one return register or the system fan access.
2. Attach the fan flowmeter device to the duct system at the unsealed register or access door.
3. Install a static pressure probe at a supply.
4. Adjust the fan flowmeter to produce a 25 Pascal (0.1 in water) pressure difference between the supply duct and the outside or the building space with the entry door open to the outside.
5. Record the flow through the flowmeter ( $Q_{\text{total},25}$ ) - this is the total duct leakage flow at 25 Pascals.

When the diagnostic leakage test is performed and the measured total duct leakage is less than 6% of the total fan flow, the duct leakage factor shall be 0.96 as shown in Table 4.3.

#### **4.3.8.2.2 Diagnostic Duct Leakage at Rough-in Construction Stage Using An Aerosol Sealant Closure System**

Duct leakage in new construction may be determined by using diagnostic measurements at the rough-in building construction stage prior to installation of the interior finishing wall when using an aerosol sealant closure system. When using this measurement technique, additional verification (as described in section 4.3.8.2.2.3) of duct integrity shall be completed after the finishing wall has been installed. In addition, after the finishing wall is installed, spaces between the register boots and the wallboard shall be sealed. Cloth backed rubber adhesive duct tapes shall not be used to seal the space between the register boot and the wall board.

The duct leakage measurement at rough-in construction stage shall be performed using a fan pressurization device. The duct leakage shall be determined by pressurizing both the supply and return ducts to 25 Pa. The procedures in Sections 4.3.8.2.2.1 and 4.3.8.2.2.2 shall be used for measuring duct leakage before the interior finishing wall is installed.

##### **4.3.8.2.2.1 For ducts with the air handling unit installed and connected:**



**For total leakage:**

1. Verify that supply and return plenums and all the connectors, transition pieces and duct boots have been installed. If a platform is used as part of the air distribution system, it must contain a duct, and all return connectors and transition parts shall be installed and sealed. The platform, duct and connectors shall be included in the total leakage test.
2. Seal all the supply duct boots and return boxes except for one return duct box.
3. Attach the fan flowmeter device at the unsealed duct box.
4. Insert a static pressure probe at one of the sealed supply duct boots.
5. Adjust the fan flowmeter to maintain 25 Pa(0.1 in water)between the duct system and outside or the building space with the entry door open to the outside.
6. Record the air flow through the flowmeter ( $Q_{\text{total},25}$ ) - This is the total duct leakage at 25 Pa at rough-in stage.
7. Divide the measured total leakage by the total fan flow calculated from equation 4.4 or 4.5.

If the total leakage is less than 6% of the total fan flow, the duct leakage factor shall be 0.96 as shown in Table 4.3.

**1****4.3.8.2.2.2 For ducts with air handling unit not yet installed:****For total leakage:**

1. Verify that all the connectors, transition pieces and duct boots have been installed. If a platform is used as part of the air distribution system, it must contain a duct, and all return connectors and transition parts shall be installed and sealed. The platform, duct and connectors shall be included in the total leakage test.
2. Use a duct connector to connect supply and/or return duct box to the fan flowmeter. Supply and return leaks may be tested separately. If there is only one return register, the supply and return leaks shall be tested at the same time.
3. Seal all the supply duct boots and/or return boxes except for one supply or return duct box.
4. Attach the fan flowmeter device at the unsealed duct box.
5. Insert a static pressure probe at one of the sealed supply duct boots.
6. Adjust the fan flowmeter to maintain 25 Pa (0.1 in water) between the building conditioned space and the duct system.
7. Record the air flow through the flowmeter ( $Q_{\text{total},25}$ ) - This is the total duct leakage at 25 Pa.
8. Divide the measured total leakage by the total fan flow calculated from equation 4.4 or 4.5. If the total leakage is less than 4% of the total fan flow, the total duct leakage factor shall be 0.96 as shown in Table 4.3.

**4.3.8.2.2.3 Post rough-in duct leakage verification**

After installing the interior finishing wall and verifying that one of the above rough-in tests was completed, one of the following post rough-in verification tests shall be performed to ensure that there is no major leakage in the duct system.

**4.3.8.2.2.3.1 Visual inspection**



Remove at least one supply and one return register to verify that the spaces between the register boot and the interior finishing wall are properly sealed. In addition, if the house rough-in duct leakage test was conducted without an air handler installed, inspect the connection points between the air handler and the supply and return plenums to verify that the connection points are properly sealed. All joints shall be inspected to ensure that no cloth backed rubber adhesive duct tape is used.

#### **4.3.8.2.2.3.2 Pressure pan test**

With register dampers fully open, the house is pressurized to 25 pascals by a blower door, ( If two registers are within 5 feet of each other and are connected to the same duct run, one register shall be sealed off before the pressure pan test is performed). the pressure difference across each register shall not exceed 1.5 Pa.

#### **4.3.8.2.2.3.3 House Pressure Test**

The pressure difference between the building conditioned space and a vented attic shall be measured to determine whether the house pressure is changed appreciably by the operation of the air handler. To perform this test, the pressure difference ( $P_{\text{house}} - P_{\text{out}}$ ) between the building conditioned space and a vented attic (or outside if impossible to access the attic), shall be measured four times:

1. with the fan off ( $\Delta P_{\text{off1}}$ )
2. with the fan on ( $\Delta P_{\text{on}}$ )
3. with the fan on and the return grille 80% blocked ( $\Delta P_{\text{RB}}$ ). Block 80% on all return grilles if the house has two or more returns.
4. with the fan off ( $\Delta P_{\text{off2}}$ )

For each of these measurements, the five-second average pressure shall be measured 10 times and these 10 measurements shall be averaged.

For the house to pass this test, the following conditions must be true:

1.  $\Delta P_{\text{on}} - (\Delta P_{\text{off2}} + \Delta P_{\text{off1}})/2$  must be between +0.8 Pa and -0.8 Pa and
2.  $\Delta P_{\text{RB}} - \Delta P_{\text{on}}$  must be less than 0.8 Pa.

In addition, the absolute value of ( $\Delta P_{\text{off2}} - \Delta P_{\text{off1}}$ ) must be less than 0.25 Pa, or else the test must be repeated. If the repeated test does not meet the above specified values, visual inspection or the pressure pan test or the fan pressurization test must be used. If these tests fail, the duct system needs to be properly sealed and re-verified by a fan pressurization test.

### **4.4 Delivery Effectiveness (DE) Calculations**

Seasonal delivery effectiveness shall be calculated using the seasonal design temperatures from Tables 4.2.

#### **4.4.1 Calculation of Duct Zone Temperatures**

The temperatures of the duct zones outside the conditioned space are determined in Section 4.3.5 for seasonal conditions for both heating and cooling. If the ducts are not all in the same location, the duct ambient temperature for use in the delivery effectiveness and distribution system efficiency calculations shall be determined using an area weighted average of the duct zone temperatures:



$$T_{amb,s} = \frac{(A_{s,attic} + 0.001)T_{attic} + A_{s,crawl}T_{crawl} + A_{s,base}T_{base}}{A_{s,out} + 0.001} \quad (4.7)$$

$$T_{amb,r} = \frac{A_{r,attic}T_{attic} + A_{r,crawl}T_{crawl} + A_{r,base}T_{base}}{A_{r,out}} \quad (4.8)$$

The return ambient temperature,  $T_{amb,r}$ , shall be limited as follows:

For heating, the maximum  $T_{amb,r}$  is  $T_{in,heat}$ . For cooling, the minimum  $T_{amb,r}$  is  $T_{in,cool}$ .

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#### 4.4.2 Seasonal Delivery Effectiveness (DE)

The supply and return conduction fractions,  $B_s$  and  $B_r$ , shall be calculated as follows:

$$B_s = \exp\left(\frac{-A_{s,out}}{1.08Q_e R_s}\right) \quad (4.9)$$

$$B_r = \exp\left(\frac{-A_{r,out}}{1.08 Q_e R_r}\right) \quad (4.10)$$

The temperature difference across the heat exchanger in the following equation is used:  
for heating:

$$\Delta T_e = 55 \quad (4.11)$$

for cooling:

$$\Delta T_e = -20 \quad (4.12)$$

The temperature difference between the building conditioned space and the ambient temperature surrounding the supply,  $\Delta T_s$ , and return,  $\Delta T_r$ , shall be calculated using the indoor and the duct ambient temperatures.

$$\Delta T_s = T_{in} - T_{amb,s} \quad (4.13)$$

$$\Delta T_r = T_{in} - T_{amb,r} \quad (4.14)$$

The seasonal delivery effectiveness for heating systems shall be calculated using:



$$DE_{\text{seasonal}} = \frac{a_s B_s - a_s B_s (1 - B_{\text{rar}}) \frac{\Delta T_r}{\Delta T_e} - a_s (1 - B_s) \frac{\Delta T_s}{\Delta T_e}}{4} \quad (4.15)$$

#### 4.5 Seasonal Distribution System Efficiency

Seasonal distribution system efficiency shall be calculated using delivery effectiveness, equipment, load, and recovery factors calculated for seasonal conditions.

##### 4.5.1 Equipment Efficiency Factor ( $F_{\text{equip}}$ )

Equipment efficiency factor accounts for interactions between the duct system and the operation of the heating or cooling equipment. If the duct size and layout are designed and installed according to ACCA manual D and if the fan flow measurement meets the design specifications, the efficiency factor for  $F_{\text{equip}}$  is 1. Otherwise  $F_{\text{equip}}$  shall be 0.925. For heating,  $F_{\text{equip}}$  is 1.

##### 4.5.2 Thermal Regain ( $F_{\text{regain}}$ )

The reduction in building load due to regain of duct losses shall be calculated using the thermal regain factor. The default thermal regain factors are provided in Table 4.4.

Table 4.4 Thermal Regain Factors	
Supply Duct Location	Thermal Regain Factor [ $F_{\text{regain}}$ ]
Attic	0.10
Crawlspace	0.12
Basement	0.30
Other	0.10

##### 4.5.3 Recovery Factor ( $F_{\text{recovery}}$ )

The recovery factor,  $F_{\text{recovery}}$ , is calculated based on the thermal regain factor,  $F_{\text{regain}}$ , and the duct losses without return leakage.

$$F_{\text{recovery}} = 1 + F_{\text{regain}} \left( \frac{1 - a_s B_s + a_s B_s (1 - B_r) \frac{\Delta T_r}{\Delta T_e} + a_s (1 - B_s) \frac{\Delta T_s}{\Delta T_e}}{DE_{\text{seasonal}}} \right) \quad (4.16)$$



**4.5.4 Seasonal Distribution System Efficiency**

The seasonal distribution system efficiency shall be calculated using the seasonal delivery effectiveness from section 4.4.2 or 4.4.3, the equipment efficiency factor from section 4.5.1, the load factor from section 4.5.3 and the thermal recovery factor from Section 4.5.4. Note that  $DE_{\text{seasonal}}$ ,  $F_{\text{equip}}$ ,  $F_{\text{recov}}$  must be calculated separately for cooling and heating conditions. Distribution system efficiency shall be determined using the following equation:

$$h_{\text{dist,seasonal}} = 0.98 DE_{\text{seasonal}} F_{\text{equip}} F_{\text{recov}} \quad (4.17)$$

where 0.98 accounts for the energy losses from heating and cooling the duct thermal mass.







# APPENDIX G



**APPENDIX G**

**APPLICATION PACKAGE FOR CERTIFICATION OF SOLAR  
WATER HEATING ENERGY PERFORMANCE CALCULATION  
METHODS FOR RESIDENTIAL BUILDINGS**

California Energy Commission

1516 Ninth Street

Sacramento California 95814

June 25, 1985

Revision: June 1, 1998







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## I. INTRODUCTION

On July 15, 1981 the California Energy Commission (CEC) adopted new standards for residential buildings that include a performance or energy budget approach for demonstrating compliance. The new building standards were devised to reduce energy consumption in the housing market through the use of more efficient appliances and greater utilization of conservation and solar design technologies.

These performance standards establish energy budgets for both the space conditioning and water heating elements of a proposed building. One option for demonstrating compliance requires the designer to calculate the building's estimated annual energy use using a certified energy analysis calculation method in conjunction with established weather and building operation information. Solar domestic hot water systems are an integral part of these standards and can be used to demonstrate compliance with the water heating element. For typical flat plate solar collector systems as used in active solar water heating systems, the CEC has certified F-Chart 4.0 and 4.1. For all passive type water heating systems, thermosyphon and integral collector/storage (ICS) systems, the CEC has certified a calculation procedure to calculate system total annual energy contribution (Attachment J). Passive solar water heating credits are derived from test results published by the Solar Rating and Certification Corporation (SRCC) in conjunction with climate zone specific weather data for California. Climate zone insolation data and ambient air temperature and water main temperature data are required to calculate passive solar credit. Documentation for each analysis approach can be obtained from the following sources:

F-Chart

Solar Energy Laboratory  
University of Wisconsin  
Madison, WI 53706  
(608)263-1590

Passive Method

California Energy Commission  
Residential Office  
1516 Ninth Street, MS-25  
Sacramento CA 95814-5512

The purpose of this certification package is: (1) to provide a procedure by which other analytical approaches can be used for solar water heating compliance purposes; and (2) to establish a method for certifying their use.

Other methods may be used in lieu of F-Chart 4.0 or 4.1 or the CEC's Passive Solar Heating Calculation Method to demonstrate compliance once they have been certified by the Commission. Section 10-109 (b)(1) of the California Code of Regulations, Energy Efficiency Standards for Residential and Non-residential Buildings, provides that certification may be given if documentation is provided demonstrating that the alternative calculation method:

- A. Makes no changes in any input parameter values specified by the Commission;
- B. Provides input and output documentation that facilitates the enforcement agency's review and meets the formatting and content criteria found in the appropriate ACM Manual;
- C. Is supported by clear and concise instructions for using the method to demonstrate that the energy budget requirements of Part 6 , are met;
- D. Is reliable and accurate relative to the appropriate public domain computer program; and
- E. Establishes factors that, when applied to method's outputs, result in energy budgets for that alternative calculation method that are equivalent to those in Part 6 , when the buildings used to develop the energy budgets in Part 6 are modeled.

This certification process will be used to verify comparability of computer calculation results against results of the Commission's public domain solar water heating computer programs. An applicant for certification is required to perform three types of simulations in three different California specified



climate zones. For those methods which are able to generate water heating budgets, the CEC's assumptions and calculation procedure for establishing the water heating budgets are presented in Section 4.21 of this ACM Manual. Section 4.21.4 considers credits for active and passive solar water heating systems. The completed certification application package must be sent to:

California Energy Commission  
1516 Ninth Street, MS-25  
Sacramento, CA 95814

Attn: RESIDENTIAL SOLAR WATER HEATING  
CALCULATION METHOD CERTIFICATION

Any questions regarding the application package should be directed to the above address or by telephone (916) 654-4064.

Only complete applications for programs meeting the minimum requirements discussed in Section II will be evaluated.

A list of certified programs including a program abstract, an information form, and certified budget forms for each program will be made available and updated periodically as new programs are certified. Write the above address for a current list.



## II. APPLICATION PACKAGE REQUIREMENTS

In order to ensure rapid processing of applications it is essential that each application be complete and be presented in a consistent format. Each certification package must contain the following items:

- A. Application Form for certification of An Energy Analysis Computer Program (Form 1)
- B. Tabulated Sensitivity Runs (Form 2)
- C. Program Abstract
- D. Table of Fixed Input Parameters and Explanation of Fixed Values
- E. Summary of Sensitivity Analysis
- F. Program User's Manual

If any one of these elements is missing, processing of the application will be postponed until the missing information is provided.

A. Application Form

Form 1: " Application Form for Certification of an Energy Analysis Computer Program" must be filled out completely. This form will be used by CEC staff to assess the completeness of the application package and to notify the applicant upon certification of the computer program. The applicant may then attach this form with local building department permit requests as verification to local jurisdictions of certification.

B. Tabulated Sensitivity Runs

Form 2: The program's calculated energy performance, based on net solar fractions (NSF) in "Sensitivity Analysis", must be tabulated for easy reference against the base case systems of F-Chart 4.1. Use of this form will ensure consistency in building department and program user interpretation of program results.

C. Program Abstract

This summary will enable building departments to quickly determine if the program is being used in the correct application. The abstract must briefly describe measures the program simulates and the method used for simulation such as hourly calculations, thermal equilibrium, degree days, etc. The description should include types of buildings, solar system types, applicable climate zones, output descriptions (hourly, daily, etc.) and any other features significant to the program.

D. Table of Fixed Input Parameters

This table shall list all input parameters necessary to run the program and provide definitions for their use. Explanations shall also be provided for any parameter which is different than those provided by the reference program F-Chart 4.1. This table will be used to distinguish program characteristics and to identify areas where unit values are not comparable.

E. Program Sensitivity Analysis

The results of each sensitivity analysis run must be provided as support for the summarized data presented in Form 2. Each summary must reference the particular computer input / output runs using a code or some other easily recognized means.

F. Program User's Manual

A program user's guide / manual must be submitted which describes how the program works and how one may use it in a particular computer service facility. The information provided to CEC must include all documentation that would be needed by a user of this method.



The manual must list all of the variables used, provide an explanation of each variable, and explain how to read the input and output data and distinguish their significance. It should also explain how to enter the data to run the program and describe the default values if there are any.

The User's Manual must also contain a separate section / chapter dealing specifically with California Title 24 requirements. This section should include a general description of the Title 24 process, a listing of all fixed parameters, description and listing of California weather data and climate zones and other water heating compliance criteria.

NOTE: In addition to the above certification package requirements, all applicants must submit a copy of the program on the appropriate software (3 1/2" diskette) and must be compatible with MS-DOS formats.

### III. SPECIFIC CRITERIA FOR CERTIFICATION

1. Input data shall be in a standard format as specified in Attachment A.
2. Output data shall be in a standard format as specified in Attachment B.
3. The discrepancy in each individual run shall not exceed  $\pm 10\%$  of the result of the same run for F-Chart 4.1.

Example: If the nth run of F-Chart 4.1 yields .63, then the nth run of an applicant program must yield .63  $\pm$  .06 or 0.57 to 0.69.

4. Solar system data used for certification runs shall be the same data used from the test for solar equipment certification (SRCC, ARI).

Example: Collector efficiencies and flow rates specified in the SRCC and ARI Directories must be used for certification runs.

For program use, flow rates shall be converted from gallons per minute per square foot to pounds per hour per square foot in the following manner:

$$\frac{\text{gal.}}{\text{min}} \times \frac{60 \text{ min.}}{\text{hr.}} \times \frac{8.33 \text{ lb.}}{\text{gal.}} \times \frac{1}{\text{ft}^2} = \text{flow rate} \frac{\text{lb.}}{\text{hr. ft}^2}$$

5. The average water use profile as given in Attachment C shall be used for certification purposes. No other load profile may be substituted.

### IV. ALTERNATIVE MODELING PARAMETERS

Alternative modeling parameters such as storage tank stratification are allowed. They must, however, be completely defined and proven suitable as modeling parameters through calculation and empirical test documentation. Certification runs will exclude alternative modeling parameters.

### V. FIXED INPUT PARAMETERS

The following is a list of fixed input parameters for modeling purposes:

1. Water main temperatures (variable, see Table 1).
2. Ambient air temperatures (variable, see Table 1).
3. Minimum hot water set point (140 °F).
4. Hot water demand: 50 gallons per day per unit for single family dwellings, 35 gallons per day per unit for multi-family dwellings.
5. California specific weather, by climate zone (see Attachment I).
6. Auxiliary water heater efficiency
7. Incident angle modifier constant: compliance can be determined by: (a) use of the incidence angle modifier constant, determined experimentally as described in the ASHRAE Standards 96-1980 and 93-1986 collector test procedure and provided by SRCC and ARI in the collector Directory; or (b)



- setting this parameter to 0.00 and allowing the program to automatically calculate the incident angle modifier using Fresnel equations for the number of glass panes.
8. Ground reflectance: 0.20 (may use up to 0.90 if documented).

Note: See Attachment E for a listing of all certification modeling parameters. Individual sensitivity parameters for computer certification are listed on FORM 2, Section VII of this Appendix.



## VI. PROGRAM REFERENCE INFORMATION

The water heating budgets were calculated according to the methodology presented in Section 4.21 of this ACM Manual. Section 4.21.4 considers credits for active and passive solar systems.

The water heating methodology provides all assumptions used to determine the water heating budgets. It documents the method use to determine water heater recovery efficiency and standby losses, and can be used for all conventional gas and electric hot water heaters, as well as heat pump water heaters, instantaneous systems, systems requiring pumping energy and recirculated water, and solar water heating systems.






For purposes of this certification procedure, all programs for certification will be compared against the performance results of the reference F-Chart 4.1 program. However, the applicant is encouraged to thoroughly review Section 4.21 of this manual and this Attachment regarding the CEC's general water heating methodology.

Those areas which are critical to comparing performance results are:

- (1) comparing the thermal performance of a solar hot water heating system using fixed system values;
- (2) comparing the thermal performance of a solar water heating system using variable system values; and
- (3) comparing the thermal performance of a solar water heating system under different weather conditions.

### A. Active Systems

All active solar water heating programs shall be compared against the results of F-Chart 4.1. The following parameters must be varied to demonstrate the program's sensitivities (this will result in 21 separate sensitivity runs):

-  Collector efficiency rates
-  Collector area
-  Hot water use (load)
-  Collector orientation
-  Weather

1. **Collector Efficiency**  
Sensitivity runs shall be made for the following three conditions: Slope (FR-UL Product) and Y-intercept (FR-TAU-ALPHA).  
Slope: .55, .70, and 1.25  
Y-intercept: .75, .65, and .50
2. **Collector Area**  
Sensitivity runs shall be made for the following two conditions:  
Collector area: 48 sq. ft. and 64 sq. ft.  
The storage tank shall be sized at the ratio of 1.5-2.0 gallons of water storage per square foot of collector area.
3. **Hot Water Use**  
Sensitivity for the following three conditions:  
Hot water use: 30, 50, and 80 gallons
4. **Collector Orientation**  
Sensitivity for the following three conditions:  
Collector orientation: South (0°), West (90°), North (180°)
5. **Weather**



Sensitivity runs shall be made for three California Climate Zones: Zone 5 (Santa Maria), Zone 7 (San Diego), and Zone 13 (Fresno). All solar water heating programs certified for use in the Residential Building Standards must use the weather data as specified in Attachment I.

B. Passive Systems

The CEC has certified a calculation procedure for determining the annual performance of passive solar water heating systems (Attachment J). Passive solar water heating credits are derived from test results published by the Solar Rating and Certification Corporation (SRCC) in conjunction with climate zone specific weather data for California. Climate zone insolation data and ambient air temperature and water main temperature data are required to calculate passive solar credit. Applicants wishing to certify programs to be used for demonstrating compliance for passive type solar water heating systems must provide the CEC with all documentation specified in this certification package. The applicant's analysis methodology will be reviewed by CEC staff against the existing method.

Parameters which all passive solar water heating calculation methods must incorporate are the following:

- (1) Qsav rating from SRCC test
- (2) L rating from SRCC test.
- (3) All fixed parameters as specified in Section V.

Table 2 lists SRCC Qsav, Qcap and L rating for most of the passive solar water heating systems currently listed with SRCC. For those systems that are not listed in the Table please contact SRCC or Florida Solar Energy Center for certification.



Solar Rating and Certification Corporation  
c/o FSEC  
1679 Clearlake Road  
Cocoa, FL 32926  
(407) 638-1537  
(407) 638-1010 Fax  
SRCC@fsec.ucf.edu

VII. CERTIFICATION FORMS

See the attached forms.



Form 1

CALIFORNIA ENERGY RESOURCES  
CONSERVATION AND DEVELOPMENT COMMISSION

## APPLICATION FORM FOR CERTIFICATION OF AN ENERGY ANALYSIS COMPUTER PROGRAM

## Part 1: General Information

1. Organization requesting certification:  
 Name: \_\_\_\_\_ Phone: (\_\_\_\_) \_\_\_\_\_  
 Address: \_\_\_\_\_  
 \_\_\_\_\_  
 Contact person: \_\_\_\_\_  
 Applicants signature: \_\_\_\_\_  
 Application date: \_\_\_\_\_
2. Program Name: \_\_\_\_\_
3. The above named program is to be used for:  

<input type="checkbox"/> Space Conditioning <input type="checkbox"/> Solar Water Heating	<input type="checkbox"/> Space Conditioning and Solar Water Heating
---	---
4. Has the above-named program ever been used to analyze the energy use of a new residential building in California?  
☐ YES ☐ NO

---

 For Staff Use Only. Do Not Write Below These Lines.
 

---

1. Date received: \_\_\_\_\_
2. Application checklist:
 

	<u>Complete</u>	<u>Incomplete</u>
Form 1	_____	_____
Form 2	_____	_____
Program Abstract	_____	_____
Fixed Input Parameters	_____	_____
Sensitivity Summary	_____	_____
User's Manual	_____	_____
3. Comments: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_
4. The above named program is certified for use in demonstrating compliance for California's Residential Building Regulations:  
☐ YES ☐ NO
5. Staff signature: \_\_\_\_\_ Date: \_\_\_\_\_
6. Executive Director approval: \_\_\_\_\_ Date: \_\_\_\_\_



## SENSITIVITY ANALYSIS

## FOR INTERIM CERTIFICATION OF A SOLAR WATER HEATING ENERGY ANALYSIS COMPUTER PROGRAM

Program Name: \_\_\_\_\_

Organization Name: \_\_\_\_\_

Applicant Name: \_\_\_\_\_

Run	Collector Area (sq.ft.)	Slope (FR-UL)	Y-intercept (FR-TAU-ALPHA)	Hot Water Use (Gal.)	Climate Zone	Annual S (0°)	F-Chart W (90°)	N (180°)	ComparisonPr ogram
1	48	.70	.65	50	5	.60			
2	48	.70	.65	50	7	.63			
3	48	.70	.65	50	13	.67			
4	48	.55	.75	50	5	.74			
5	48	.55	.75	50	7	.77			
6	48	.55	.75	50	13	.77			
7	48	1.25	.50	50	5	.37			
8	48	1.25	.50	50	7	.38			
9	48	1.25	.50	50	13	.44			
10	64	.70	.65	50	5	.71			
11	64	.70	.65	50	7	.74			
12	64	.70	.65	50	13	.76			
13	48	.70	.65	30	5	.72			
14	48	.70	.65	30	7	.75			
15	48	.70	.65	30	13	.77			
16	48	.70	.65	80	5	.48			
17	48	.70	.65	80	7	.50			
18	48	.70	.65	80	13	.55			
19	48	.70	.65	50	5		.53	.42	
20	48	.70	.65	50	7		.55	.44	
21	48	.70	.65	50	13		.60	.48	
22	48	.70	.65	50	5				
23	48	.70	.65	50	7				
24	48	.70	.65	50	13				



TABLE 1

Climate <u>Zone</u>	Average Daily Temperature (°F)	Solar Radiation		Average Water Main Temperatures (°F)
		Btu/ft <sup>2</sup> /day on <u>horizontal</u> <u>surface</u>	Btu/ft <sup>2</sup> /day on <u>tilted</u> <u>surface</u> *	
1	52.1	1,241	1,340	60
2	57.9	1,535	1,658	65
3	56.9	1,559	1,684	65
4	59.6	1,606	1,734	65
5	60.3	1,623	1,753	65
6	63.5	1,596	1,724	70
7	62.9	1,619	1,748	70
8	63.0	1,637	1,768	70
9	63.6	1,618	1,747	70
10	63.3	1,777	1,919	70
11	62.8	1,580	1,706	65
12	60.3	1,641	1,772	65
13	62.3	1,708	1,845	65
14	55.9	1,841	1,988	65
15	72.6	1,858	2,007	70
16	42.8	1,656	1,788	60

\* These values represent the correction for tilted surface based upon the ratio multiplier (1.08) of total horizontal radiation to total south facing radiation on a 30° tilt.



Table 2  
Input Parameters for Passive Solar Water Heating Systems

Company	Model	ID #	Volume (gal)	L (Btu/hr-F)	Q Save (Btu/day)	Q cap (Btu)
Radco	CSHX60	94006A	60	5.3	20131	22466
Radco	CSHX80	94006B	80	6.8	23238	22466
Radco	CSHX100	94006C	100	8.4	24865	22466
Radco	CSHX40	94006D	40	3.8	15928	22466
SunEarth	CC-30	92011A	32	13.5	19889	22466
SunEarth	CC-40	92011B	42	17.0	22728	22466
SunEarth	CC-60P	92011C	64	28.4	28564	22466
SunEarth	CC-60S	92011D	64	16.8	28564	22466
SunEarth	CP-30	92011E	32	16.0	20016	22466
SunEarth	CP-40	92011F	42	20.1	22700	22466
SunEarth	CP-60P	92011G	64	33.6	27951	22466
SunEarth	CP-60S	92011H	64	16.8	28561	22466
TCT	PT-30-CN	95002A	30	13.7	21416	22466
TCT	PT-35-CN	95002B	35	13.7	21388	22466
TCT	PT-40-CN	95002C	40	17.7	26047	22466
TCT	PT-50-CN	95002D	50	17.7	25872	22466

Qsave = Energy Savings

L = Heat Loss Coefficient, UA

Qcap = Storage capacity of tank at 131 °F



## VIII. ATTACHMENTS

<b><u>Attachment</u></b>		<b><u>Page</u></b>
A	Standard Input	G-17
B	Standard Output	G-18
C	Water Use Profile	G-19
D	Examples of Solar Water Heating Systems	G-20
E	F-Chart 4.1 Computer Certification Base Case Input Parameters	G-22
F	F-Chart 4.1 Default Parameters	G-23
G	F-Chart 4.0 Input Parameters for the Solar Sizing Charts Pursuant to the Residential Building Standards	G-25
H	F-Chart 4.0 Assumptions Used for Residential Solar Domestic Hot Water Sizing Tables	G-26
I	Climate Zone Weather Data	G-27
J	Alternative Calculation Method for Passive Solar Credit	G-33



## ATTACHMENT A

## STANDARD INPUT

The input parameters shall be listed under the appropriate headings for clarity. When listing the parameters all units shall be specified. The following is a list of headings that shall be used:

1. Collector Parameter
2. Collector-Store-Transfer
3. Storage Unit
4. Load Parameters
5. Loss Correction
6. Weather

Additional parameters such as economic and auxiliary parameters may be used but shall be listed after the parameters listed above.



ATTACHMENT B

STANDARD OUTPUT

The standard output to be used for computer program certification purposes is defined as the solar contribution to the hot water load (including backup tank losses). This output shall be provided by all solar computer programs in kBtu/yr. Other system parameters may be shown on the standard data summary output summary but each output must contain at least the following:

System Type (See Attachment D)	_____
Annual Delivered Energy	_____kBtu/yr.
California Climate Zone	_____

THERMAL PERFORMANCE

HT (MMBTU)	TA (°F)	HWLOAD (MMBTU)	QU (MMBTU)	QLOSS (MMBTU)	FDHW
	*		*	*	

Other output may be added here.



## ATTACHMENT C

## WATER USE PROFILE

The following Table is a load profile of average water use by the hour for a given day. This must be a basic assumption in the calculations of an applicant's computer program.

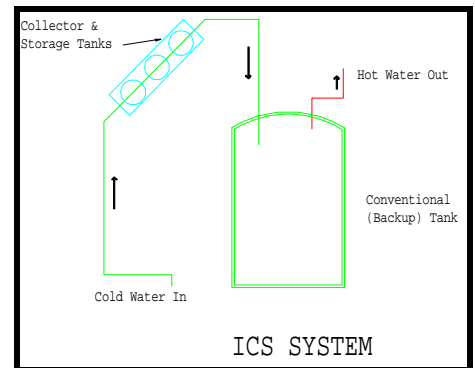
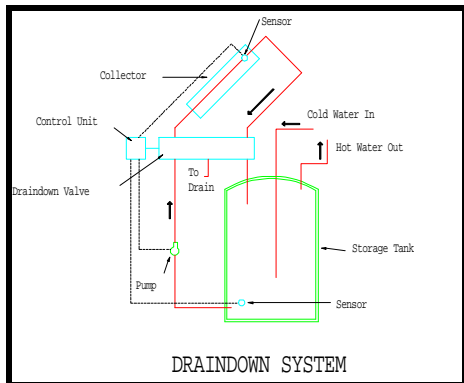
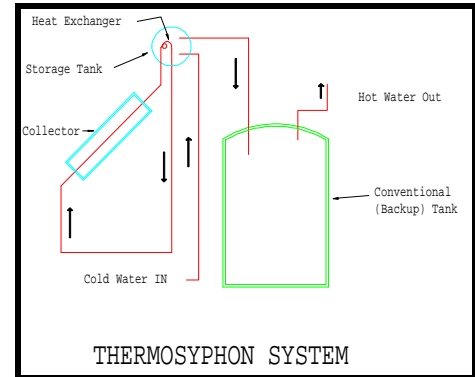
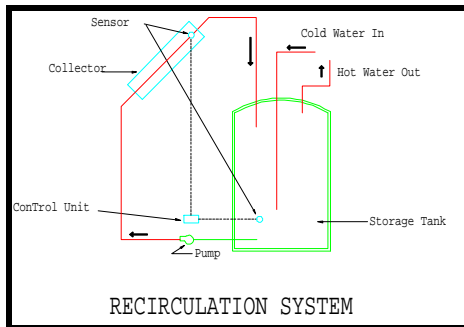
Time of Day	% of Daily Water Use	Time of Day	% of Daily Water Use
1AM	0	1PM	5.5
2AM	0	2PM	2.8
3AM	0	3PM	2.6
4AM	0	4PM	2.2
5AM	0	5PM	3.7
6AM	1.4	6PM	7.2
7AM	4.7	7PM	12.2
8AM	7.5	8PM	9.6
9AM	8.7	9PM	7.2
10AM	7.2	10PM	5.5
11AM	4.4	11PM	4.7
12PM	3.7	12AM	2.0

Average Time Distribution Of Water Usage is derived from Beckman, Klein, Duffie; Solar Heating Design By the F-Chart Method, John Wiley & Sons, Inc., New York, 1977, p.56.



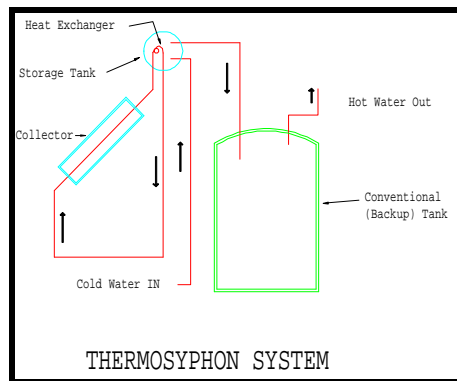
ATTACHMENT D

TYPICAL SOLAR WATER HEATING SYSTEMS



DIRECT ACTIVE SYSTEMS

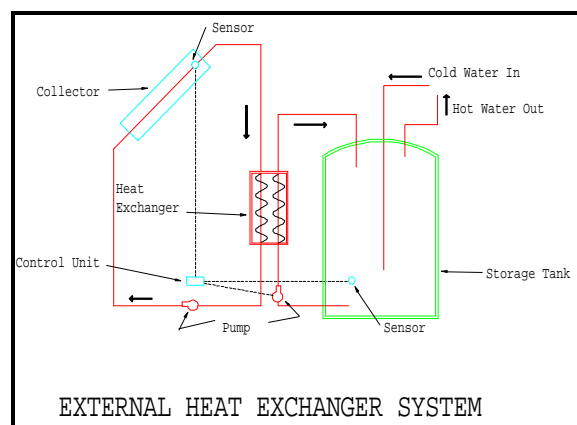
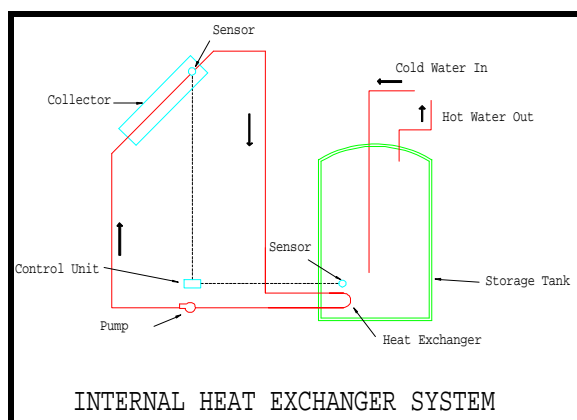
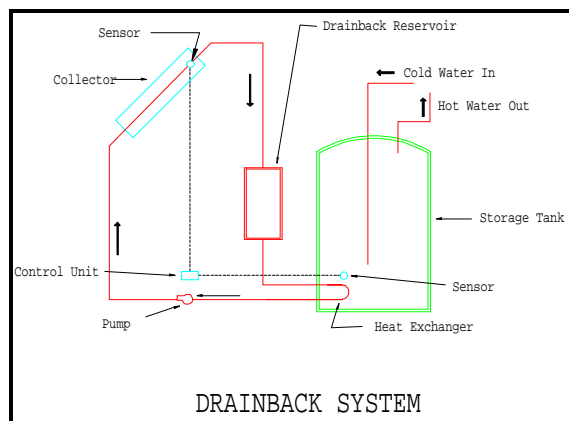
DIRECT PASSIVE SYSTEMS



INDIRECT PASSIVE SYSTEMS



## ATTACHMENT D -- cont'd.

**INDIRECT ACTIVE SYSTEMS**



## ATTACHMENT E

## F-Chart 4.1 Base Case Input Parameters

## COLLECTOR PARAMETERS

C1.	COLLECTOR AREA.....	48.00 FT2
C2.	FR-UL PRODUCT .....	.70 BTU/HR-FT2-DEG F
C3.	FR-TAU-ALPHA (NORMAL INCIDENCE) .....	.65
C6.	NUMBER OF CURVERS .....	1.00
C7.	INDEX OF REFRACTION .....	1.53
C8.	EXTINCTION COEFFICIENT $\times$ LENGTH (KL) .....	.04
C9.	INCIDENCE ANGLE MODIFIER CONSTANT .....	.00
C10.	COLLECTOR FLOW RATE * SPECIFIC HEAT/AREA .....	9.69 BTU/HR-FT2-DEG F
C12.	COLLECTOR SLOPE .....	18.50 DEGREES
C13.	COLLECTOR AZIMUTH .....	.00 DEGREES
C14.	GROUND REFLECTANCE .....	.20
C15.	INCIDENCE ANGLE MODIFIERS (10, 20, 30, 40, 50, 60, 70, 80, DEG.)	
	1.00    .99    .98    .95    .90    .80    .63    .37	

## COLLECTOR-STORE TRANSFER PARAMETERS

T2.	UA OF COLLECTOR INLET PIPE OR DUCT .....	4.25 BTU/HR-DEG F
T3.	UA OF COLLECTOR OUTLET PIPE OR DUCT .....	4.25 BTU/HR-DEG F

## STORAGE UNIT PARAMETERS

S1.	TANK CAPACITY/COLLECTOR AREA .....	13.88 BTU/DEG F-FT2
S2.	STORAGE UNIT HEIGHT/DIAMETER RATIO .....	2.00
S3.	HEAT LOSS COEFFICIENT .....	.08 BTU/HR-FT2-DEG F
S4.	ENVIRONMENT TEMP. (-1000 FOR TENV=TAMB).....	68.00 DEG F
S5.	HOT WATER AUXILIARY TANK UA .....	13.45 BTU/HR-DEG F
S6.	HOT WATER AUX TANK ENVIRONMENT TEMP.....	68.00 DEG F

## LOAD PARAMETERS

L3.	HOT WATER USE .....	50.00 GALLONS/DAY
L4.	HOT WATER SET TEMPERATURE .....	140.00 DEG F
L5.	WATER MAINS TEMPERATURE .....	65.00 DEG F

## AUXILIARY PARAMETERS

A3.	HOT WATER AUXILIARY FUEL (1=GAS, 2=ELEC, 3=OIL) .....	1.
A4.	AUXILIARY WATER HEATER EFFICIENCY .....	.76



## ATTACHMENT F

## F-Chart 4.1 Default Parameters

## COLLECTOR PARAMETERS

C1.	COLLECTOR AREA .....	538.20 FT2
C2.	FR-UL PRODUCT .....	.74 BTU/HR-FT2-DEG F
C3.	FR-TAU-ALPHA (NORMAL INCIDENCE) .....	.70
C4.	CONCENTRATION RATIO .....	2.00
C5.	CPC ACCEPTANCE HALF-ANGLE .....	30.00 DEGREES
C6.	NUMBER OF COVERS (IF 0, CIS IS USED) .....	2.00
C7.	INDEX OF REFRACTION .....	1.53
C8.	EXTINCTION COEFFICIENT X LENGTH (KL) .....	.04
C9.	INC. ANGLE MOD. CONSTANT (IF 0, C6-C USED) .....	.00
C10.	COLLECTOR FLOW RATE & SPECIFIC HEAT/AREA .....	9.69 BTU/HR-FT2-DEG F
C11.	TRACKING AXIS (1=EW, 2=NS, 3=2-AXIS) .....	3.00
C12.	COLLECTOR SLOPE .....	43.00 DEGREES
C13.	COLLECTOR AZIMUTH .....	.00 DEGREES
C14.	GROUND REFLECTANCE .....	.20
C15.	INCIDENCE ANGLE MODIFIERS (10, 20, 30, 40, 50, 60, 70, 80 DEG.)	
	1.00 .99 .98 .95 .90 .80 .63 .37	

## COLLECTOR-STORE TRANSFER PARAMETERS

T1.	EPS-CHIN OF COLLECTOR-STORE HX/COLLECTOR AREA .....	9.69 BTU/HR-FT2-DEG F
T2.	UA OF COLLECTOR INLET PIPE OR DUCT .....	.00 BTU/HR-DEG F
T3.	UA OF COLLECTOR OUTLET PIPE OR DUCT .....	.00 BTU/HR-DEG F
T4.	COLLECTOR DUCT LEAK RATE (PER CENT) .....	15.00
T5.	DUCT LEAK LOCATION (1=INLET, 2=OUTLET, 3=BOTH) .....	3.00

## STORAGE UNIT PARAMETERS

S1.	TANK CAPACITY/COLLECTOR AREA .....	17.12 BTU/DEG F-T2
S2.	STORAGE UNIT HEIGHT/DIAMETER RATIO .....	2.00
S3.	HEAT LOSS COEFFICIENT .....	.09 BTU/HR-FT2-DEG F
S4.	ENVIRONMENT TEMPERATURE (-1000 FOR TENV=TAMB) .....	68.00 DEG F
S5.	HOT WATER AUXILIARY TANK UA .....	7.58 BTU/HR-DEG F
S6.	HOT WATER AUX TANK ENVIRONMENT TEMPERATURE .....	68.00 DEG F
S7.	ROCK BED CAPACITY/COLLECTOR AREA .....	17.12 BTU/DEG F-T2
S8.	PHASE-CHANGE VOLUME/COLLECTOR AREA (X1000) .....	246.07 FT3/FT2
S9.	PHASE-CHANGE MATERIAL DENSITY .....	91.15 LB/FT3
S10.	VOID FRACTION .....	.25
S11.	SOLID PHASE SPECIFIC HEAT .....	.46 BTU/LB-DEG F
S12.	LIQUID PHASE SPECIFIC HEAT .....	.78 BTU/LB-DEG F
S13.	HEAT OF MELTING .....	107.94 BTU/LB
S14.	MELTING TEMPERATURE .....	89.60 DEG F

## DELIVERY DEVICE PARAMETERS

D1.	EPS-CHIN OF LOAD HEAT EXCHANGER .....	2274.72 BTU/HR-DEG F
D2.	MINIMUM TEMPERATURE FOR HX OPERATION .....	68.00 DEG F
D3.	DELIVERY HEAT PUMP NUMBER .....	2.00
D4.	MINIMUM HEAT PUMP ABSORBER TEMPERATURE .....	50.00 DEG F
D5.	HEAT PUMP BYPASS TEMPERATURE .....	104.00 DEG F



## ATTACHMENT F-cont'd

## LOAD PARAMETERS

L1.	BUILDING UA .....	521.29 BTU/HR-DEG F
L2.	ROOM TEMPERATURE .....	68.00 DEG F
L3.	HOT WATER USE .....	79.26 GALLONS/DAY
L4.	HOT WATER SET TEMPERATURE .....	140.00 DEG F
L5.	WATER MAINS TEMPERATURE .....	51.80 DEG F
L6.	TOTAL PROCESS OR SPACE HEATING LOAD .....	473.90 MBTU/DAY
L7.	HOURS PER DAY .....	24.00
L8.	LOAD RETURN TEMPERATURE .....	63.00 DEG F

## AUXILIARY PARAMETERS

A1.	AUXILIARY FUEL TYPE (1=GAS, 2=ELEC, 3=OIL) .....	2.
A2.	AUXILIARY DEVICE EFFICIENT .....	1.00
A3.	HOT WATER AUXILIARY FUEL (1=GAS, 2=ELEC, 3=OIL) .....	2.
A4.	AUXILIARY WATER HEATER EFFICIENCY .....	1.00
A5.	AUXILIARY HEAT PUMP NUMBER .....	1.

## ECONOMIC PARAMETERS

E1.	ECONOMIC OUTPUT DETAIL (1, 2 OR 3) .....	2.00
E2.	REFERENCE OR COMPARISON SYSTEM (1 OR 2) .....	1.00
E3.	CALCULATE RATE OF RETURN (YES=1, NO=2) .....	2.00
E4.	INCOME PRODUCING BUILDING (YES=1, 2=NO) .....	2.00
E5.	DEPRC: STR, LN,=1, DC,BAL.=2, SM-YR-DGT=3, NONE 4.....	1.00
E6.	CONSIDER FEDERAL TAX CREDITS (YES=1, 2=NO) .....	1.00
E7.	LENGTH OF ANALYSIS .....	20.00 YEARS
E8.	TAX CREDITABLE SYSTEM BASE COST .....	\$6000.00
E9.	NON-TAX CREDITABLE SYSTEM BASE COST .....	\$ .00
E10.	ANNUAL INCREASE IN PURCHASED ENERGY DEMAND .....	.00 %/YR
E11.	TERM OF MORTGAGE .....	20.00 YEARS
E12.	DOWN PAYMENT .....	10.00 %
E13.	MORTGAGE ANNUAL INTEREST RATE (% OF ORIG. INV.) .....	8.00 %
E14.	RESALE VALUE (% OF ORIGINAL INVESTMENT) .....	.00 %
E15.	ANNUAL NOMINAL (MARKET) DISCOUNT RATE .....	8.00 %
E16.	EXTRA INSUR., MAINT. IN YEAR 1 (% OF ORIG. INV.) .....	1.00 %
E17.	ANNUAL % INCREASE IN ABOVE EXPENSES .....	6.00 %
E18.	EFFECTIVE FEDERAL-STATE INCOME TAX RATE .....	35.00 %
E19.	TRUE PROP. TAX RATE PER \$ OF ORIGINAL INVEST .....	2.00 %
E20.	ANNUAL % INCREASE IN PROPERTY TAX RATE .....	6.00 %/YR
E21.	STATE CREDIT IN TIER ONE .....	24.00 %
E22.	STATE CREDIT TIER ONE BREAK .....	\$10000.00
E23.	STATE CREDIT IN TIER TWO .....	.00 %
E24.	STATE CREDIT TIER TWO BREAK .....	\$10000.00
E25.	USEFUL LIFE FOR DEPREC. PURPOSES .....	20.00 YEARS
E26.	% OF ST. LINE DEP. RATE (DC. BAL. DEPRC.) .....	150.00 %



## ATTACHMENT G

F-Chart 4.0 Input Parameters  
for the Solar Sizing Charts  
Pursuant to the Residential Building Standards

## COLLECTOR PARAMETERS

C1.	COLLECTOR AREA .....	VARIABLE
C2.	FR-UL PRODUCT .....	VARIABLE
C3.	FR-TAU-ALPHA (NORMAL INCIDENCE).....	VARIABLE
C6.	NUMBER OF COVERS .....	1.00
C7.	INDEX OF REFRACTION.....	1.53
C8.	EXTINCTION COEFFICIENT X LENGTH (KL) .....	0.04
C9.	INCIDENCE ANGLE MODIFIER CONSTANT .....	0.0
C10.	COLLECTOR FLOW RATE * SPECIFIC HEAT/AREA .....	9.69 BTU/HR-FT <sup>2</sup> -DEG F
C12.	COLLECTOR SLOPE .....	18.50 DEGREES
C13.	COLLECTOR AZIMUTH.....	0.00 DEGREES
C14.	GROUND REFLECTANCE.....	0.20 DEGREES

## COLLECTOR-STORE TRANSFER PARAMETERS

T2.	UA OF COLLECTOR INLET PIPE OR DUCT .....	4.25 BTU/HR-DEG F
T3.	UA OF COLLECTOR OUTLET PIPE OR DUCT .....	4.25 BTU/HR-DEG F

## STORAGE UNIT PARAMETERS

S1.	TANK CAPACITY/COLLECTOR AREA .....	10.40 BTU/DEG F-FT <sup>2</sup>
S2.	STORAGE UNIT HEIGHT/DIAMETER RATIO.....	2.14
S3.	HEAT LOSS COEFFICIENT .....	0.08 BTU/HR-FT <sup>2</sup> -DEG
S4.	ENVIRONMENT TEMPERATURE (-1000 FOR TENV=TAMB) .....	68.00 DEG F
S5.	HOT WATER AUXILIARY TANK UA .....	13.45 BTU/HR-DEG F
S6.	HOT WATER AUX TANK ENVIRONMENT TEMPERATURE.....	68.00 DEG F

## LOAD PARAMETERS

L3.	HOT WATER USE .....	50.00 GALLONS/DAY
L4.	HOT WATER SET TEMPERATURE.....	140.00 DEG F
L5.	WATER MAINS TEMPERATURE.....	VARIABLE BY CLIMATE ZONE

## AUXILIARY PARAMETERS

A3.	HOT WATER AUXILIARY FUEL (1=GAS, 2=ELEC, 3=OIL).....	1.
A4.	AUXILIARY WATER HEATER EFFICIENCY .....	0.76



## ATTACHMENT H

F-Chart 4.0 Assumptions  
Used for Residential  
Solar Domestic Hot Water Sizing Tables

1. Two-tank gas backup solar system
2. C12: collectors are mounted flush on the roof, with a pitch of 4 in 12
3. T2 and T3 assumes heat losses from the collector to storage piping (2.5 feet of outside piping with 3/4 inch insulation, nominal pipe diameter of 3/4 inch; and 15 feet of inside piping with 1/2 inch insulation on the collector inlet).

$$T2 = (.31 \text{ Btu/hr} \cdot \text{ft}^2 \cdot ^\circ\text{F}) \times (.6 \text{ ft}^2/\text{ft}) \times 2.5 +$$

$$(.51 \text{ Btu/hr} \cdot \text{ft}^2 \cdot ^\circ\text{F}) \times (.49 \text{ ft}^2/\text{ft}) \times 15$$

Therefore

$$T2 = UA = \frac{4.25 \text{ Btu}}{\text{hr} \cdot ^\circ\text{F}}$$

4. S1: 82 gallon storage tank.
5. S5: Assumes pump parasitic losses, backup tank skin and pilot light losses, and corrected for electrical resource energy line losses.

$$\text{Pump Energy} = 85 \text{ W pump} \times 6 \text{ hrs/day} \times 365 \text{ days/yr} \times 10,239 \text{ Btu/Wh}$$

$$= 1,906,000 \text{ Btu/year}$$

Tank Standby Losses (include pilot energy loss and standby loss of 3.3 percent/hour) :

$$\left[ 24 \text{ h} / \text{d} - \frac{(15.0 \times 10^6 \text{ Btu} / \text{yr})}{365 \text{ d} / \text{yr} \times 40,000 \text{ Btu} / \text{h}} \right] \times 365 \text{ d} / \text{yr} \times (8.25 \text{ Btu} / \text{gal} \cdot ^\circ\text{F}) \times .033 / \text{h} \times 40 \text{ gal} \times (140 - 68)^\circ\text{F}$$

$$= 6,574,500 \text{ Btu/year}$$

Therefore Hot Water Auxiliary Tank UA :

$$\frac{(1,906,000 + 6,574,500) \text{ Btu} / \text{year}}{8,760 \text{ hour} / \text{year} \times (140 - 68)^\circ\text{F}} = UA = 13.45 \text{ Btu/hr} \cdot ^\circ\text{F}$$

6. L3: Household hot water load - 50 gal./day
7. L4: Hot water set temperature - 140°F.
8. A4: Gas backup tank efficiency - 76%



## ATTACHMENT I

## Climate Zone Weather Data

CALL NO.	CITY	STATE	LATTITUDE
245	TITLE 24 ZONE 1	CA	41.00
SOLAR DATA FOR SURFACE SLOPE=.00 AZIMUTH=.00			
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
663.8	760.8	1046.8	1641.7
1947.6	1462.7	1115.8	803.8
1874.6	612.9	2103.5	497.9
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST			
637.2	489.6	543.6	462.6
313.2	198.0	214.2	313.2
408.6	379.8	358.2	496.8
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.			
42.8	48.2	46.4	50.0
51.8	53.6	48.2	51.8
CALL NO.	CITY	STATE	LATTITUDE
246	TITLE 24 ZONE 2	CA	38.50
SOLAR DATA FOR SURFACE SLOPE=.00 AZIMUTH=.00			
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
752.8	1082.8	1477.7	2033.6
2488.5	2092.6	1792.6	1262.7
2120.6	829.9	2429.5	610.8
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST			
586.8	426.6	385.2	277.2
32.4	21.6	45.0	158.4
158.4	349.2	531.0	79.2
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.			
44.6	48.2	51.8	55.4
59.0	64.4	46.4	59.0
51.8	46.4	59.0	51.8
CALL NO.	CITY	STATE	LATTITUDE
247	TITLE 24 ZONE 3	CA	37.70
SOLAR DATA FOR SURFACE SLOPE=.00 AZIMUTH=.00			
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
843.9	904.8	1443.7	2040.5
2306.6	2087.5	1580.7	1086.7
2272.5	843.9	2392.5	590.9
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.			
518.4	410.4	403.2	207.0
111.6	41.4	102.6	144.0
223.2	262.8	120.8	478.8
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.			
48.2	50.0	51.8	57.2
57.2	60.8	48.2	57.2
59.0	55.4	48.2	59.0



ATTACHMENT I cont'd.

CALL NO.	CITY	STATE	LATTITUDE
248	TITLE 24 ZONE 4	CA	37.40
SOLAR DATA FOR SURFACE SLOPE=.00		AZIMUTH=.00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
766.8	1099.8	1491.7	2046.6
2492.5	2100.6	1808.7	1280.7
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.		2125.6	2431.5
527.4	318.6	372.6	843.9
34.2	21.6	64.8	622.9
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.		253.8	255.6
46.4	53.6	51.8	72.0
66.2	66.2	64.4	331.2
		60.8	534.6
		57.2	57.2
		60.8	64.4
		53.6	48.2

CALL NO.	CITY	STATE	LATTITUDE
249	TITLE 24 ZONE 5	CA	34.90
SOLAR DATA FOR SURFACE SLOPE=.00		AZIMUTH=.00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
843.9	1100.7	1549.7	1919.6
2368.5	2108.6	1687.6	2043.6
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.		1365.7	2394.5
464.4	381.6	354.6	931.8
91.8	93.6	106.2	248.4
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.		313.2	216.0
48.2	51.8	53.6	163.8
60.8	60.8	60.8	246.6
		59.0	363.6
		57.2	57.2
		55.4	51.8

CALL NO.	CITY	STATE	LATTITUDE
250	TITLE 24 ZONE 6	CA	33.80
SOLAR DATA FOR SURFACE SLOPE=.00		AZIMUTH=.00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
916.8	1282.8	1593.7	1949.6
2312.5	2089.6	1682.7	1992.6
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.		1358.7	2123.5
338.4	262.8	194.4	138.6
.0	.0	1.8	95.4
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.		18.0	.0
53.6	55.4	59.0	120.6
71.6	73.4	71.6	315.0
		60.8	60.8
		62.6	68.0
		66.2	55.4



CALL NO.	CITY	STATE	LATTITUDE
251	TITLE 24 ZONE 7	CA	32.70
SOLAR DATA FOR SURFACE SLOPE=.00		AZIMUTH=.00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
1012.8	1142.8	1575.6	1869.6
2232.5	2130.6	1749.6	1387.7
2031.6			997.6
1927.5			871.5
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.			
268.2	246.6	297.0	122.4
1.8	.0	1.8	32.4
91.8			163.8
46.8			262.8
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.			
55.4	55.4	55.4	60.8
66.2	69.8	66.2	64.4
60.8			59.0
62.6			55.4
CALL NO.	CITY	STATE	LATTITUDE
252	TITLE 24 ZONE 8	CA	33.70
SOLAR DATA FOR SURFACE SLOPE=.00		AZIMUTH=.00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
974.8	1205.7	1636.7	2077.6
2477.5	2202.5	1890.6	1429.7
2249.5			992.8
2180.5			958.5
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.			
370.8	280.8	199.8	126.0
3.6	.0	.0	41.4
66.6			178.2
5.4			243.0
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.			
51.8	53.6	57.2	60.8
71.6	69.8	71.6	64.4
64.4			57.2
66.2			57.2
CALL NO.	CITY	STATE	LATTITUDE
253	TITLE 24 ZONE 9	CA	34.30
SOLAR DATA FOR SURFACE SLOPE=.00		AZIMUTH=.00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
964.8	1196.8	1530.7	2072.6
2477.5	2200.6	1884.6	1421.7
2248.5			983.8
2184.6			946.8
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.			
352.8	318.6	266.4	171.0
1.8	.0	1.8	46.8
79.2			127.8
3.6			329.4
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.			
51.8	51.8	53.6	59.0
71.6	69.8	68.0	62.6
62.6			59.0
64.4			53.6
CALL NO.	CITY	STATE	LATTITUDE
254	TITLE 24 ZONE 10	CA	33.90
SOLAR DATA FOR SURFACE SLOPE=.00		AZIMUTH=.00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
891.8	1212.8	1604.7	1926.6
2276.5	2085.6	1796.6	1360.7
2021.6			1070.8
2195.6			892.3
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.			
408.6	347.4	286.2	194.4
.0	.0	5.4	32.4
102.6			169.2
30.6			349.2
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.			
51.8	51.8	55.4	59.0
75.2	77.0	73.4	66.2
64.4			57.2
69.8			53.8
CALL NO.	CITY	STATE	LATTITUDE
255	TITLE 24 ZONE 11	CA	40.20
SOLAR DATA FOR SURFACE SLOPE = .00		AZIMUTH = .00	
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
568.8	866.8	1318.7	1952.6
2685.4	2350.5	1855.6	1250.7
2338.5			736.8
2541.6			492.9
LONG TERM MONTHLY AVERAGE DEG=F DAYS, JAN FIRST.			
667.8	424.8	421.2	221.4
.0	.0	10.8	81.0
43.2			403.2
7.2			608.49



LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG F, JAN FIRST.

42.8	50.0	51.8	57.2	68.0	77.0
82.4	80.6	75.2	64.4	51.8	44.6

CALL NO.	CITY	STATE	LATITUDE
256	TITLE 24 ZONE 12	CA	38.50

SOLAR DATA FOR SURFACE SLOPE = .00 AZIMUTH = .00

DATA IN BTU/FT2/DAY, LISTED JAN FIRST

700.9	752.8	1476.7	2193.5	2453.5	2812.4
2718.5	2422.5	1938.6	1108.7	879.9	474.9

LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.

725.4	496.8	439.2	133.2	93.6	7.2
.0	.0	3.6	104.4	311.4	592.2

LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG-F, JAN FIRST.

41.0	46.4	50.0	60.8	60.8	69.8
71.6	73.4	68.0	60.8	53.6	44.6

CALL NO.	CITY	STATE	LATITUDE
257	TITLE 24 ZONE 13	CA	36.80

SOLAR DATA FOR SURFACE SLOPE = .00 AZIMUTH = .00

DATA IN BTU/FT2/DAY, LISTED JAN FIRST

669.8	1032.8	1589.6	2116.6	2501.5	2720.4
2707.5	2398.5	2023.5	1455.7	910.8	569.9

LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.

653.4	421.2	277.2	190.8	39.6	7.2
.0	.0	10.8	59.4	358.2	682.2

LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG-F, JAN FIRST.

42.8	50.0	55.4	59.0	68.0	77.0
82.4	78.8	73.4	64.4	51.8	42.8

CALL NO.	CITY	STATE	LATITUDE
258	TITLE 24 ZONE 14	CA	35.70

SOLAR DATA FOR SURFACE SLOPE = .00 AZIMUTH = .00

DATA IN BTU/FT2/DAY, LISTED JAN FIRST

877.8	1187.8	1722.7	2278.6	2585.4	2732.5
2581.5	2459.5	1985.6	1504.7	1022.8	883.8

LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.

707.4	457.2	171.0	104.4	19.8	.0
.0	.0	.0	52.2	372.6	604.8

LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG-F, JAN FIRST.

41.0	48.2	59.0	64.4	71.6	86.0
89.6	86.0	80.6	66.2	51.8	44.6



CALL NO.	CITY	STATE	LATITUDE
259	TITLE 24 ZONE 15	CA	32.80
SOLAR DATA FOR SURFACE SLOPE = .00 AZIMUTH = .00			
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
	1150.7	1428.7	1830.6
	2373.5	2280.5	2032.6
			2326.5
			2533.5
			2632.4
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.			
	334.8	203.4	106.2
	.0	.0	.0
			30.6
			.0
			73.8
			281.0
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG-F, JAN FIRST.			
	53.6	57.2	64.4
	91.4	91.4	86.0
			71.6
			75.2
			78.8
			86.0
			62.6
			55.4
CALL NO.	CITY	STATE	LATITUDE
260	TITLE 24 ZONE 16	CA	41.30
SOLAR DATA FOR SURFACE SLOPE = .00 AZIMUTH = .00			
DATA IN BTU/FT2/DAY, LISTED JAN FIRST			
	568.8	798.9	1309.7
	2602.4	2234.6	1786.7
			1779.6
			2198.5
			2480.5
LONG TERM MONTHLY AVERAGE DEG-F DAYS, JAN FIRST.			
	1004.4	720.0	646.2
	30.6	64.8	111.6
			543.6
			437.4
			304.2
			687.6
			156.6
LONG TERM MONTHLY AVERAGE AMBIENT TEMPERATURE, DEG-F, JAN FIRST.			
	32.0	39.2	44.6
	71.6	68.0	62.6
			46.4
			51.8
			55.4
			62.6
			42.8
			37.4



Attachment J Determining Energy Savings from a Passive Solar Water Heater  
(Alternative Calculation Method for Passive Solar Credit)

Calculating the performance of a passive solar water heater is done by using test results published by the Solar Rating & Certification Corporation (SRCC) for passive solar water heaters and calculating the amount of energy which can be contributed by the equipment using local weather data. The calculation method is as follows:

Step 1. Calculate temperature difference from SRCC data:

$$T_{SRCC} = [Q_{SAV} / (100 \text{ gal/day} \times 8.25 \text{ Btu/gal-}^{\circ}\text{F})] + [Q_{CAP} / (V_t \times 8.25 \text{ Btu/gal-}^{\circ}\text{F})]$$

Where:  $Q_{SAV}$  (Btu/day) = from SRCC test results  
 $Q_{CAP}$  (Btu) = from SRCC test results  
 $V_t$  (gal) = total volume of solar storage tank

Step 2. Calculate energy losses during SRCC test:

$$Q_{LOSS, SRCC} = T_{SRCC} \times 16 \text{ hr/day} \times L \text{ Btu/hr-}^{\circ}\text{F}$$

Where: 16 = number of hours system is losing heat  
 $L$  (Heat Loss Coefficient, Btu/hr- $^{\circ}\text{F}$  from SRCC test results)

Step 3. Calculate energy collected during the SRCC test:

$$Q_{TOTAL, SRCC} = Q_{SAV} + Q_{LOSS, SRCC}$$

Step 4. Adjust energy collected to climate zone insolation values (see Table J-1)

$$Q_{TOTAL, LOCAL} = 1204 + [(Q_{TOTAL, SRCC} - 1204) / 1500] \times \text{CZ insolation}$$

Table J-1

Climate Zone	CZ Insolation	Climate Zone	CZ Insolation
1	1340	9	1747
2	1658	10	1919
3	1684	11	1706
4	1734	12	1772
5	1753	13	1845
6	1724	14	1988
7	1748	15	2007
8	1768	16	1788

Step 5. Determine  $T_{TANK, LOCAL}$ , average tank temperature delivered to the site:

$$Q_{TOTAL, LOCAL} = (50 \text{ gal/day}) \times (8.25 \text{ Btu/gal-}^{\circ}\text{F}) \times (T_{TANK, LOCAL} - \text{CZ Water Main Temp}) \\ + 16 \text{ hrs/day} \times L \times (T_{TANK, LOCAL} - \text{CZ Ambient Air Temp})$$

Solving for  $T_{TANK, LOCAL}$ :

$$T_{TANK, LOCAL} = (A_1 + A_2 + Q_{TOTAL, LOCAL}) / (A_3 + A_4)$$

Where:  $A_1 = (50 \text{ gal/day}) \times (8.25 \text{ Btu/gal-}^{\circ}\text{F}) \times (\text{CZ Water Main Temp})$   
 $A_2 = 16 \text{ hrs/day} \times L \times (\text{CZ Ambient Air Temp})$   
 $A_3 = (50 \text{ gal/day}) \times (8.25 \text{ Btu/gal-}^{\circ}\text{F})$   
 $A_4 = 16 \text{ hrs/day} \times L$



## CZ Water Main Temp and CZ Ambient Air Temp from Table J-2

Table J-2  
Climate Zone Water Main & Ambient Air Temp

Climate Zone	Ambient Air Temp °F	Water Main Temp °F
1	52.1	60
2	57.9	65
3	56.9	65
4	59.6	65
5	60.3	65
6	63.5	70
7	62.9	70
8	63	70
9	63.6	70
10	63.3	70
11	62.8	65
12	60.3	65
13	62.3	65
14	55.9	65
15	72.6	70
16	42.8	60

Step 6. Determine energy losses at the site:

$$Q_{\text{LOSS, LOCAL}} = L \times 16 \text{ hrs} \times (T_{\text{TANK, LOCAL}} - \text{CZ Ambient Air Temp})$$

Step 7. Determine energy used by electric resistance freeze protection devices:

$$\text{ERP} = (\text{Freeze days/yr} + 4) \times (\text{Collector Area}) \times (0.5 \text{ kBtu /ft}^2 \text{ -freeze day})$$

This is calculated only if the system uses electric resistance freeze protection.

Step 8. Calculate system total annual energy contribution (mmBtu/yr):

$$\{(Q_{\text{TOTAL, LOCAL}} - Q_{\text{LOSS, LOCAL}}) \times 0.365 \times 0.001 - \text{ERP}\} \times (\text{No. of Dwelling Units})$$

Step 9. Calculate Standard Recovery Load, SRL (mmBtu/yr):

$$\text{SRL}_k = \sum_{i=1}^n \{0.0855347(\text{CFA}_i / 1000)^2 + 3.61307 (\text{CFA}_i / 1000) + 6.036\} / \text{number of systems}$$

Step 10: Determine Distribution System Credit/Penalty:

Select Distribution System Credit/Penalty from Table J-3.

**Table J-3: Distribution System Credit/Penalty<sup>1</sup> (per worksheet)**



Standard Recovery Load	Point- of-Use	Hot Water Recovery <sup>1</sup>	Pipe Insulation <sup>1</sup>	Recirculation Systems				
				Time/Temp	Demand	Time	Temp	Cont
< 6.3	1.1	1.1	0.5	0.2	0.1	-1.7	-0.3	-3.1
6.3 - 6.99	1.2	1.2	0.5	0.2	0.1	-1.8	-0.3	-3.4
7.0 - 7.49	1.3	1.3	0.5	0.3	0.1	-1.9	-0.4	-3.7
7.5 - 7.99	1.4	1.4	0.6	0.3	0.1	-2.1	-0.4	-3.9
8.0 - 8.49	1.5	1.5	0.6	0.3	0.1	-2.2	-0.4	-4.2
8.5 - 8.99	1.6	1.6	0.6	0.3	0.1	-2.3	-0.4	-4.4
9.0 - 9.49	1.7	1.7	0.7	0.3	0.2	-2.5	-0.5	-4.7
9.5 - 9.99	1.7	1.7	0.7	0.4	0.2	-2.6	-0.5	-5.0
10.0 - 10.99	1.8	1.8	0.8	0.4	0.2	-2.8	-0.5	-5.2
11.0 - 11.99	2.0	2.0	0.8	0.4	0.2	-3.0	-0.6	-5.7
12.0 - 12.99	2.2	2.2	0.9	0.5	0.2	-3.3	-0.6	-6.3
13.0 - 13.99	2.4	2.4	1.0	0.5	0.2	-3.6	-0.7	-6.8
14.0 - 15.99	2.6	2.6	1.1	0.5	0.2	-3.9	-0.7	-7.3
16.0 - 17.99	2.9	2.9	1.2	0.6	0.3	-4.4	-0.8	-8.4
18.0 - 19.99	3.3	3.3	1.4	0.7	0.3	-5.0	-0.9	-9.4
20.0 - 21.99	3.7	3.7	1.5	0.8	0.3	-5.5	-1.0	-10.4
22.0 - 23.99	4.0	4.0	1.7	0.8	0.4	-6.1	-1.1	-11.5
24.0 - 25.99	4.4	4.4	1.8	0.9	0.4	-6.6	-1.2	-12.5
26.0+	4.8	4.8	2.0	1.0	0.4	-7.2	-1.4	-13.6

1. Hot water recovery and pipe insulation credits may only be applied to non-recirculating systems and demand recirculating systems. All other recirculating systems must have pipe insulation.

Step 11: Adjust Recovery Load:

$$\text{Adjust Recovery Load} = \text{SRL (from Step 9)} - \text{Distribution System Credit/Penalty (from Step 10)} \\ - \text{System total annual energy contribution (from Step 8)}$$

The adjusted recovery load must be greater than 3 mmBtu/yr, (if the result is less than 3 assign a value of three.)

Step 12: Estimate Basic Energy Use

Estimate basic energy use using the adjust recovery load from step 11 and Table J-4

Step 13: Calculate water heating energy budget (mmBtu/yr):

$$\text{Water heating energy budget} = 0.00485 \times \sum_{i=1}^N \text{CFA}_i + 16.37 N$$

Step 14: Calculate Solar Savings Fraction:

$$\text{Solar Savings Fraction} = 1 - \text{Basic Energy Use (Step 12)} / \text{Water Heating Energy Budget (Step 13)}$$



Table J-4A: Basic Energy Use (BEU) - Storage Gas Heater [no interpolation]

Adjusted Load	Energy Factor																						
	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.60	0.62	0.64	0.66	0.68	0.70	0.74	0.78	0.82
3.0	19.9	18.5	17.3	16.2	15.3	14.4	13.7	13.0	12.4	11.8	11.3	10.8	10.4	10.0	9.3	8.7	8.1	7.7	7.2	6.8	6.2	5.7	5.2
3.2	19.6	18.3	17.2	16.2	15.3	14.5	13.8	13.1	12.6	12.0	11.5	11.1	10.6	10.3	9.6	8.9	8.4	7.9	7.5	7.1	6.5	5.9	5.5
3.4	19.4	18.2	17.2	16.2	15.4	14.6	14.0	13.3	12.8	12.2	11.8	11.3	10.9	10.5	9.8	9.2	8.7	8.2	7.8	7.4	6.7	6.2	5.7
3.6	19.3	18.2	17.2	16.3	15.5	14.8	14.2	13.6	13.0	12.5	12.0	11.6	11.2	10.8	10.1	9.5	9.0	8.5	8.1	7.7	7.0	6.4	5.9
3.8	19.3	18.2	17.3	16.5	15.7	15.0	14.4	13.8	13.2	12.7	12.3	11.8	11.4	11.1	10.4	9.8	9.2	8.8	8.3	7.9	7.3	6.7	6.2
4.0	19.3	18.3	17.4	16.6	15.9	15.2	14.6	14.0	13.5	13.0	12.5	12.1	11.7	11.3	10.7	10.1	9.5	9.0	8.6	8.2	7.5	6.9	6.4
4.2	19.4	18.4	17.6	16.8	16.1	15.4	14.8	14.2	13.7	13.2	12.8	12.4	12.0	11.6	10.9	10.3	9.8	9.3	8.9	8.5	7.8	7.2	6.7
4.4	19.5	18.6	17.7	17.0	16.3	15.6	15.0	14.5	14.0	13.5	13.1	12.6	12.3	11.9	11.2	10.6	10.1	9.6	9.1	8.7	8.0	7.4	6.9
4.6	19.6	18.7	17.9	17.2	16.5	15.9	15.3	14.7	14.2	13.8	13.3	12.9	12.5	12.2	11.5	10.9	10.3	9.8	9.4	9.0	8.3	7.7	7.1
4.8	19.8	18.9	18.1	17.4	16.7	16.1	15.5	15.0	14.5	14.0	13.6	13.2	12.8	12.4	11.8	11.2	10.6	10.1	9.7	9.3	8.5	7.9	7.4
5.0	19.9	19.1	18.3	17.6	17.0	16.4	15.8	15.3	14.8	14.3	13.9	13.5	13.1	12.7	12.0	11.4	10.9	10.4	9.9	9.5	8.8	8.1	7.6
5.2	20.1	19.3	18.5	17.8	17.2	16.6	16.0	15.5	15.0	14.6	14.1	13.7	13.3	13.0	12.3	11.7	11.1	10.6	10.2	9.8	9.0	8.4	7.8
5.4	20.3	19.5	18.8	18.1	17.4	16.9	16.3	15.8	15.3	14.8	14.4	14.0	13.6	13.2	12.6	12.0	11.4	10.9	10.4	10.0	9.3	8.6	8.1
5.6	20.5	19.7	19.0	18.3	17.7	17.1	16.6	16.0	15.6	15.1	14.7	14.3	13.9	13.5	12.8	12.2	11.7	11.2	10.7	10.3	9.5	8.9	8.3
5.8	20.7	19.9	19.2	18.6	17.9	17.4	16.8	16.3	15.8	15.4	14.9	14.5	14.1	13.8	13.1	12.5	11.9	11.4	11.0	10.5	9.8	9.1	8.5
6.0	20.9	20.2	19.5	18.8	18.2	17.6	17.1	16.6	16.1	15.6	15.2	14.8	14.4	14.0	13.4	12.8	12.2	11.7	11.2	10.8	10.0	9.3	8.7
6.2	21.2	20.4	19.7	19.1	18.4	17.9	17.3	16.8	16.3	15.9	15.5	15.1	14.7	14.3	13.6	13.0	12.5	11.9	11.5	11.0	10.2	9.6	9.0
6.4	21.4	20.6	20.0	19.3	18.7	18.1	17.6	17.1	16.6	16.2	15.7	15.3	14.9	14.6	13.9	13.3	12.7	12.2	11.7	11.3	10.5	9.8	9.2
6.6	21.6	20.9	20.2	19.6	19.0	18.4	17.9	17.4	16.9	16.4	16.0	15.6	15.2	14.8	14.2	13.5	13.0	12.4	12.0	11.5	10.7	10.0	9.4
6.8	21.9	21.1	20.5	19.8	19.2	18.7	18.1	17.6	17.1	16.7	16.3	15.9	15.5	15.1	14.4	13.8	13.2	12.7	12.2	11.8	10.9	10.2	9.6
7.0	22.1	21.4	20.7	20.1	19.5	18.9	18.4	17.9	17.4	17.0	16.5	16.1	15.7	15.4	14.7	14.1	13.5	12.9	12.5	12.0	11.2	10.5	9.8
7.2	22.3	21.6	21.0	20.3	19.7	19.2	18.6	18.1	17.7	17.2	16.8	16.4	16.0	15.6	14.9	14.3	13.7	13.2	12.7	12.2	11.4	10.7	10.1
7.4	22.6	21.9	21.2	20.6	20.0	19.4	18.9	18.4	17.9	17.5	17.1	16.7	16.3	15.9	15.2	14.6	14.0	13.4	12.9	12.5	11.6	10.9	10.3
7.6	22.8	22.1	21.5	20.8	20.3	19.7	19.2	18.7	18.2	17.8	17.3	16.9	16.5	16.2	15.5	14.8	14.2	13.7	13.2	12.7	11.9	11.1	10.5
7.8	23.1	22.4	21.7	21.1	20.5	20.0	19.4	18.9	18.5	18.0	17.6	17.2	16.8	16.4	15.7	15.1	14.5	13.9	13.4	13.0	12.1	11.4	10.7
8.0	23.3	22.6	22.0	21.4	20.8	20.2	19.7	19.2	18.7	18.3	17.8	17.4	17.0	16.7	16.0	15.3	14.7	14.2	13.7	13.2	12.3	11.6	10.9
8.2	23.6	22.9	22.2	21.6	21.0	20.5	20.0	19.5	19.0	18.5	18.1	17.7	17.3	16.9	16.2	15.6	15.0	14.4	13.9	13.4	12.6	11.8	11.1
8.4	23.8	23.1	22.5	21.9	21.3	20.7	20.2	19.7	19.3	18.8	18.4	18.0	17.6	17.2	16.5	15.8	15.2	14.7	14.2	13.7	12.8	12.0	11.3
8.6	24.1	23.4	22.8	22.1	21.6	21.0	20.5	20.0	19.5	19.1	18.6	18.2	17.8	17.4	16.7	16.1	15.5	14.9	14.4	13.9	13.0	12.2	11.6
8.8	24.3	23.7	23.0	22.4	21.8	21.3	20.7	20.2	19.8	19.3	18.9	18.5	18.1	17.7	17.0	16.3	15.7	15.2	14.6	14.1	13.2	12.5	11.8
9.0	24.6	23.9	23.3	22.7	22.1	21.5	21.0	20.5	20.0	19.6	19.1	18.7	18.3	18.0	17.2	16.6	16.0	15.4	14.9	14.4	13.5	12.7	12.0
9.2	24.8	24.2	23.5	22.9	22.3	21.8	21.3	20.8	20.3	19.8	19.4	19.0	18.6	18.2	17.5	16.8	16.2	15.6	15.1	14.6	13.7	12.9	12.2
9.4	25.1	24.4	23.8	23.2	22.6	22.0	21.5	21.0	20.5	20.1	19.7	19.2	18.8	18.5	17.7	17.1	16.4	15.9	15.3	14.8	13.9	13.1	12.4
9.6	25.4	24.7	24.0	23.4	22.9	22.3	21.8	21.3	20.8	20.3	19.9	19.5	19.1	18.7	18.0	17.3	16.7	16.1	15.6	15.1	14.1	13.3	12.6
9.8	25.6	24.9	24.3	23.7	23.1	22.6	22.0	21.5	21.1	20.6	20.2	19.7	19.3	19.0	18.2	17.6	16.9	16.3	15.8	15.3	14.4	13.5	12.8
10.0	25.9	25.2	24.6	23.9	23.4	22.8	22.3	21.8	21.3	20.9	20.4	20.0	19.6	19.2	18.5	17.8	17.2	16.6	16.0	15.5	14.6	13.8	13.0
10.5	26.5	25.8	25.2	24.6	24.0	23.5	22.9	22.4	22.0	21.5	21.0	20.6	20.2	19.8	19.1	18.4	17.8	17.2	16.6	16.1	15.1	14.3	13.5
11.0	27.1	26.5	25.8	25.2	24.7	24.1	23.6	23.1	22.6	22.1	21.7	21.2	20.8	20.4	19.7	19.0	18.4	17.7	17.2	16.6	15.7	14.8	14.0
11.5	27.8	27.1	26.5	25.9	25.3	24.7	24.2	23.7	23.2	22.7	22.3	21.9	21.5	21.1	20.3	19.6	18.9	18.3	17.7	17.2	16.2	15.3	14.5
12.0	28.4	27.7	27.1	26.5	25.9	25.4	24.8	24.3	23.8	23.4	22.9	22.5	22.1	21.7	20.9	20.2	19.5	18.9	18.3	17.8	16.8	15.9	15.1
12.5	29.0	28.4	27.7	27.1	26.6	26.0	25.5	25.0	24.5	24.0	23.5	23.1	22.7	22.3	21.5	20.8	20.1	19.5	18.9	18.3	17.3	16.4	15.6
13.0	29.7	29.0	28.4	27.8	27.2	26.6	26.1	25.6	25.1	24.6	24.1	23.7	23.3	22.9	22.1	21.3	20.7	20.0	19.4	18.9	17.8	16.9	16.0
13.5	30.3	29.6	29.0	28.4	27.8	27.2	26.7	26.2	25.7	25.2	24.7	24.3	23.9	23.5	22.7	21.9	21.2	20.6	20.0	19.4	18.3	17.4	16.5
14.0	30.9	30.3	29.6	29.0	28.4	27.9	27.3	26.8	26.3	25.8	25.3	24.9	24.5	24.0	23.2	22.5	21.8	21.1	20.5	19.9	18.9	17.9	17.0
14.5	31.6	30.9	30.3	29.6	29.0	28.5	27.9	27.4	26.9	26.4	25.9	25.5	25.1	24.6	23.8	23.1	22.4	21.7	21.1	20.5	19.4	18.4	17.5
15.0	32.2	31.5	30.9	30.3	29.7	29.1	28.5	28.0	27.5	27.0	26.5	26.1	25.6	25.2									



**Table J-4B: Basic Energy Use (BEU) - Storage Electric Heater [no interpolation]**

Adjusted Recover	Energy Factor																							
	Load	0.77	0.78	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99
	3.0	22.4	21.1	20.0	19.0	18.1	17.2	16.5	15.8	15.2	14.6	14.0	13.5	13.0	12.6	12.2	11.8	11.5	11.1	10.8	10.5	10.2	9.9	9.7
	3.2	23.0	21.8	20.7	19.7	18.8	18.0	17.2	16.5	15.9	15.3	14.7	14.2	13.8	13.3	12.9	12.5	12.1	11.8	11.5	11.1	10.8	10.6	10.3
	3.4	23.6	22.4	21.3	20.4	19.5	18.7	17.9	17.2	16.6	16.0	15.4	14.9	14.4	14.0	13.6	13.2	12.8	12.4	12.1	11.8	11.5	11.2	10.9
	3.6	24.2	23.1	22.0	21.1	20.2	19.4	18.6	17.9	17.3	16.7	16.1	15.6	15.1	14.7	14.2	13.8	13.5	13.1	12.7	12.4	12.1	11.8	11.5
	3.8	24.8	23.7	22.7	21.7	20.9	20.1	19.3	18.6	18.0	17.4	16.8	16.3	15.8	15.4	14.9	14.5	14.1	13.7	13.4	13.1	12.7	12.4	12.1
	4.0	25.5	24.4	23.3	22.4	21.6	20.8	20.0	19.3	18.7	18.1	17.5	17.0	16.5	16.0	15.6	15.2	14.8	14.4	14.0	13.7	13.4	13.1	12.8
	4.2	26.1	25.0	24.0	23.1	22.2	21.4	20.7	20.0	19.4	18.8	18.2	17.7	17.2	16.7	16.3	15.8	15.4	15.0	14.7	14.3	14.0	13.7	13.4
	4.4	26.7	25.6	24.7	23.8	22.9	22.1	21.4	20.7	20.1	19.5	18.9	18.4	17.8	17.4	16.9	16.5	16.1	15.7	15.3	15.0	14.6	14.3	14.0
	4.6	27.3	26.3	25.3	24.4	23.6	22.8	22.1	21.4	20.7	20.1	19.6	19.0	18.5	18.0	17.6	17.1	16.7	16.3	15.9	15.6	15.2	14.9	14.6
	4.8	28.0	26.9	26.0	25.1	24.3	23.5	22.7	22.1	21.4	20.8	20.2	19.7	19.2	18.7	18.2	17.8	17.4	17.0	16.6	16.2	15.9	15.5	15.2
	5.0	28.6	27.6	26.6	25.7	24.9	24.1	23.4	22.7	22.1	21.5	20.9	20.4	19.8	19.3	18.9	18.4	18.0	17.6	17.2	16.8	16.5	16.1	15.8
	5.2	29.2	28.2	27.3	26.4	25.6	24.8	24.1	23.4	22.7	22.1	21.6	21.0	20.5	20.0	19.5	19.1	18.6	18.2	17.8	17.5	17.1	16.7	16.4
	5.4	29.8	28.8	27.9	27.0	26.2	25.5	24.7	24.1	23.4	22.8	22.2	21.7	21.1	20.6	20.2	19.7	19.3	18.9	18.5	18.1	17.7	17.4	17.0
	5.6	30.4	29.5	28.5	27.7	26.9	26.1	25.4	24.7	24.1	23.5	22.9	22.3	21.8	21.3	20.8	20.3	19.9	19.5	19.1	18.7	18.3	18.0	17.6
	5.8	31.0	30.1	29.2	28.3	27.5	26.8	26.0	25.4	24.7	24.1	23.5	23.0	22.4	21.9	21.4	21.0	20.5	20.1	19.7	19.3	18.9	18.6	18.2
	6.0	31.6	30.7	29.8	29.0	28.2	27.4	26.7	26.0	25.4	24.7	24.2	23.6	23.1	22.6	22.1	21.6	21.2	20.7	20.3	19.9	19.5	19.2	18.8
	6.2	32.3	31.3	30.4	29.6	28.8	28.0	27.3	26.7	26.0	25.4	24.8	24.2	23.7	23.2	22.7	22.2	21.8	21.4	20.9	20.5	20.2	19.8	19.4
	6.4	32.9	31.9	31.1	30.2	29.4	28.7	28.0	27.3	26.6	26.0	25.4	24.9	24.3	23.8	23.3	22.9	22.4	22.0	21.6	21.2	20.8	20.4	20.0
	6.6	33.5	32.5	31.7	30.8	30.1	29.3	28.6	27.9	27.3	26.7	26.1	25.5	25.0	24.5	24.0	23.5	23.0	22.6	22.2	21.8	21.4	21.0	20.6
	6.8	34.1	33.2	32.3	31.5	30.7	29.9	29.2	28.6	27.9	27.3	26.7	26.2	25.6	25.1	24.6	24.1	23.7	23.2	22.8	22.4	22.0	21.6	21.2
	7.0	34.7	33.8	32.9	32.1	31.3	30.6	29.9	29.2	28.6	27.9	27.3	26.8	26.2	25.7	25.2	24.7	24.3	23.8	23.4	23.0	22.6	22.2	21.8
	7.2	35.3	34.4	33.5	32.7	31.9	31.2	30.5	29.8	29.2	28.6	28.0	27.4	26.9	26.3	25.8	25.4	24.9	24.4	24.0	23.6	23.2	22.8	22.4
	7.4	35.9	35.0	34.1	33.3	32.6	31.8	31.1	30.5	29.8	29.2	28.6	28.0	27.5	27.0	26.5	26.0	25.5	25.1	24.6	24.2	23.8	23.4	23.0
	7.6	36.5	35.6	34.7	33.9	33.2	32.4	31.7	31.1	30.4	29.8	29.2	28.7	28.1	27.6	27.1	26.6	26.1	25.7	25.2	24.8	24.4	24.0	23.6
	7.8	37.0	36.2	35.3	34.5	33.8	33.1	32.4	31.7	31.1	30.4	29.8	29.3	28.7	28.2	27.7	27.2	26.7	26.3	25.8	25.4	25.0	24.6	24.2
	8.0	37.6	36.8	35.9	35.2	34.4	33.7	33.0	32.3	31.7	31.1	30.5	29.9	29.4	28.8	28.3	27.8	27.3	26.9	26.4	26.0	25.6	25.2	24.8
	8.2	38.2	37.4	36.5	35.8	35.0	34.3	33.6	32.9	32.3	31.7	31.1	30.5	30.0	29.4	28.9	28.4	28.0	27.5	27.0	26.6	26.2	25.8	25.4
	8.4	38.8	37.9	37.1	36.4	35.6	34.9	34.2	33.5	32.9	32.3	31.7	31.1	30.6	30.0	29.5	29.0	28.6	28.1	27.7	27.2	26.8	26.4	26.0
	8.6	39.4	38.5	37.7	37.0	36.2	35.5	34.8	34.2	33.5	32.9	32.3	31.7	31.2	30.7	30.1	29.7	29.2	28.7	28.3	27.8	27.4	27.0	26.6
	8.8	40.0	39.1	38.3	37.6	36.8	36.1	35.4	34.8	34.1	33.5	32.9	32.4	31.8	31.3	30.8	30.3	29.8	29.3	28.9	28.4	28.0	27.6	27.2
	9.0	40.5	39.7	38.9	38.1	37.4	36.7	36.0	35.4	34.7	34.1	33.5	33.0	32.4	31.9	31.4	30.9	30.4	29.9	29.5	29.0	28.6	28.2	27.8
	9.2	41.1	40.3	39.5	38.7	38.0	37.3	36.6	36.0	35.3	34.7	34.1	33.6	33.0	32.5	32.0	31.5	31.0	30.5	30.1	29.6	29.2	28.8	28.4
	9.4	41.7	40.9	40.1	39.3	38.6	37.9	37.2	36.6	35.9	35.3	34.7	34.2	33.6	33.1	32.6	32.1	31.6	31.1	30.7	30.2	29.8	29.4	29.0
	9.6	42.3	41.4	40.7	39.9	39.2	38.5	37.8	37.2	36.5	35.9	35.3	34.8	34.2	33.7	33.2	32.7	32.2	31.7	31.3	30.8	30.4	30.0	29.5
	9.8	42.8	42.0	41.2	40.5	39.8	39.1	38.4	37.8	37.1	36.5	35.9	35.4	34.8	34.3	33.8	33.3	32.8	32.3	31.9	31.4	31.0	30.5	30.1
	10.0	43.4	42.6	41.8	41.1	40.4	39.7	39.0	38.4	37.7	37.1	36.5	36.0	35.4	34.9	34.4	33.9	33.4	32.9	32.4	32.0	31.6	31.1	30.7
	10.5	44.8	44.0	43.3	42.5	41.8	41.1	40.5	39.8	39.2	38.6	38.0	37.5	36.9	36.4	35.9	35.4	34.9	34.4	33.9	33.5	33.0	32.6	32.2
	11.0	46.2	45.4	44.7	44.0	43.3	42.6	41.9	41.3	40.7	40.1	39.5	39.0	38.4	37.9	37.4	36.8	36.4	35.9	35.4	35.0	34.5	34.1	33.7
	11.5	47.6	46.8	46.1	45.4	44.7	44.0	43.4	42.8	42.2	41.6	41.0	40.4	39.9	39.3	38.8	38.3	37.8	37.4	36.9	36.4	36.0	35.6	35.1
	12.0	49.0	48.2	47.5	46.8	46.1	45.5	44.8	44.2	43.6	43.0	42.5	41.9	41.3	40.8	40.3	39.8	39.3	38.8	38.4	37.9	37.5	37.0	36.6
	12.5	50.3	49.6	48.9	48.2	47.6	46.9	46.3	45.7	45.1	44.5	43.9	43.4	42.8	42.3	41.8	41.3	40.8	40.3	39.8	39.4	38.9	38.5	38.1
	13.0	51.7	51.0	50.3	49.6	49.0	48.3	47.7	47.1	46.5	45.9	45.4	44.8	44.3	43.7	43.2	42.7	42.2	41.8	41.3	40.8	40.4	40.0	39.5
	13.5	53.1	52.4	51.7	51.0	50.4	49.7	49.1	48.5	47.9	47.3	46.8	46.2	45.7	45.2	44.7	44.2	43.7	43.2	42.8	42.3	41.8	41.4	41.0
	14.0	54.4	53.7	53.0	52.4	51.7	51.1	50.5	49.9	49.3	48.8	48.2	47.7	47.2	46.6	46.1</								



**Table J-4C: Basic Energy Use (BEU) - Storage Heat Pump Heater [no interpolation]**

Adjusted Recover	Energy Factor																					
	Load	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8
6.0	14.1	13.5	13.0	12.6	12.1	11.7	11.3	11.0	10.6	10.3	10.0	9.7	9.5	9.2	9.0	8.7	8.5	8.3	8.1	7.9	7.8	
6.2	14.4	13.8	13.3	12.8	12.3	11.9	11.5	11.1	10.8	10.5	10.2	9.9	9.6	9.3	9.1	8.9	8.7	8.4	8.2	8.0	7.9	
6.4	14.7	14.1	13.5	13.0	12.5	12.1	11.7	11.3	11.0	10.6	10.3	10.0	9.7	9.5	9.2	9.0	8.8	8.6	8.3	8.2	8.0	
6.6	14.9	14.3	13.8	13.2	12.8	12.3	11.9	11.5	11.1	10.8	10.5	10.2	9.9	9.6	9.4	9.1	8.9	8.7	8.5	8.3	8.1	
6.8	15.2	14.6	14.0	13.5	13.0	12.5	12.1	11.7	11.3	11.0	10.6	10.3	10.0	9.8	9.5	9.3	9.0	8.8	8.6	8.4	8.2	
7.0	15.5	14.8	14.2	13.7	13.2	12.7	12.3	11.9	11.5	11.1	10.8	10.5	10.2	9.9	9.6	9.4	9.1	8.9	8.7	8.5	8.3	
7.2	15.8	15.1	14.5	13.9	13.4	12.9	12.5	12.1	11.7	11.3	11.0	10.6	10.3	10.0	9.8	9.5	9.3	9.0	8.8	8.6	8.4	
7.4	16.0	15.4	14.7	14.2	13.6	13.1	12.7	12.2	11.8	11.5	11.1	10.8	10.5	10.2	9.9	9.6	9.4	9.1	8.9	8.7	8.5	
7.6	16.3	15.6	15.0	14.4	13.8	13.3	12.9	12.4	12.0	11.6	11.3	10.9	10.6	10.3	10.0	9.8	9.5	9.3	9.0	8.8	8.6	
7.8	16.6	15.9	15.2	14.6	14.0	13.5	13.0	12.6	12.2	11.8	11.4	11.1	10.8	10.5	10.2	9.9	9.6	9.4	9.2	8.9	8.7	
8.0	16.8	16.1	15.4	14.8	14.3	13.7	13.2	12.8	12.4	12.0	11.6	11.2	10.9	10.6	10.3	10.0	9.8	9.5	9.3	9.0	8.8	
8.2	17.1	16.4	15.7	15.0	14.5	13.9	13.4	13.0	12.5	12.1	11.7	11.4	11.0	10.7	10.4	10.1	9.9	9.6	9.4	9.2	8.9	
8.4	17.4	16.6	15.9	15.3	14.7	14.1	13.6	13.1	12.7	12.3	11.9	11.5	11.2	10.9	10.6	10.3	10.0	9.7	9.5	9.3	9.0	
8.6	17.7	16.9	16.1	15.5	14.9	14.3	13.8	13.3	12.9	12.4	12.0	11.7	11.3	11.0	10.7	10.4	10.1	9.9	9.6	9.4	9.1	
8.8	17.9	17.1	16.4	15.7	15.1	14.5	14.0	13.5	13.0	12.6	12.2	11.8	11.5	11.1	10.8	10.5	10.2	10.0	9.7	9.5	9.3	
9.0	18.2	17.4	16.6	15.9	15.3	14.7	14.2	13.7	13.2	12.8	12.4	12.0	11.6	11.3	11.0	10.7	10.4	10.1	9.8	9.6	9.4	
9.2	18.4	17.6	16.8	16.1	15.5	14.9	14.4	13.9	13.4	12.9	12.5	12.1	11.8	11.4	11.1	10.8	10.5	10.2	10.0	9.7	9.5	
9.4	18.7	17.9	17.1	16.4	15.7	15.1	14.5	14.0	13.5	13.1	12.7	12.3	11.9	11.5	11.3	10.9	10.6	10.3	10.1	9.8	9.6	
9.6	19.0	18.1	17.3	16.6	15.9	15.3	14.7	14.2	13.7	13.3	12.8	12.4	12.0	11.7	11.4	11.0	10.7	10.5	10.2	9.9	9.7	
9.8	19.2	18.3	17.5	16.8	16.1	15.5	14.9	14.4	13.9	13.4	13.0	12.6	12.2	11.8	11.5	11.2	10.9	10.6	10.3	10.0	9.8	
10.0	19.5	18.6	17.8	17.0	16.3	15.7	15.1	14.6	14.0	13.6	13.1	12.7	12.3	12.0	11.7	11.3	11.0	10.7	10.4	10.1	9.9	
10.5	20.1	19.2	18.3	17.6	16.8	16.2	15.6	15.0	14.5	14.0	13.5	13.1	12.7	12.3	11.9	11.6	11.3	11.0	10.7	10.4	10.2	
11.0	20.8	19.8	18.9	18.1	17.3	16.7	16.0	15.4	14.9	14.4	13.9	13.4	13.0	12.6	12.3	11.9	11.6	11.3	11.0	10.7	10.4	
11.5	21.4	20.4	19.5	18.6	17.8	17.1	16.5	15.9	15.3	14.8	14.3	13.8	13.4	13.0	12.6	12.2	11.9	11.6	11.3	11.0	10.7	
12.0	22.1	21.0	20.0	19.1	18.3	17.6	16.9	16.3	15.7	15.1	14.6	14.2	13.7	13.3	12.9	12.5	12.2	11.9	11.5	11.2	11.0	
12.5	22.7	21.6	20.6	19.7	18.8	18.1	17.4	16.7	16.1	15.5	15.0	14.5	14.1	13.6	13.2	12.8	12.5	12.1	11.8	11.5	11.2	
13.0	23.3	22.2	21.1	20.2	19.3	18.5	17.8	17.1	16.5	15.9	15.4	14.9	14.4	14.0	13.5	13.1	12.8	12.4	12.1	11.8	11.5	
13.5	23.9	22.7	21.7	20.7	19.8	19.0	18.2	17.6	16.9	16.3	15.8	15.2	14.7	14.3	13.9	13.5	13.1	12.7	12.4	12.0	11.7	
14.0	24.5	23.3	22.2	21.2	20.3	19.5	18.7	18.0	17.3	16.7	16.1	15.6	15.1	14.6	14.2	13.8	13.4	13.0	12.6	12.3	12.0	
14.5	25.2	23.9	22.8	21.7	20.8	19.9	19.1	18.4	17.7	17.1	16.5	15.9	15.4	14.9	14.5	14.1	13.7	13.3	12.9	12.6	12.3	
15.0	25.8	24.5	23.3	22.2	21.3	20.4	19.6	18.8	18.1	17.4	16.8	16.3	15.8	15.3	14.8	14.4	13.9	13.6	13.2	12.8	12.5	
15.5	26.4	25.0	23.8	22.7	21.7	20.8	20.0	19.2	18.5	17.8	17.2	16.6	16.1	15.6	15.1	14.7	14.2	13.8	13.5	13.1	12.8	
16.0	27.0	25.6	24.4	23.2	22.2	21.3	20.4	19.6	18.9	18.2	17.6	17.0	16.4	15.9	15.4	15.0	14.5	14.1	13.7	13.4	13.0	
16.5	27.6	26.2	24.9	23.7	22.7	21.7	20.8	20.0	19.3	18.6	17.9	17.3	16.7	16.2	15.7	15.2	14.8	14.4	14.0	13.6	13.3	
17.0	28.2	26.7	25.4	24.2	23.2	22.2	21.3	20.4	19.7	18.9	18.3	17.7	17.1	16.5	16.0	15.5	15.1	14.7	14.3	13.9	13.5	
17.5	28.8	27.3	25.9	24.7	23.6	22.6	21.7	20.8	20.0	19.3	18.6	18.0	17.4	16.8	16.3	15.8	15.4	14.9	14.5	14.1	13.8	
18.0	29.4	27.8	26.5	25.2	24.1	23.1	22.1	21.2	20.4	19.7	19.0	18.3	17.7	17.2	16.6	16.1	15.7	15.2	14.8	14.4	14.0	
18.5	29.9	28.4	27.0	25.7	24.5	23.5	22.5	21.6	20.8	20.0	19.3	18.7	18.0	17.5	16.9	16.4	15.9	15.5	15.1	14.7	14.3	
19.0	30.5	28.9	27.5	26.2	25.0	23.9	23.3	22.0	21.2	20.4	19.7	19.0	18.4	17.8	17.2	16.7	16.2	15.8	15.3	14.9	14.5	
19.5	31.1	29.5	28.0	26.7	25.5	24.4	23.3	22.4	21.6	20.8	20.0	19.3	18.7	18.1	17.5	17.0	16.5	16.0	15.6	15.2	14.8	
20.0	31.7	30.0	28.5	27.2	25.9	24.8	23.8	22.8	21.9	21.1	20.4	19.7	19.0	18.4	17.8	17.3	16.8	16.3	15.8	15.4	15.0	
21.0	32.8	31.1	29.5	28.1	26.8	25.7	24.6	23.6	22.7	21.8	21.1	20.3	19.6	19.0	18.4	17.8	17.3	16.8	16.4	15.9	15.5	
22.0	34.0	32.2	30.5	29.1	27.7	26.5	25.4	24.4	23.4	22.5	21.7	21.0	20.3	19.6	19.0	18.4	17.9	17.4	16.9	16.4	16.0	

Climate Zone	Factor
1, 14	1.04
2, 3	0.99
4, 5, 12	1.07
6-11, 13, 15	0.92
16	1.50

Basic Energy Use x CZ Factor. = BEU to Line 2a,  
DHW-1

Instructions: Multiply Basic Energy Use by appropriate Climate  
Zone Factor from table. **Do not interpolate.**



# APPENDIX H



## **Appendix H**

### **Glossary of Terms**

**Approved**, as to a home energy rating provider and home energy rating system, means a provider and home energy rating system reviewed and certified by the Commission under the California Code of Regulations, Title 20, Section 1674.

**Certified**, as to a home energy rater, means having been found by a certified home energy rating provider to have successfully completed the requirements established by that home energy rating provider and registered by that provider in accordance with the California Code of Regulations, Title 20, Sections 1673(a), 1673(b), and 1673(c).

**Home Energy Rater** means a person certified by a certified home energy rating provider and listed on the provider's registry of certified raters to perform the site inspection and data collection, diagnostic testing, and data entry and analysis required to produce a home energy rating.

**Home Energy Rating** means a representation on a 0 to 100 scale of the annual source energy efficiency of a home.

**Home Energy Rating Provider** means a person or entity which administers an approved home energy rating system.

**Home Energy Rating System** means a fixed set of procedures, utilizing specifically defined assumptions, measurements and calculations, which produces a home energy rating.

**Low-Rise Residential Building** means a building, other than a hotel/motel as defined in Title 24, Part 6, Section 101(b), of the California Code of Regulations, that is of occupancy group R-1 and is three stories or less, or that is of occupancy group R-3, as those occupancy groups are defined in Title 24, Part 2, Section 1201, of the California Code of Regulations







# APPENDIX I







## Appendix I: Interior Mass Capacity

The *Interior Mass Capacity (IMC)* of a material is calculated by multiplying its *Area* times its *Unit Interior Mass Capacity (UIMC)* using Equation I-1. Tables 3-2a, 3-2b and 3-3 list the UIMCs for a number of thermal mass materials. This method allows for multiple mass types in both raised-floor and slab-on-grade construction.

The *Interior Mass Capacity* for the *Standard Design* shall be determined as 20 percent of the *Proposed Design's* conditioned slab floor as 3.5 inch thick exposed slab (UIMC=4.6), 80% of the conditioned slab as 3.5 inch thick rug-covered slab (UIMC=1.8), and 5% of the *Proposed Design's* conditioned nonslab floor area as exposed 2 inch thick concrete (UIMC=2.5). If the user does not specify a high mass design, the *Interior Mass Capacity* of the *Proposed Design* shall be the same as for the *Standard Design*. If the user specifies a high mass design with an *Interior Mass Capacity* greater than the high mass threshold, the user is allowed to model the mass specified in the *Proposed Design*. The high mass threshold *Interior Mass Capacity* is determined as 30% of the conditioned floor area as exposed slab (UIMC=4.6), 70% of the conditioned slab floor area as rug-covered slab (UIMC=1.8), and 15% of the conditioned nonslab floor area as 2 inch thick concrete (UIMC=2.5).

### EQUATION NO. I-1 CALCULATION OF INTERIOR MASS CAPACITY

$$IMC = [(A_1 \times UIMC_1) + (A_2 \times UIMC_2) \dots + (A_n \times UIMC_n)]$$

Where,

$A_n$  = Area of mass material  $n$ , and

$UIMC_n$  = Unit Interior Mass Capacity of mass material  $n$

Based on the UIMCs given above:

$$IMC_{threshold} = 2.64 \times CSA + 0.375 \times (CFA - CSA)$$

Where:

$CSA$  = Conditioned Slab floor Area

$CFA$  = total Conditioned Floor Area



Table 3-2a: Interior Mass UIMC Values:

Interior Mass<sup>11</sup> - Surfaces Exposed on One Side<sup>13</sup>

Material	Surface Condition	Mass Thickness (inches)	Unit Interior Mass Capacity
Concrete Slab-on-Grade and Raised Concrete Floors	Exposed <sup>1</sup>	2.00	3.6
		3.50	4.6
	Covered <sup>2</sup>	6.00	5.1
		2.00	1.6
		3.50	1.8
		6.00	1.9
Lightweight Concrete	Exposed	0.75	1.0
		1.00	1.4
		1.50	2.0
		2.00	2.5
	Covered	0.75	0.9
		1.00	1.0
		1.50	1.2
		2.00	1.4
Solid Wood <sup>9</sup>	Exposed	1.50	1.2
		3.00	1.6
Tile <sup>3,9</sup>	Exposed	0.50	0.8
		1.00	1.7
		1.50	2.4
		2.00	3.0
Masonry <sup>4,9</sup>	Exposed	1.00	2.0
		2.00	2.7
		4.00	4.2
Adobe <sup>9</sup>	Exposed	4.00	3.8
		6.00	3.9
		8.00	3.9
Framed Wall	0.50" Gypsum	na	0.0
	0.63" Gypsum	na	0.1
	1.00" Gypsum	na	0.5
	0.88" Stucco	na	1.1
Masonry Infill <sup>7</sup>	0.50" Gypsum	3.50	1.3



Table 3-2 continued on next page.  
**Table 3-2b: Interior Mass UIMC Values:**

**Interior Mass<sup>11</sup> - Surfaces Exposed on Two Sides<sup>5, 13</sup>**

<b>Material</b>	<b>Surface Condition</b>	<b>Mass Thickness (inches)</b>	<b>Unit Interior Mass Capacity</b>
Partial Grout Masonry <sup>4</sup>	Exposed <sup>1</sup>	4.00	6.9
		6.00	7.4
		8.00	7.4
Solid Grout Masonry <sup>4,6</sup>	Exposed	4.00	8.3
		6.00	9.2
		8.00	9.6
Adobe	Exposed	4.00	7.6
		12.00	7.8
		16.00	7.6
Solid Wood/ Logs	Exposed	3.00	3.3
		4.00	3.3
		6.00	3.3
		8.00	3.3
Framed Wall	0.50" Gypsum	na	0.0
	0.63" Gypsum	na	0.2
	1.00" Gypsum	na	0.9
	0.88" Stucco	na	2.1
Masonry Infill <sup>7</sup>	0.50" Gypsum	3.50	2.6

Notes follow Table 3-3.



Table 3-3: Exterior Wall Mass UIMC Values and Exterior Mass Factors<sup>13</sup>

Material	Surface Condition	Mass Thickness (inches)	Wall U-value	Unit Interior Mass Capacity	Exterior <sup>8</sup> Mass Factor
Partial Grout Masonry <sup>4</sup>	Exposed <sup>1</sup>	4.00	0.68	0.9	1.1
			0.58	1.0	1.0
		6.00	0.54	1.3	1.3
			0.44	1.5	1.1
		8.00	0.49	1.5	1.3
			0.38	1.7	1.2
	Furred <sup>10</sup>	4.00	0.40	0.5	0.9
			0.30	0.5	0.7
			0.20	0.5	0.5
			0.10	0.5	0.3
			0.08	0.5	0.2
		6.00	0.40	0.9	1.2
			0.30	0.6	1.0
			0.20	0.5	0.7
			0.10	0.5	0.4
			0.08	0.5	0.3
		8.00	0.30	0.8	1.0
			0.20	0.5	0.7
			0.10	0.5	0.4
			0.08	0.5	0.3
Solid Grout Masonry <sup>4,6</sup>	Exposed	4.00	0.79	1.0	1.4
		6.00	0.68	1.5	1.9
		8.00	0.62	1.8	2.1
	Furred <sup>10</sup>	4.00	0.40	0.5	1.0
			0.30	0.5	0.8
			0.20	0.5	0.6
			0.10	0.5	0.3
			0.08	0.5	0.3
		6.00	0.40	0.7	1.4
			0.30	0.5	1.1
			0.20	0.5	0.7
			0.10	0.5	0.4
			0.08	0.5	0.3
		8.00	0.40	0.8	1.5
			0.30	0.6	1.2
			0.20	0.5	0.8
			0.10	0.5	0.4
			0.08	0.5	0.3

Table 3-3 continued on next page



**Table 3-3: Exterior Wall Mass UIMC Values and Exterior Mass Factors<sup>13</sup>**

Material	Surface Condition	Mass Thickness (inches)	Wall U-value	Unit Interior Mass Capacity	Exterior <sup>9</sup> Mass Factor
Solid Wood/ Logs	Exposed <sup>1</sup>	3.00	0.22	0.7	0.5
		4.00	0.17	0.9	0.6
		6.00	0.12	1.1	0.6
		8.00	0.093	1.2	0.4
		10.00	0.075	1.3	0.3
		12.00	0.063	1.3	0.3
Wood Cavity Wall <sup>12</sup>	Exposed	3.00 <sup>12</sup>	0.11	1.1	0.5
			0.065	1.3	0.3
			0.045	1.4	0.2
Adobe	Exposed	8.00	0.35	2.1	1.5
		16.00	0.21	2.8	0.8
		24.00	0.15	3.1	0.5
Masonry Veneer <sup>4</sup>	Framed Wall	4.00	0.10	na	0.3
			0.08	na	0.3
			0.06	na	0.2
Adobe Veneer	Framed Wall	4.00	0.10	na	0.4
			0.08	na	0.3
			0.06	na	0.2

**Notes For Tables 3-2 and 3-3:**

1. "Exposed" means that the mass is directly exposed to room air or covered with a conductive material such as ceramic tile.
2. "Covered" includes carpet, cabinets, closets or walls.
3. The indicated thickness includes both the tile and the mortar bed, when applicable.
4. Masonry includes brick, stone, concrete masonry units, hollow clay tile and other masonry.
5. The unit interior mass capacity for surfaces exposed on two sides is based on the area of one side only.
6. "Solid Grout Masonry" means that all the cells of the masonry units are filled with grout.
7. The indicated thickness for masonry infill is for the masonry material itself.
8. Use the Exterior Mass value for calculating Exterior Wall Mass.
9. Mass located inside exterior walls or ceilings may be considered interior mass (exposed one side) when it is insulated on the exterior with at least R-11 insulation, or a total resistance of R-9 including framing effects.
10. "Furred" means that 0.50-inch gypsum board is placed on the inside of the mass wall separated from the mass with insulation or an air space.
11. When mass types are layered, e.g. tile over slab-on-grade or lightweight concrete floor, only the mass type with the greatest interior mass capacity may be accounted for, based on the total thickness of both layers.
12. This wall consists of 3 inches of wood on each side of a cavity. The cavity may be insulated as indicated by the U-value column.
13. Values based on properties of materials listed in 1993 *ASHRAE Handbook of Fundamentals*.







# APPENDIX J







CASE CODE	Input Assumptions for Duct System							
	Supply duct	Return duct	Total duct	ACCA	Radiant	Supply duct	Return duct	Duct Surface
	Location	Location	Leakage,%	Design	Barrier	R Value	R value	Area Reduction
1001	attic	attic	22	no	no	4.2	4.2	0
1002	attic	attic	22	no	no	8	4.2	0
1003	attic	attic	22	no	no	4.2	8	0
1004	attic	attic	8	no	no	4.2	4.2	0
1005	attic	attic	8	no	no	8	4.2	0
1006	attic	attic	8	no	no	4.2	8	0
1007	attic	attic	8	yes	no	4.2	4.2	0
1008	attic	attic	8	yes	yes	4.2	4.2	0
1009	attic	attic	8	yes	yes	8	8	0
1010	attic	attic	22	no	yes	4.2	4.2	0
1011	attic	attic	22	no	no	8	8	0
1012	attic	attic	22	yes	no	4.2	4.2	0
1013	attic	attic	8	no	no	8	8	0
1014	attic	attic	8	no	no	8	4.2	0
1015	attic	attic	8	no	no	4.2	8	0
1016	attic	attic	8	yes	yes	4.2	4.2	0
1017	attic	attic	8	yes	no	4.2	4.2	50%
1018	attic	attic	8	yes	no	4.2	4.2	25%
1019	attic	attic	8	no	no	4.2	4.2	50%
1020	attic	attic	22	no	no	4.2	4.2	50%
1021	attic	attic	8	no	no	4.2	4.2	25%
1022	attic	attic	22	no	no	4.2	4.2	25%
1023	attic	crawlspace	22	no	no	4.2	4.2	0
1024	attic	crawlspace	22	no	no	8	4.2	0
1025	attic	crawlspace	22	no	no	4.2	8	0
1026	attic	crawlspace	8	no	no	4.2	4.2	0
1027	attic	crawlspace	8	no	no	8	4.2	0
1028	attic	crawlspace	8	no	no	4.2	8	0
1029	attic	crawlspace	8	yes	no	4.2	4.2	0
1030	attic	crawlspace	8	yes	yes	4.2	4.2	0
1031	attic	crawlspace	8	yes	yes	8	8	0
1032	attic	crawlspace	22	no	yes	4.2	4.2	0
1033	attic	crawlspace	22	no	no	8	8	0
1034	attic	crawlspace	22	yes	no	4.2	4.2	0
1035	attic	crawlspace	8	no	no	8	8	0
1036	attic	crawlspace	8	no	no	8	4.2	0



CASE CODE	Input Assumptions for Duct System							
	Supply duct	Return duct	Total duct	ACCA	Radiant	Supply duct	Return duct	Duct Surface
	Location	Location	Leakage,%	Design	Barrier	R Value	R value	Area Reduction
1037	attic	crawlspace	8	no	no	4.2	8	0
1038	attic	crawlspace	8	yes	yes	4.2	4.2	0
1039	attic	crawlspace	8	yes	no	4.2	4.2	50%
1040	attic	crawlspace	8	yes	no	4.2	4.2	25%
1041	attic	crawlspace	8	no	no	4.2	4.2	50%
1042	attic	crawlspace	22	no	no	4.2	4.2	50%
1043	attic	crawlspace	8	no	no	4.2	4.2	25%
1044	attic	crawlspace	22	no	no	4.2	4.2	25%
1045	conditioned space	attic	22	no	no	4.2	4.2	0
1046	conditioned space	attic	8	no	no	4.2	4.2	0
1047	conditioned space	attic	8	yes	no	4.2	4.2	0
1048	conditioned space	attic	8	yes	no	8	8	0
1049	conditioned space	attic	8	yes	yes	8	8	0
1050	conditioned space	attic	22	no	yes	8	8	0
1051	conditioned space	attic	22	yes	yes	8	8	0
1052	conditioned space	attic	22	no	no	8	8	0
1053	conditioned space	attic	22	yes	no	4.2	4.2	0
1054	crawlspace	crawlspace	22	no	no	4.2	4.2	0
1055	crawlspace	crawlspace	8	no	no	4.2	4.2	0
1056	crawlspace	crawlspace	8	yes	no	4.2	4.2	0
1057	crawlspace	crawlspace	8	yes	no	4.2	8	0
1058	crawlspace	crawlspace	8	yes	no	8	4.2	0
1059	crawlspace	crawlspace	8	yes	no	8	8	0
1060	crawlspace	crawlspace	22	yes	no	4.2	4.2	0
1061	crawlspace	crawlspace	22	no	no	8	8	0
1062	crawlspace	crawlspace	22	no	no	4.2	8	0
1063	crawlspace	crawlspace	22	no	no	8	4.2	0
1064	crawlspace	crawlspace	22	no	no	4.2	4.2	50%
1065	crawlspace	crawlspace	22	no	no	4.2	4.2	25%
1066	crawlspace	crawlspace	22	yes	no	4.2	4.2	50%
1067	crawlspace	crawlspace	8	no	no	4.2	4.2	50%
1068	crawlspace	crawlspace	8	no	no	8	8	50%
1069	crawlspace	crawlspace	8	no	no	8	8	25%
1070	crawlspace	attic	22	no	no	4.2	4.2	0
1071	crawlspace	attic	8	no	no	4.2	4.2	0
1072	crawlspace	attic	8	yes	no	4.2	4.2	0



CASE CODE	Input Assumptions for Duct System							
	Supply duct	Return duct	Total duct	ACCA	Radiant	Supply duct	Return duct	Duct Surface
	Location	Location	Leakage,%	Design	Barrier	R Value	R value	Area Reduction
1073	crawlspace	attic	8	yes	no	4.2	8	0
1074	crawlspace	attic	8	yes	no	8	4.2	0
1075	crawlspace	attic	8	yes	no	8	8	0
1076	crawlspace	attic	22	yes	no	4.2	4.2	0
1077	crawlspace	attic	22	no	no	8	8	0
1078	crawlspace	attic	22	no	no	8	4.2	0
1079	crawlspace	attic	22	no	no	4.2	8	0
1080	crawlspace	attic	22	no	no	4.2	4.2	50%
1081	crawlspace	attic	22	no	no	4.2	4.2	25%
1082	crawlspace	attic	22	yes	no	4.2	4.2	50%
1083	crawlspace	attic	8	no	no	4.2	4.2	50%
1084	crawlspace	attic	8	no	no	8	8	50%
1085	crawlspace	attic	8	no	no	8	8	25%
1086	conditioned space	crawlspace	22	no	no	4.2	4.2	0
1087	conditioned space	crawlspace	8	no	no	4.2	4.2	0
1088	conditioned space	crawlspace	8	no	no	8	8	0
1089	conditioned space	crawlspace	8	yes	no	4.2	4.2	0
1090	conditioned space	crawlspace	8	yes	no	8	8	0
1091	conditioned space	crawlspace	22	yes	no	4.2	4.2	0
1092	conditioned space	crawlspace	22	yes	no	8	8	0
1093	conditioned space	crawlspace	22	no	no	8	8	0
1094	basement	basement	22	no	no	4.2	4.2	0
1095	basement	basement	22	no	no	8	8	0
1096	basement	basement	8	no	no	4.2	4.2	0
1097	basement	basement	8	yes	no	4.2	4.2	0
1098	basement	basement	8	yes	no	8	8	0
1099	basement	basement	22	yes	no	4.2	4.2	0
1100	basement	basement	22	no	no	4.2	4.2	50%
1101	basement	basement	8	no	no	4.2	4.2	50%
1102	conditioned space	basement	22	no	no	4.2	4.2	0
1103	conditioned space	basement	8	no	no	4.2	4.2	0
1104	conditioned space	basement	8	yes	no	4.2	4.2	0
1105	conditioned space	basement	8	yes	no	8	8	0
1106	conditioned space	basement	8	no	no	8	8	0
1107	conditioned space	basement	22	yes	no	8	8	0
1108	conditioned space	basement	22	yes	no	4.2	4.2	0



CASE CODE	Climate Zone 1				Climate Zone 2			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.756	0.810	0.785	0.812	0.743	0.674	0.773	0.702
1002	0.796	0.813	0.812	0.814	0.786	0.715	0.801	0.729
1003	0.758	0.810	0.788	0.812	0.745	0.676	0.777	0.706
1004	0.825	0.866	0.856	0.869	0.815	0.744	0.848	0.775
1005	0.869	0.869	0.886	0.871	0.862	0.790	0.879	0.805
1006	0.827	0.866	0.860	0.869	0.818	0.746	0.852	0.780
1007	0.825	0.937	0.856	0.939	0.815	0.804	0.848	0.837
1008	0.825	0.914	0.856	0.925	0.815	0.822	0.848	0.854
1009	0.871	0.927	0.889	0.933	0.864	0.869	0.883	0.888
1010	0.756	0.791	0.785	0.800	0.743	0.696	0.773	0.723
1011	0.798	0.813	0.815	0.814	0.788	0.717	0.805	0.734
1012	0.756	0.875	0.785	0.878	0.743	0.728	0.773	0.759
1013	0.871	0.869	0.889	0.871	0.864	0.792	0.883	0.810
1014	0.869	0.869	0.886	0.871	0.862	0.790	0.879	0.805
1015	0.827	0.866	0.860	0.869	0.818	0.746	0.852	0.780
1016	0.825	0.914	0.856	0.925	0.815	0.822	0.848	0.854
1017	0.876	0.941	0.890	0.942	0.869	0.861	0.883	0.875
1018	0.850	0.938	0.873	0.941	0.842	0.832	0.865	0.856
1019	0.876	0.870	0.890	0.871	0.869	0.797	0.883	0.810
1020	0.802	0.813	0.816	0.814	0.792	0.721	0.805	0.733
1021	0.850	0.868	0.873	0.870	0.842	0.770	0.865	0.792
1022	0.779	0.811	0.800	0.813	0.767	0.697	0.789	0.718
1023	0.758	0.811	0.785	0.812	0.746	0.717	0.773	0.702
1024	0.798	0.814	0.812	0.814	0.788	0.760	0.801	0.729
1025	0.760	0.811	0.788	0.812	0.748	0.717	0.777	0.706
1026	0.826	0.867	0.856	0.869	0.817	0.765	0.848	0.775
1027	0.870	0.870	0.886	0.871	0.864	0.812	0.879	0.805
1028	0.828	0.867	0.860	0.869	0.820	0.765	0.852	0.780
1029	0.826	0.937	0.856	0.939	0.817	0.827	0.848	0.837
1030	0.826	0.915	0.856	0.925	0.817	0.838	0.848	0.854
1031	0.872	0.928	0.889	0.933	0.866	0.884	0.883	0.888
1032	0.758	0.792	0.785	0.800	0.746	0.726	0.773	0.723
1033	0.800	0.814	0.815	0.814	0.790	0.760	0.805	0.734
1034	0.758	0.877	0.785	0.878	0.746	0.775	0.773	0.759
1035	0.872	0.870	0.889	0.871	0.866	0.812	0.883	0.810
1036	0.870	0.870	0.886	0.871	0.864	0.812	0.879	0.805



CASE CODE	Climate Zone 1				Climate Zone 2			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.828	0.867	0.860	0.869	0.820	0.765	0.852	0.780
1038	0.826	0.915	0.856	0.925	0.817	0.838	0.848	0.854
1039	0.877	0.941	0.890	0.942	0.871	0.885	0.883	0.875
1040	0.851	0.939	0.873	0.941	0.844	0.856	0.865	0.856
1041	0.877	0.870	0.890	0.871	0.871	0.818	0.883	0.810
1042	0.804	0.814	0.816	0.814	0.795	0.766	0.805	0.733
1043	0.851	0.869	0.873	0.870	0.844	0.791	0.865	0.792
1044	0.781	0.812	0.800	0.813	0.770	0.741	0.789	0.718
1045	0.902	0.862	0.900	0.862	0.895	0.819	0.893	0.817
1046	0.949	0.890	0.947	0.890	0.946	0.872	0.943	0.869
1047	0.949	0.962	0.947	0.962	0.946	0.942	0.943	0.939
1048	0.950	0.962	0.949	0.962	0.947	0.944	0.946	0.942
1049	0.950	0.962	0.949	0.962	0.947	0.950	0.946	0.948
1050	0.903	0.862	0.902	0.862	0.895	0.833	0.894	0.833
1051	0.903	0.931	0.902	0.931	0.895	0.901	0.894	0.900
1052	0.903	0.862	0.902	0.862	0.895	0.820	0.894	0.819
1053	0.902	0.931	0.900	0.931	0.895	0.886	0.893	0.883
1054	0.761	0.833	0.787	0.813	0.749	0.750	0.775	0.704
1055	0.828	0.889	0.857	0.869	0.820	0.800	0.849	0.776
1056	0.828	0.962	0.857	0.940	0.820	0.865	0.849	0.839
1057	0.830	0.962	0.861	0.940	0.822	0.865	0.854	0.844
1058	0.871	0.955	0.887	0.942	0.865	0.899	0.880	0.871
1059	0.873	0.955	0.890	0.942	0.867	0.899	0.884	0.877
1060	0.761	0.900	0.787	0.879	0.749	0.811	0.775	0.761
1061	0.801	0.827	0.816	0.815	0.792	0.779	0.807	0.735
1062	0.762	0.833	0.790	0.813	0.751	0.750	0.779	0.708
1063	0.800	0.827	0.813	0.815	0.791	0.779	0.803	0.731
1064	0.806	0.826	0.817	0.815	0.797	0.783	0.807	0.735
1065	0.783	0.829	0.802	0.814	0.773	0.766	0.791	0.719
1066	0.806	0.893	0.817	0.882	0.797	0.847	0.807	0.795
1067	0.878	0.882	0.891	0.872	0.872	0.836	0.884	0.810
1068	0.902	0.879	0.910	0.873	0.898	0.853	0.905	0.831
1069	0.888	0.881	0.900	0.872	0.882	0.842	0.894	0.821
1070	0.758	0.832	0.787	0.813	0.746	0.707	0.775	0.704
1071	0.826	0.889	0.857	0.869	0.818	0.779	0.849	0.776
1072	0.826	0.961	0.857	0.940	0.818	0.843	0.849	0.839



CASE CODE	Climate Zone 1				Climate Zone 2			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.828	0.961	0.861	0.940	0.820	0.845	0.854	0.844
1074	0.870	0.954	0.887	0.942	0.864	0.876	0.880	0.871
1075	0.872	0.954	0.890	0.942	0.866	0.879	0.884	0.877
1076	0.758	0.899	0.787	0.879	0.746	0.765	0.775	0.761
1077	0.800	0.826	0.816	0.815	0.790	0.737	0.807	0.735
1078	0.798	0.826	0.813	0.815	0.788	0.735	0.803	0.731
1079	0.760	0.832	0.790	0.813	0.748	0.709	0.779	0.708
1080	0.804	0.825	0.817	0.815	0.794	0.739	0.807	0.735
1081	0.781	0.828	0.802	0.814	0.770	0.723	0.791	0.719
1082	0.804	0.892	0.817	0.882	0.794	0.799	0.807	0.795
1083	0.877	0.882	0.891	0.872	0.870	0.815	0.884	0.810
1084	0.901	0.879	0.910	0.873	0.897	0.834	0.905	0.831
1085	0.887	0.881	0.900	0.872	0.881	0.823	0.894	0.821
1086	0.903	0.863	0.980	0.907	0.897	0.863	0.980	0.907
1087	0.950	0.891	0.980	0.907	0.947	0.891	0.980	0.907
1088	0.951	0.891	0.980	0.907	0.948	0.891	0.980	0.907
1089	0.950	0.963	0.980	0.980	0.947	0.963	0.980	0.980
1090	0.951	0.963	0.980	0.980	0.948	0.963	0.980	0.980
1091	0.903	0.933	0.980	0.980	0.897	0.933	0.980	0.980
1092	0.904	0.933	0.980	0.980	0.897	0.933	0.980	0.980
1093	0.904	0.863	0.980	0.907	0.897	0.863	0.980	0.907
1094	0.786	0.859	0.814	0.853	0.808	0.816	0.835	0.825
1095	0.821	0.849	0.839	0.846	0.839	0.824	0.856	0.830
1096	0.847	0.907	0.876	0.898	0.862	0.860	0.890	0.868
1097	0.847	0.981	0.876	0.971	0.862	0.930	0.890	0.939
1098	0.886	0.968	0.903	0.963	0.897	0.939	0.913	0.945
1099	0.786	0.929	0.814	0.922	0.808	0.882	0.835	0.892
1100	0.824	0.847	0.839	0.845	0.843	0.825	0.857	0.831
1101	0.889	0.894	0.903	0.890	0.901	0.870	0.914	0.875
1102	0.905	0.869	0.906	0.872	0.919	0.869	0.921	0.872
1103	0.950	0.893	0.949	0.894	0.956	0.893	0.956	0.894
1104	0.950	0.965	0.949	0.966	0.956	0.965	0.956	0.966
1105	0.951	0.965	0.951	0.966	0.957	0.965	0.957	0.966
1106	0.951	0.893	0.951	0.894	0.957	0.893	0.957	0.894
1107	0.905	0.940	0.907	0.942	0.919	0.940	0.921	0.942
1108	0.905	0.940	0.906	0.942	0.919	0.940	0.921	0.942



CASE CODE	Climate Zone 3				Climate Zone 4			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.766	0.730	0.794	0.755	0.759	0.738	0.788	0.763
1002	0.804	0.763	0.820	0.777	0.799	0.769	0.814	0.783
1003	0.767	0.731	0.796	0.756	0.761	0.738	0.791	0.763
1004	0.832	0.786	0.863	0.813	0.827	0.792	0.858	0.818
1005	0.874	0.821	0.891	0.836	0.871	0.826	0.887	0.841
1006	0.833	0.786	0.865	0.814	0.829	0.792	0.862	0.819
1007	0.832	0.850	0.863	0.879	0.827	0.856	0.858	0.885
1008	0.832	0.856	0.863	0.886	0.827	0.860	0.858	0.888
1009	0.876	0.894	0.894	0.911	0.873	0.896	0.891	0.913
1010	0.766	0.740	0.794	0.766	0.759	0.744	0.788	0.769
1011	0.806	0.763	0.822	0.778	0.801	0.770	0.817	0.784
1012	0.766	0.789	0.794	0.816	0.759	0.798	0.788	0.824
1013	0.876	0.822	0.894	0.837	0.873	0.826	0.891	0.841
1014	0.874	0.821	0.891	0.836	0.871	0.826	0.887	0.841
1015	0.833	0.786	0.865	0.814	0.829	0.792	0.862	0.819
1016	0.832	0.856	0.863	0.886	0.827	0.860	0.858	0.888
1017	0.881	0.893	0.895	0.908	0.877	0.898	0.892	0.912
1018	0.856	0.871	0.879	0.893	0.852	0.877	0.875	0.898
1019	0.881	0.826	0.895	0.840	0.877	0.831	0.892	0.844
1020	0.810	0.767	0.824	0.780	0.805	0.774	0.818	0.786
1021	0.856	0.806	0.879	0.826	0.852	0.811	0.875	0.831
1022	0.788	0.749	0.809	0.767	0.782	0.756	0.803	0.774
1023	0.767	0.741	0.794	0.755	0.761	0.745	0.788	0.763
1024	0.806	0.774	0.820	0.777	0.801	0.776	0.814	0.783
1025	0.768	0.741	0.796	0.756	0.763	0.745	0.791	0.763
1026	0.833	0.792	0.863	0.813	0.829	0.795	0.858	0.818
1027	0.875	0.827	0.891	0.836	0.872	0.829	0.887	0.841
1028	0.835	0.792	0.865	0.814	0.830	0.795	0.862	0.819
1029	0.833	0.856	0.863	0.879	0.829	0.860	0.858	0.885
1030	0.833	0.858	0.863	0.886	0.829	0.861	0.858	0.888
1031	0.877	0.895	0.894	0.911	0.874	0.897	0.891	0.913
1032	0.767	0.743	0.794	0.766	0.761	0.746	0.788	0.769
1033	0.807	0.774	0.822	0.778	0.802	0.776	0.817	0.784
1034	0.767	0.801	0.794	0.816	0.761	0.805	0.788	0.824
1035	0.877	0.827	0.894	0.837	0.874	0.829	0.891	0.841
1036	0.875	0.827	0.891	0.836	0.872	0.829	0.887	0.841



CASE CODE	Climate Zone 3				Climate Zone 4			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.835	0.792	0.865	0.814	0.830	0.795	0.862	0.819
1038	0.833	0.858	0.863	0.886	0.829	0.861	0.858	0.888
1039	0.882	0.899	0.895	0.908	0.878	0.901	0.892	0.912
1040	0.857	0.877	0.879	0.893	0.853	0.880	0.875	0.898
1041	0.882	0.832	0.895	0.840	0.878	0.834	0.892	0.844
1042	0.811	0.778	0.824	0.780	0.807	0.780	0.818	0.786
1043	0.857	0.811	0.879	0.826	0.853	0.814	0.875	0.831
1044	0.789	0.760	0.809	0.767	0.784	0.762	0.803	0.774
1045	0.908	0.852	0.906	0.852	0.904	0.857	0.902	0.857
1046	0.952	0.886	0.950	0.885	0.950	0.888	0.948	0.888
1047	0.952	0.958	0.950	0.957	0.950	0.960	0.948	0.960
1048	0.952	0.958	0.952	0.958	0.951	0.960	0.950	0.960
1049	0.952	0.962	0.952	0.962	0.951	0.962	0.950	0.962
1050	0.908	0.861	0.907	0.861	0.904	0.862	0.904	0.862
1051	0.908	0.930	0.907	0.930	0.904	0.931	0.904	0.931
1052	0.908	0.852	0.907	0.852	0.904	0.857	0.904	0.857
1053	0.908	0.921	0.906	0.921	0.904	0.926	0.902	0.926
1054	0.769	0.771	0.795	0.757	0.763	0.774	0.790	0.764
1055	0.834	0.823	0.863	0.814	0.830	0.827	0.859	0.819
1056	0.834	0.890	0.863	0.880	0.830	0.894	0.859	0.886
1057	0.836	0.890	0.866	0.881	0.832	0.894	0.863	0.886
1058	0.876	0.914	0.892	0.905	0.873	0.916	0.888	0.910
1059	0.878	0.914	0.895	0.906	0.875	0.916	0.892	0.910
1060	0.769	0.834	0.795	0.818	0.763	0.837	0.790	0.826
1061	0.808	0.791	0.824	0.779	0.804	0.793	0.819	0.785
1062	0.770	0.771	0.798	0.758	0.765	0.774	0.792	0.765
1063	0.807	0.791	0.821	0.778	0.802	0.793	0.816	0.785
1064	0.813	0.794	0.825	0.781	0.808	0.796	0.820	0.788
1065	0.791	0.783	0.810	0.769	0.785	0.785	0.805	0.776
1066	0.813	0.859	0.825	0.844	0.808	0.861	0.820	0.852
1067	0.882	0.848	0.896	0.840	0.879	0.850	0.893	0.845
1068	0.906	0.860	0.913	0.854	0.903	0.861	0.911	0.857
1069	0.891	0.852	0.904	0.846	0.889	0.854	0.901	0.849
1070	0.767	0.761	0.795	0.757	0.761	0.768	0.790	0.764
1071	0.833	0.818	0.863	0.814	0.829	0.824	0.859	0.819
1072	0.833	0.884	0.863	0.880	0.829	0.890	0.859	0.886



CASE CODE	Climate Zone 3				Climate Zone 4			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.834	0.885	0.866	0.881	0.830	0.891	0.863	0.886
1074	0.875	0.908	0.892	0.905	0.872	0.912	0.888	0.910
1075	0.877	0.909	0.895	0.906	0.874	0.913	0.892	0.910
1076	0.767	0.822	0.795	0.818	0.761	0.831	0.790	0.826
1077	0.807	0.781	0.824	0.779	0.802	0.787	0.819	0.785
1078	0.806	0.781	0.821	0.778	0.801	0.787	0.816	0.785
1079	0.768	0.761	0.798	0.758	0.763	0.769	0.792	0.765
1080	0.812	0.784	0.825	0.781	0.807	0.790	0.820	0.788
1081	0.789	0.772	0.810	0.769	0.784	0.779	0.805	0.776
1082	0.812	0.847	0.825	0.844	0.807	0.854	0.820	0.852
1083	0.882	0.843	0.896	0.840	0.878	0.847	0.893	0.845
1084	0.905	0.855	0.913	0.854	0.903	0.858	0.911	0.857
1085	0.891	0.848	0.904	0.846	0.888	0.851	0.901	0.849
1086	0.908	0.863	0.980	0.907	0.905	0.863	0.980	0.907
1087	0.952	0.891	0.980	0.907	0.950	0.891	0.980	0.907
1088	0.953	0.891	0.980	0.907	0.951	0.891	0.980	0.907
1089	0.952	0.963	0.980	0.980	0.950	0.963	0.980	0.980
1090	0.953	0.963	0.980	0.980	0.951	0.963	0.980	0.980
1091	0.908	0.933	0.980	0.980	0.905	0.933	0.980	0.980
1092	0.909	0.933	0.980	0.980	0.905	0.933	0.980	0.980
1093	0.909	0.863	0.980	0.907	0.905	0.863	0.980	0.907
1094	0.813	0.821	0.839	0.828	0.808	0.825	0.835	0.831
1095	0.843	0.826	0.860	0.832	0.839	0.829	0.856	0.833
1096	0.866	0.866	0.893	0.872	0.862	0.870	0.890	0.875
1097	0.866	0.936	0.893	0.943	0.862	0.940	0.890	0.945
1098	0.899	0.943	0.915	0.947	0.897	0.945	0.913	0.948
1099	0.813	0.887	0.839	0.895	0.808	0.891	0.835	0.898
1100	0.847	0.827	0.861	0.832	0.843	0.829	0.857	0.834
1101	0.903	0.873	0.917	0.876	0.901	0.875	0.914	0.878
1102	0.922	0.869	0.924	0.872	0.919	0.869	0.921	0.872
1103	0.958	0.893	0.958	0.894	0.956	0.893	0.956	0.894
1104	0.958	0.965	0.958	0.966	0.956	0.965	0.956	0.966
1105	0.958	0.965	0.959	0.966	0.957	0.965	0.957	0.966
1106	0.958	0.893	0.959	0.894	0.957	0.893	0.957	0.894
1107	0.922	0.940	0.924	0.942	0.919	0.940	0.922	0.942
1108	0.922	0.940	0.924	0.942	0.919	0.940	0.921	0.942



CASE CODE	Climate Zone 5				Climate Zone 6			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.747	0.760	0.776	0.779	0.772	0.722	0.800	0.747
1002	0.788	0.784	0.804	0.795	0.810	0.756	0.825	0.770
1003	0.748	0.760	0.779	0.779	0.773	0.723	0.802	0.749
1004	0.818	0.813	0.850	0.834	0.837	0.780	0.867	0.807
1005	0.864	0.839	0.880	0.851	0.878	0.817	0.894	0.832
1006	0.820	0.813	0.854	0.834	0.838	0.781	0.869	0.809
1007	0.818	0.879	0.850	0.901	0.837	0.843	0.867	0.873
1008	0.818	0.874	0.850	0.898	0.837	0.851	0.867	0.881
1009	0.866	0.904	0.885	0.918	0.879	0.890	0.897	0.908
1010	0.747	0.756	0.776	0.777	0.772	0.734	0.800	0.760
1011	0.790	0.784	0.807	0.795	0.811	0.757	0.827	0.771
1012	0.747	0.822	0.776	0.843	0.772	0.781	0.800	0.808
1013	0.866	0.839	0.885	0.851	0.879	0.818	0.897	0.834
1014	0.864	0.839	0.880	0.851	0.878	0.817	0.894	0.832
1015	0.820	0.813	0.854	0.834	0.838	0.781	0.869	0.809
1016	0.818	0.874	0.850	0.898	0.837	0.851	0.867	0.881
1017	0.871	0.911	0.885	0.923	0.884	0.889	0.898	0.903
1018	0.844	0.895	0.867	0.912	0.860	0.866	0.883	0.888
1019	0.871	0.843	0.885	0.853	0.884	0.822	0.898	0.835
1020	0.795	0.788	0.808	0.798	0.815	0.761	0.829	0.773
1021	0.844	0.828	0.867	0.843	0.860	0.801	0.883	0.821
1022	0.770	0.774	0.792	0.789	0.793	0.741	0.814	0.760
1023	0.749	0.762	0.776	0.779	0.773	0.738	0.800	0.747
1024	0.791	0.786	0.804	0.795	0.810	0.772	0.825	0.770
1025	0.751	0.762	0.779	0.779	0.774	0.738	0.802	0.749
1026	0.820	0.814	0.850	0.834	0.838	0.788	0.867	0.807
1027	0.865	0.840	0.880	0.851	0.879	0.824	0.894	0.832
1028	0.822	0.814	0.854	0.834	0.839	0.788	0.869	0.809
1029	0.820	0.880	0.850	0.901	0.838	0.852	0.867	0.873
1030	0.820	0.875	0.850	0.898	0.838	0.855	0.867	0.881
1031	0.867	0.905	0.885	0.918	0.880	0.893	0.897	0.908
1032	0.749	0.758	0.776	0.777	0.773	0.741	0.800	0.760
1033	0.793	0.786	0.807	0.795	0.812	0.772	0.827	0.771
1034	0.749	0.824	0.776	0.843	0.773	0.797	0.800	0.808
1035	0.867	0.840	0.885	0.851	0.880	0.824	0.897	0.834
1036	0.865	0.840	0.880	0.851	0.879	0.824	0.894	0.832



CASE CODE	Climate Zone 5				Climate Zone 6			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.822	0.814	0.854	0.834	0.839	0.788	0.869	0.809
1038	0.820	0.875	0.850	0.898	0.838	0.855	0.867	0.881
1039	0.872	0.912	0.885	0.923	0.885	0.897	0.898	0.903
1040	0.846	0.896	0.867	0.912	0.861	0.874	0.883	0.888
1041	0.872	0.843	0.885	0.853	0.885	0.830	0.898	0.835
1042	0.797	0.789	0.808	0.798	0.816	0.777	0.829	0.773
1043	0.846	0.829	0.867	0.843	0.861	0.809	0.883	0.821
1044	0.773	0.775	0.792	0.789	0.794	0.757	0.814	0.760
1045	0.896	0.862	0.895	0.862	0.911	0.848	0.910	0.847
1046	0.947	0.890	0.944	0.890	0.953	0.884	0.952	0.883
1047	0.947	0.962	0.944	0.962	0.953	0.956	0.952	0.955
1048	0.948	0.962	0.947	0.962	0.954	0.956	0.953	0.955
1049	0.948	0.962	0.947	0.962	0.954	0.960	0.953	0.960
1050	0.897	0.862	0.896	0.862	0.912	0.857	0.911	0.857
1051	0.897	0.931	0.896	0.931	0.912	0.926	0.911	0.926
1052	0.897	0.862	0.896	0.862	0.912	0.848	0.911	0.847
1053	0.896	0.931	0.895	0.931	0.911	0.916	0.910	0.915
1054	0.752	0.790	0.778	0.781	0.774	0.768	0.801	0.749
1055	0.822	0.843	0.851	0.834	0.838	0.820	0.867	0.808
1056	0.822	0.912	0.851	0.902	0.838	0.887	0.867	0.874
1057	0.824	0.912	0.856	0.902	0.840	0.887	0.870	0.876
1058	0.867	0.926	0.882	0.921	0.879	0.912	0.895	0.900
1059	0.869	0.926	0.886	0.921	0.880	0.912	0.897	0.902
1060	0.752	0.854	0.778	0.844	0.774	0.831	0.801	0.810
1061	0.795	0.802	0.809	0.797	0.813	0.790	0.828	0.773
1062	0.754	0.790	0.782	0.781	0.775	0.768	0.803	0.750
1063	0.793	0.802	0.806	0.797	0.812	0.790	0.826	0.771
1064	0.799	0.804	0.810	0.799	0.817	0.793	0.830	0.775
1065	0.775	0.797	0.794	0.790	0.796	0.780	0.815	0.762
1066	0.799	0.869	0.810	0.864	0.817	0.857	0.830	0.837
1067	0.873	0.859	0.886	0.854	0.885	0.847	0.899	0.836
1068	0.899	0.865	0.906	0.863	0.908	0.859	0.916	0.850
1069	0.884	0.861	0.896	0.857	0.894	0.851	0.907	0.842
1070	0.749	0.788	0.778	0.781	0.773	0.753	0.801	0.749
1071	0.820	0.843	0.851	0.834	0.837	0.813	0.867	0.808
1072	0.820	0.911	0.851	0.902	0.837	0.878	0.867	0.874



CASE CODE	Climate Zone 5				Climate Zone 6			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.822	0.911	0.856	0.902	0.838	0.879	0.870	0.876
1074	0.865	0.925	0.882	0.921	0.879	0.903	0.895	0.900
1075	0.867	0.925	0.886	0.921	0.880	0.904	0.897	0.902
1076	0.749	0.852	0.778	0.844	0.773	0.814	0.801	0.810
1077	0.792	0.801	0.809	0.797	0.812	0.775	0.828	0.773
1078	0.791	0.801	0.806	0.797	0.811	0.774	0.826	0.771
1079	0.751	0.788	0.782	0.781	0.774	0.754	0.803	0.750
1080	0.797	0.803	0.810	0.799	0.817	0.777	0.830	0.775
1081	0.773	0.795	0.794	0.790	0.795	0.765	0.815	0.762
1082	0.797	0.868	0.810	0.864	0.817	0.840	0.830	0.837
1083	0.872	0.858	0.886	0.854	0.885	0.839	0.899	0.836
1084	0.898	0.865	0.906	0.863	0.907	0.852	0.916	0.850
1085	0.883	0.860	0.896	0.857	0.894	0.844	0.907	0.842
1086	0.898	0.863	0.980	0.907	0.911	0.863	0.980	0.907
1087	0.948	0.891	0.980	0.907	0.953	0.891	0.980	0.907
1088	0.949	0.891	0.980	0.907	0.954	0.891	0.980	0.907
1089	0.948	0.963	0.980	0.980	0.953	0.963	0.980	0.980
1090	0.949	0.963	0.980	0.980	0.954	0.963	0.980	0.980
1091	0.898	0.933	0.980	0.980	0.911	0.933	0.980	0.980
1092	0.899	0.933	0.980	0.980	0.912	0.933	0.980	0.980
1093	0.899	0.863	0.980	0.907	0.912	0.863	0.980	0.907
1094	0.796	0.838	0.823	0.839	0.817	0.817	0.844	0.826
1095	0.829	0.836	0.846	0.838	0.847	0.824	0.864	0.830
1096	0.854	0.884	0.882	0.884	0.869	0.861	0.896	0.869
1097	0.854	0.956	0.882	0.955	0.869	0.931	0.896	0.940
1098	0.891	0.954	0.908	0.954	0.902	0.940	0.918	0.945
1099	0.796	0.906	0.823	0.907	0.817	0.883	0.844	0.893
1100	0.833	0.836	0.847	0.838	0.851	0.825	0.865	0.831
1101	0.894	0.882	0.908	0.882	0.906	0.871	0.919	0.875
1102	0.911	0.869	0.913	0.872	0.925	0.869	0.927	0.872
1103	0.953	0.893	0.952	0.894	0.959	0.893	0.959	0.894
1104	0.953	0.965	0.952	0.966	0.959	0.965	0.959	0.966
1105	0.954	0.965	0.954	0.966	0.959	0.965	0.960	0.966
1106	0.954	0.893	0.954	0.894	0.959	0.893	0.960	0.894
1107	0.911	0.940	0.914	0.942	0.925	0.940	0.927	0.942
1108	0.911	0.940	0.913	0.942	0.925	0.940	0.927	0.942



CASE CODE	Climate Zone 7				Climate Zone 8			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.788	0.760	0.815	0.779	0.775	0.752	0.803	0.770
1002	0.823	0.784	0.838	0.795	0.812	0.775	0.828	0.785
1003	0.788	0.760	0.816	0.779	0.776	0.752	0.805	0.770
1004	0.848	0.813	0.878	0.834	0.839	0.809	0.869	0.829
1005	0.887	0.839	0.903	0.851	0.880	0.835	0.896	0.846
1006	0.849	0.813	0.879	0.834	0.840	0.810	0.871	0.830
1007	0.848	0.879	0.878	0.901	0.839	0.875	0.869	0.896
1008	0.848	0.874	0.878	0.898	0.839	0.881	0.869	0.902
1009	0.888	0.904	0.905	0.918	0.881	0.908	0.898	0.920
1010	0.788	0.756	0.815	0.777	0.775	0.761	0.803	0.780
1011	0.824	0.784	0.839	0.795	0.813	0.776	0.830	0.786
1012	0.788	0.822	0.815	0.843	0.775	0.813	0.803	0.832
1013	0.888	0.839	0.905	0.851	0.881	0.835	0.898	0.847
1014	0.887	0.839	0.903	0.851	0.880	0.835	0.896	0.846
1015	0.849	0.813	0.879	0.834	0.840	0.810	0.871	0.830
1016	0.848	0.874	0.878	0.898	0.839	0.881	0.869	0.902
1017	0.893	0.911	0.907	0.923	0.886	0.907	0.900	0.917
1018	0.870	0.895	0.892	0.912	0.862	0.891	0.884	0.906
1019	0.893	0.843	0.907	0.853	0.886	0.839	0.900	0.848
1020	0.828	0.788	0.842	0.798	0.818	0.779	0.831	0.788
1021	0.870	0.828	0.892	0.843	0.862	0.824	0.884	0.839
1022	0.808	0.774	0.828	0.789	0.796	0.765	0.817	0.779
1023	0.788	0.762	0.815	0.779	0.776	0.762	0.803	0.770
1024	0.823	0.786	0.838	0.795	0.813	0.786	0.828	0.785
1025	0.788	0.762	0.816	0.779	0.777	0.762	0.805	0.770
1026	0.849	0.814	0.878	0.834	0.840	0.814	0.869	0.829
1027	0.887	0.840	0.903	0.851	0.880	0.840	0.896	0.846
1028	0.850	0.814	0.879	0.834	0.841	0.814	0.871	0.830
1029	0.849	0.880	0.878	0.901	0.840	0.880	0.869	0.896
1030	0.849	0.875	0.878	0.898	0.840	0.882	0.869	0.902
1031	0.888	0.905	0.905	0.918	0.881	0.909	0.898	0.920
1032	0.788	0.758	0.815	0.777	0.776	0.764	0.803	0.780
1033	0.823	0.786	0.839	0.795	0.814	0.786	0.830	0.786
1034	0.788	0.824	0.815	0.843	0.776	0.824	0.803	0.832
1035	0.888	0.840	0.905	0.851	0.881	0.840	0.898	0.847
1036	0.887	0.840	0.903	0.851	0.880	0.840	0.896	0.846



CASE CODE	Climate Zone 7				Climate Zone 8			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.850	0.814	0.879	0.834	0.841	0.814	0.871	0.830
1038	0.849	0.875	0.878	0.898	0.840	0.882	0.869	0.902
1039	0.892	0.912	0.907	0.923	0.886	0.912	0.900	0.917
1040	0.870	0.896	0.892	0.912	0.863	0.896	0.884	0.906
1041	0.892	0.843	0.907	0.853	0.886	0.844	0.900	0.848
1042	0.828	0.789	0.842	0.798	0.818	0.789	0.831	0.788
1043	0.870	0.829	0.892	0.843	0.863	0.829	0.884	0.839
1044	0.808	0.775	0.828	0.789	0.797	0.776	0.817	0.779
1045	0.920	0.862	0.920	0.862	0.913	0.852	0.912	0.852
1046	0.957	0.890	0.957	0.890	0.954	0.886	0.953	0.886
1047	0.957	0.962	0.957	0.962	0.954	0.958	0.953	0.958
1048	0.958	0.962	0.957	0.962	0.955	0.958	0.954	0.958
1049	0.958	0.962	0.957	0.962	0.955	0.962	0.954	0.962
1050	0.921	0.862	0.920	0.862	0.913	0.861	0.913	0.861
1051	0.921	0.931	0.920	0.931	0.913	0.931	0.913	0.930
1052	0.921	0.862	0.920	0.862	0.913	0.853	0.913	0.852
1053	0.920	0.931	0.920	0.931	0.913	0.921	0.912	0.921
1054	0.788	0.790	0.815	0.781	0.777	0.784	0.804	0.771
1055	0.849	0.843	0.878	0.834	0.840	0.838	0.870	0.830
1056	0.849	0.912	0.878	0.902	0.840	0.905	0.870	0.897
1057	0.849	0.912	0.879	0.902	0.842	0.905	0.872	0.898
1058	0.887	0.926	0.903	0.921	0.881	0.923	0.897	0.915
1059	0.888	0.926	0.905	0.921	0.882	0.923	0.899	0.916
1060	0.788	0.854	0.815	0.844	0.777	0.848	0.804	0.834
1061	0.824	0.802	0.840	0.797	0.815	0.799	0.831	0.787
1062	0.789	0.790	0.817	0.781	0.778	0.784	0.806	0.772
1063	0.823	0.802	0.839	0.797	0.814	0.799	0.829	0.787
1064	0.829	0.804	0.843	0.799	0.820	0.801	0.833	0.789
1065	0.808	0.797	0.829	0.790	0.798	0.793	0.818	0.780
1066	0.829	0.869	0.843	0.864	0.820	0.866	0.833	0.853
1067	0.893	0.859	0.907	0.854	0.887	0.856	0.901	0.849
1068	0.913	0.865	0.922	0.863	0.909	0.864	0.917	0.858
1069	0.900	0.861	0.913	0.857	0.895	0.859	0.908	0.853
1070	0.788	0.788	0.815	0.781	0.776	0.774	0.804	0.771
1071	0.848	0.843	0.878	0.834	0.839	0.833	0.870	0.830
1072	0.848	0.911	0.878	0.902	0.839	0.900	0.870	0.897



CASE CODE	Climate Zone 7				Climate Zone 8			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.849	0.911	0.879	0.902	0.841	0.901	0.872	0.898
1074	0.887	0.925	0.903	0.921	0.880	0.917	0.897	0.915
1075	0.888	0.925	0.905	0.921	0.881	0.918	0.899	0.916
1076	0.788	0.852	0.815	0.844	0.776	0.837	0.804	0.834
1077	0.824	0.801	0.840	0.797	0.815	0.789	0.831	0.787
1078	0.824	0.801	0.839	0.797	0.814	0.789	0.829	0.787
1079	0.789	0.788	0.817	0.781	0.777	0.774	0.806	0.772
1080	0.829	0.803	0.843	0.799	0.819	0.791	0.833	0.789
1081	0.808	0.795	0.829	0.790	0.797	0.782	0.818	0.780
1082	0.829	0.868	0.843	0.864	0.819	0.855	0.833	0.853
1083	0.893	0.858	0.907	0.854	0.886	0.851	0.901	0.849
1084	0.913	0.865	0.922	0.863	0.909	0.859	0.917	0.858
1085	0.900	0.860	0.913	0.857	0.895	0.854	0.908	0.853
1086	0.919	0.863	0.980	0.907	0.913	0.863	0.980	0.907
1087	0.957	0.891	0.980	0.907	0.954	0.891	0.980	0.907
1088	0.957	0.891	0.980	0.907	0.955	0.891	0.980	0.907
1089	0.957	0.963	0.980	0.980	0.954	0.963	0.980	0.980
1090	0.957	0.963	0.980	0.980	0.955	0.963	0.980	0.980
1091	0.919	0.933	0.980	0.980	0.913	0.933	0.980	0.980
1092	0.920	0.933	0.980	0.980	0.913	0.933	0.980	0.980
1093	0.920	0.863	0.980	0.907	0.913	0.863	0.980	0.907
1094	0.819	0.824	0.845	0.830	0.818	0.822	0.844	0.829
1095	0.848	0.828	0.865	0.833	0.848	0.827	0.864	0.832
1096	0.870	0.869	0.897	0.874	0.870	0.867	0.896	0.873
1097	0.870	0.940	0.897	0.945	0.870	0.937	0.896	0.944
1098	0.902	0.945	0.918	0.948	0.902	0.944	0.918	0.947
1099	0.819	0.891	0.845	0.897	0.818	0.889	0.844	0.896
1100	0.852	0.829	0.866	0.833	0.851	0.828	0.866	0.833
1101	0.906	0.875	0.920	0.878	0.906	0.874	0.920	0.877
1102	0.926	0.869	0.928	0.872	0.925	0.869	0.927	0.872
1103	0.959	0.893	0.960	0.894	0.959	0.893	0.959	0.894
1104	0.959	0.965	0.960	0.966	0.959	0.965	0.959	0.966
1105	0.960	0.965	0.960	0.966	0.959	0.965	0.960	0.966
1106	0.960	0.893	0.960	0.894	0.959	0.893	0.960	0.894
1107	0.926	0.940	0.928	0.942	0.925	0.940	0.928	0.942
1108	0.926	0.940	0.928	0.942	0.925	0.940	0.927	0.942



CASE CODE	Climate Zone 9				Climate Zone 10			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.759	0.702	0.788	0.723	0.759	0.674	0.788	0.696
1002	0.799	0.732	0.814	0.743	0.799	0.708	0.814	0.718
1003	0.761	0.704	0.791	0.726	0.761	0.676	0.791	0.700
1004	0.827	0.775	0.858	0.798	0.827	0.756	0.858	0.780
1005	0.871	0.809	0.887	0.820	0.871	0.794	0.887	0.805
1006	0.829	0.777	0.862	0.802	0.829	0.759	0.862	0.785
1007	0.827	0.838	0.858	0.863	0.827	0.817	0.858	0.843
1008	0.827	0.853	0.858	0.876	0.827	0.837	0.858	0.861
1009	0.873	0.887	0.891	0.900	0.873	0.875	0.891	0.889
1010	0.759	0.722	0.788	0.742	0.759	0.699	0.788	0.720
1011	0.801	0.734	0.817	0.746	0.801	0.710	0.817	0.723
1012	0.759	0.759	0.788	0.781	0.759	0.728	0.788	0.752
1013	0.873	0.811	0.891	0.824	0.873	0.797	0.891	0.811
1014	0.871	0.809	0.887	0.820	0.871	0.794	0.887	0.805
1015	0.829	0.777	0.862	0.802	0.829	0.759	0.862	0.785
1016	0.827	0.853	0.858	0.876	0.827	0.837	0.858	0.861
1017	0.877	0.880	0.892	0.890	0.877	0.864	0.892	0.874
1018	0.852	0.859	0.875	0.876	0.852	0.841	0.875	0.859
1019	0.877	0.814	0.892	0.823	0.877	0.800	0.892	0.809
1020	0.805	0.737	0.818	0.746	0.805	0.713	0.818	0.722
1021	0.852	0.794	0.875	0.810	0.852	0.778	0.875	0.794
1022	0.782	0.719	0.803	0.734	0.782	0.693	0.803	0.709
1023	0.761	0.745	0.788	0.723	0.761	0.718	0.788	0.696
1024	0.801	0.776	0.814	0.743	0.801	0.754	0.814	0.718
1025	0.763	0.745	0.791	0.726	0.763	0.719	0.791	0.700
1026	0.829	0.795	0.858	0.798	0.829	0.777	0.858	0.780
1027	0.872	0.829	0.887	0.820	0.872	0.815	0.887	0.805
1028	0.830	0.795	0.862	0.802	0.830	0.778	0.862	0.785
1029	0.829	0.860	0.858	0.863	0.829	0.840	0.858	0.843
1030	0.829	0.868	0.858	0.876	0.829	0.851	0.858	0.861
1031	0.874	0.901	0.891	0.900	0.874	0.889	0.891	0.889
1032	0.761	0.751	0.788	0.742	0.761	0.728	0.788	0.720
1033	0.802	0.776	0.817	0.746	0.802	0.754	0.817	0.723
1034	0.761	0.805	0.788	0.781	0.761	0.777	0.788	0.752
1035	0.874	0.829	0.891	0.824	0.874	0.816	0.891	0.811
1036	0.872	0.829	0.887	0.820	0.872	0.815	0.887	0.805



CASE CODE	Climate Zone 9				Climate Zone 10			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.830	0.795	0.862	0.802	0.830	0.778	0.862	0.785
1038	0.829	0.868	0.858	0.876	0.829	0.851	0.858	0.861
1039	0.878	0.902	0.892	0.890	0.878	0.887	0.892	0.874
1040	0.853	0.881	0.875	0.876	0.853	0.863	0.875	0.859
1041	0.878	0.834	0.892	0.823	0.878	0.821	0.892	0.809
1042	0.807	0.780	0.818	0.746	0.807	0.759	0.818	0.722
1043	0.853	0.814	0.875	0.810	0.853	0.799	0.875	0.794
1044	0.784	0.762	0.803	0.734	0.784	0.738	0.803	0.709
1045	0.904	0.820	0.902	0.818	0.904	0.802	0.902	0.799
1046	0.950	0.872	0.948	0.870	0.950	0.864	0.948	0.861
1047	0.950	0.943	0.948	0.941	0.950	0.935	0.948	0.931
1048	0.951	0.944	0.950	0.943	0.951	0.936	0.950	0.934
1049	0.951	0.950	0.950	0.949	0.951	0.943	0.950	0.942
1050	0.904	0.834	0.904	0.833	0.904	0.818	0.904	0.817
1051	0.904	0.901	0.904	0.901	0.904	0.885	0.904	0.884
1052	0.904	0.821	0.904	0.820	0.904	0.803	0.904	0.801
1053	0.904	0.887	0.902	0.885	0.904	0.867	0.902	0.864
1054	0.763	0.769	0.790	0.724	0.763	0.744	0.790	0.698
1055	0.830	0.821	0.859	0.799	0.830	0.804	0.859	0.781
1056	0.830	0.887	0.859	0.864	0.830	0.869	0.859	0.845
1057	0.832	0.887	0.863	0.868	0.832	0.870	0.863	0.850
1058	0.873	0.912	0.888	0.887	0.873	0.898	0.888	0.871
1059	0.875	0.912	0.892	0.891	0.875	0.899	0.892	0.877
1060	0.763	0.831	0.790	0.783	0.763	0.804	0.790	0.754
1061	0.804	0.790	0.819	0.747	0.804	0.769	0.819	0.724
1062	0.765	0.769	0.792	0.727	0.765	0.745	0.792	0.702
1063	0.802	0.790	0.816	0.744	0.802	0.769	0.816	0.720
1064	0.808	0.793	0.820	0.747	0.808	0.772	0.820	0.723
1065	0.785	0.781	0.805	0.736	0.785	0.758	0.805	0.710
1066	0.808	0.858	0.820	0.808	0.808	0.835	0.820	0.782
1067	0.879	0.847	0.893	0.824	0.879	0.835	0.893	0.810
1068	0.903	0.859	0.911	0.839	0.903	0.849	0.911	0.828
1069	0.889	0.851	0.901	0.832	0.889	0.840	0.901	0.820
1070	0.761	0.727	0.790	0.724	0.761	0.700	0.790	0.698
1071	0.829	0.801	0.859	0.799	0.829	0.783	0.859	0.781
1072	0.829	0.866	0.859	0.864	0.829	0.847	0.859	0.845



CASE CODE	Climate Zone 9				Climate Zone 10			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.830	0.868	0.863	0.868	0.830	0.849	0.863	0.850
1074	0.872	0.891	0.888	0.887	0.872	0.875	0.888	0.871
1075	0.874	0.893	0.892	0.891	0.874	0.878	0.892	0.877
1076	0.761	0.786	0.790	0.783	0.761	0.756	0.790	0.754
1077	0.802	0.748	0.819	0.747	0.802	0.725	0.819	0.724
1078	0.801	0.747	0.816	0.744	0.801	0.723	0.816	0.720
1079	0.763	0.728	0.792	0.727	0.763	0.702	0.792	0.702
1080	0.807	0.750	0.820	0.747	0.807	0.727	0.820	0.723
1081	0.784	0.738	0.805	0.736	0.784	0.713	0.805	0.710
1082	0.807	0.811	0.820	0.808	0.807	0.785	0.820	0.782
1083	0.878	0.827	0.893	0.824	0.878	0.814	0.893	0.810
1084	0.903	0.841	0.911	0.839	0.903	0.830	0.911	0.828
1085	0.888	0.833	0.901	0.832	0.888	0.821	0.901	0.820
1086	0.905	0.863	0.980	0.907	0.905	0.846	0.980	0.907
1087	0.950	0.891	0.980	0.907	0.950	0.884	0.980	0.907
1088	0.951	0.891	0.980	0.907	0.951	0.884	0.980	0.907
1089	0.950	0.963	0.980	0.980	0.950	0.955	0.980	0.980
1090	0.951	0.963	0.980	0.980	0.951	0.956	0.980	0.980
1091	0.905	0.933	0.980	0.980	0.905	0.915	0.980	0.980
1092	0.905	0.933	0.980	0.980	0.905	0.915	0.980	0.980
1093	0.905	0.863	0.980	0.907	0.905	0.846	0.980	0.907
1094	0.817	0.817	0.843	0.826	0.821	0.812	0.847	0.822
1095	0.847	0.824	0.863	0.830	0.850	0.821	0.866	0.829
1096	0.869	0.862	0.895	0.869	0.872	0.856	0.898	0.866
1097	0.869	0.932	0.895	0.940	0.872	0.926	0.898	0.936
1098	0.901	0.940	0.917	0.945	0.903	0.937	0.919	0.943
1099	0.817	0.883	0.843	0.893	0.821	0.878	0.847	0.889
1100	0.850	0.825	0.865	0.831	0.854	0.823	0.868	0.830
1101	0.905	0.871	0.919	0.875	0.908	0.868	0.921	0.873
1102	0.924	0.869	0.926	0.872	0.927	0.869	0.929	0.872
1103	0.959	0.893	0.959	0.894	0.960	0.893	0.960	0.894
1104	0.959	0.965	0.959	0.966	0.960	0.965	0.960	0.966
1105	0.959	0.965	0.960	0.966	0.960	0.965	0.961	0.966
1106	0.959	0.893	0.960	0.894	0.960	0.893	0.961	0.894
1107	0.925	0.940	0.927	0.942	0.927	0.940	0.930	0.942
1108	0.924	0.940	0.926	0.942	0.927	0.940	0.929	0.942



CASE CODE	Climate Zone 11				Climate Zone 12			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.743	0.645	0.773	0.669	0.750	0.674	0.779	0.696
1002	0.786	0.683	0.801	0.694	0.791	0.708	0.806	0.718
1003	0.745	0.648	0.777	0.675	0.751	0.676	0.782	0.700
1004	0.815	0.737	0.848	0.762	0.820	0.756	0.852	0.780
1005	0.862	0.779	0.879	0.790	0.866	0.794	0.882	0.805
1006	0.818	0.740	0.852	0.769	0.822	0.759	0.856	0.785
1007	0.815	0.796	0.848	0.824	0.820	0.817	0.852	0.843
1008	0.815	0.821	0.848	0.846	0.820	0.837	0.852	0.861
1009	0.864	0.863	0.883	0.878	0.868	0.875	0.886	0.889
1010	0.743	0.677	0.773	0.698	0.750	0.699	0.779	0.720
1011	0.788	0.686	0.805	0.700	0.793	0.710	0.810	0.723
1012	0.743	0.698	0.773	0.723	0.750	0.728	0.779	0.752
1013	0.864	0.783	0.883	0.798	0.868	0.797	0.886	0.811
1014	0.862	0.779	0.879	0.790	0.866	0.794	0.882	0.805
1015	0.818	0.740	0.852	0.769	0.822	0.759	0.856	0.785
1016	0.815	0.821	0.848	0.846	0.820	0.837	0.852	0.861
1017	0.869	0.849	0.883	0.859	0.872	0.864	0.887	0.874
1018	0.842	0.822	0.865	0.841	0.846	0.841	0.869	0.859
1019	0.869	0.785	0.883	0.795	0.872	0.800	0.887	0.809
1020	0.792	0.689	0.805	0.698	0.797	0.713	0.811	0.722
1021	0.842	0.761	0.865	0.778	0.846	0.778	0.869	0.794
1022	0.767	0.667	0.789	0.683	0.773	0.693	0.795	0.709
1023	0.746	0.692	0.773	0.669	0.752	0.718	0.779	0.696
1024	0.788	0.731	0.801	0.694	0.793	0.754	0.806	0.718
1025	0.748	0.693	0.777	0.675	0.754	0.719	0.782	0.700
1026	0.817	0.759	0.848	0.762	0.822	0.777	0.852	0.780
1027	0.864	0.801	0.879	0.790	0.867	0.815	0.882	0.805
1028	0.820	0.760	0.852	0.769	0.824	0.778	0.856	0.785
1029	0.817	0.820	0.848	0.824	0.822	0.840	0.852	0.843
1030	0.817	0.835	0.848	0.846	0.822	0.851	0.852	0.861
1031	0.866	0.876	0.883	0.878	0.869	0.889	0.886	0.889
1032	0.746	0.705	0.773	0.698	0.752	0.728	0.779	0.720
1033	0.790	0.732	0.805	0.700	0.795	0.754	0.810	0.723
1034	0.746	0.748	0.773	0.723	0.752	0.777	0.779	0.752
1035	0.866	0.803	0.883	0.798	0.869	0.816	0.886	0.811
1036	0.864	0.801	0.879	0.790	0.867	0.815	0.882	0.805



CASE CODE	Climate Zone 11				Climate Zone 12			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.820	0.760	0.852	0.769	0.824	0.778	0.856	0.785
1038	0.817	0.835	0.848	0.846	0.822	0.851	0.852	0.861
1039	0.871	0.873	0.883	0.859	0.874	0.887	0.887	0.874
1040	0.844	0.846	0.865	0.841	0.847	0.863	0.869	0.859
1041	0.871	0.808	0.883	0.795	0.874	0.821	0.887	0.809
1042	0.795	0.737	0.805	0.698	0.799	0.759	0.811	0.722
1043	0.844	0.783	0.865	0.778	0.847	0.799	0.869	0.794
1044	0.770	0.714	0.789	0.683	0.776	0.738	0.795	0.709
1045	0.895	0.783	0.893	0.780	0.898	0.802	0.896	0.799
1046	0.946	0.857	0.943	0.853	0.948	0.864	0.945	0.861
1047	0.946	0.926	0.943	0.922	0.948	0.935	0.945	0.931
1048	0.947	0.928	0.946	0.925	0.949	0.936	0.947	0.934
1049	0.947	0.936	0.946	0.934	0.949	0.943	0.947	0.942
1050	0.895	0.803	0.894	0.801	0.899	0.818	0.898	0.817
1051	0.895	0.868	0.894	0.866	0.899	0.885	0.898	0.884
1052	0.895	0.784	0.894	0.783	0.899	0.803	0.898	0.801
1053	0.895	0.847	0.893	0.843	0.898	0.867	0.896	0.864
1054	0.749	0.719	0.775	0.671	0.755	0.744	0.781	0.698
1055	0.820	0.787	0.849	0.764	0.824	0.804	0.853	0.781
1056	0.820	0.851	0.849	0.826	0.824	0.869	0.853	0.845
1057	0.822	0.852	0.854	0.833	0.826	0.870	0.857	0.850
1058	0.865	0.884	0.880	0.856	0.868	0.898	0.883	0.871
1059	0.867	0.885	0.884	0.863	0.870	0.899	0.887	0.877
1060	0.749	0.777	0.775	0.725	0.755	0.804	0.781	0.754
1061	0.792	0.748	0.807	0.701	0.797	0.769	0.812	0.724
1062	0.751	0.720	0.779	0.677	0.757	0.745	0.784	0.702
1063	0.791	0.747	0.803	0.695	0.795	0.769	0.808	0.720
1064	0.797	0.751	0.807	0.699	0.801	0.772	0.812	0.723
1065	0.773	0.735	0.791	0.685	0.778	0.758	0.796	0.710
1066	0.797	0.812	0.807	0.756	0.801	0.835	0.812	0.782
1067	0.872	0.822	0.884	0.795	0.875	0.835	0.888	0.810
1068	0.898	0.839	0.905	0.817	0.900	0.849	0.907	0.828
1069	0.882	0.829	0.894	0.808	0.885	0.840	0.897	0.820
1070	0.746	0.673	0.775	0.671	0.752	0.700	0.781	0.698
1071	0.818	0.765	0.849	0.764	0.822	0.783	0.853	0.781
1072	0.818	0.827	0.849	0.826	0.822	0.847	0.853	0.845



CASE CODE	Climate Zone 11				Climate Zone 12			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.820	0.831	0.854	0.833	0.824	0.849	0.857	0.850
1074	0.864	0.860	0.880	0.856	0.867	0.875	0.883	0.871
1075	0.866	0.864	0.884	0.863	0.869	0.878	0.887	0.877
1076	0.746	0.727	0.775	0.725	0.752	0.756	0.781	0.754
1077	0.790	0.702	0.807	0.701	0.795	0.725	0.812	0.724
1078	0.788	0.699	0.803	0.695	0.793	0.723	0.808	0.720
1079	0.748	0.675	0.779	0.677	0.754	0.702	0.784	0.702
1080	0.794	0.703	0.807	0.699	0.799	0.727	0.812	0.723
1081	0.770	0.688	0.791	0.685	0.775	0.713	0.796	0.710
1082	0.794	0.760	0.807	0.756	0.799	0.785	0.812	0.782
1083	0.870	0.800	0.884	0.795	0.874	0.814	0.888	0.810
1084	0.897	0.819	0.905	0.817	0.899	0.830	0.907	0.828
1085	0.881	0.809	0.894	0.808	0.884	0.821	0.897	0.820
1086	0.897	0.830	0.980	0.907	0.900	0.846	0.980	0.907
1087	0.947	0.877	0.980	0.907	0.948	0.884	0.980	0.907
1088	0.948	0.877	0.980	0.907	0.949	0.884	0.980	0.907
1089	0.947	0.948	0.980	0.980	0.948	0.955	0.980	0.980
1090	0.948	0.948	0.980	0.980	0.949	0.956	0.980	0.980
1091	0.897	0.897	0.980	0.980	0.900	0.915	0.980	0.980
1092	0.897	0.898	0.980	0.980	0.901	0.915	0.980	0.980
1093	0.897	0.830	0.980	0.907	0.901	0.846	0.980	0.907
1094	0.816	0.811	0.843	0.822	0.816	0.814	0.842	0.824
1095	0.846	0.821	0.863	0.828	0.846	0.823	0.862	0.829
1096	0.868	0.855	0.895	0.865	0.868	0.859	0.895	0.867
1097	0.868	0.924	0.895	0.935	0.868	0.928	0.895	0.938
1098	0.901	0.936	0.917	0.943	0.901	0.938	0.917	0.944
1099	0.816	0.876	0.843	0.888	0.816	0.880	0.842	0.891
1100	0.850	0.822	0.864	0.829	0.849	0.824	0.864	0.830
1101	0.905	0.867	0.919	0.873	0.905	0.869	0.918	0.874
1102	0.924	0.869	0.926	0.872	0.924	0.869	0.926	0.872
1103	0.959	0.893	0.959	0.894	0.958	0.893	0.959	0.894
1104	0.959	0.965	0.959	0.966	0.958	0.965	0.959	0.966
1105	0.959	0.965	0.960	0.966	0.959	0.965	0.959	0.966
1106	0.959	0.893	0.960	0.894	0.959	0.893	0.959	0.894
1107	0.924	0.940	0.927	0.942	0.924	0.940	0.926	0.942
1108	0.924	0.940	0.926	0.942	0.924	0.940	0.926	0.942



CASE CODE	Climate Zone 13				Climate Zone 14			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.743	0.667	0.773	0.689	0.715	0.617	0.746	0.642
1002	0.786	0.702	0.801	0.712	0.762	0.659	0.777	0.669
1003	0.745	0.669	0.777	0.694	0.718	0.621	0.752	0.649
1004	0.815	0.751	0.848	0.776	0.794	0.717	0.828	0.745
1005	0.862	0.790	0.879	0.801	0.846	0.764	0.863	0.776
1006	0.818	0.754	0.852	0.781	0.797	0.721	0.835	0.753
1007	0.815	0.812	0.848	0.839	0.794	0.775	0.828	0.805
1008	0.815	0.833	0.848	0.857	0.794	0.805	0.828	0.831
1009	0.864	0.872	0.883	0.886	0.849	0.851	0.870	0.866
1010	0.743	0.694	0.773	0.714	0.715	0.654	0.746	0.676
1011	0.788	0.704	0.805	0.717	0.765	0.663	0.783	0.677
1012	0.743	0.721	0.773	0.745	0.715	0.667	0.746	0.694
1013	0.864	0.793	0.883	0.807	0.849	0.768	0.870	0.784
1014	0.862	0.790	0.879	0.801	0.846	0.764	0.863	0.776
1015	0.818	0.754	0.852	0.781	0.797	0.721	0.835	0.753
1016	0.815	0.833	0.848	0.857	0.794	0.805	0.828	0.831
1017	0.869	0.860	0.883	0.871	0.854	0.834	0.868	0.843
1018	0.842	0.836	0.865	0.854	0.824	0.804	0.848	0.824
1019	0.869	0.796	0.883	0.805	0.854	0.771	0.868	0.780
1020	0.792	0.707	0.805	0.716	0.769	0.665	0.782	0.674
1021	0.842	0.773	0.865	0.790	0.824	0.744	0.848	0.762
1022	0.767	0.687	0.789	0.702	0.741	0.641	0.764	0.658
1023	0.746	0.712	0.773	0.689	0.720	0.666	0.746	0.642
1024	0.788	0.748	0.801	0.712	0.766	0.709	0.777	0.669
1025	0.748	0.713	0.777	0.694	0.722	0.668	0.752	0.649
1026	0.817	0.772	0.848	0.776	0.797	0.740	0.828	0.745
1027	0.864	0.812	0.879	0.801	0.849	0.787	0.863	0.776
1028	0.820	0.773	0.852	0.781	0.800	0.743	0.835	0.753
1029	0.817	0.835	0.848	0.839	0.797	0.800	0.828	0.805
1030	0.817	0.847	0.848	0.857	0.797	0.819	0.828	0.831
1031	0.866	0.886	0.883	0.886	0.852	0.864	0.870	0.866
1032	0.746	0.722	0.773	0.714	0.720	0.682	0.746	0.676
1033	0.790	0.749	0.805	0.717	0.769	0.711	0.783	0.677
1034	0.746	0.770	0.773	0.745	0.720	0.720	0.746	0.694
1035	0.866	0.813	0.883	0.807	0.852	0.790	0.870	0.784
1036	0.864	0.812	0.879	0.801	0.849	0.787	0.863	0.776



CASE CODE	Climate Zone 13				Climate Zone 14			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.820	0.773	0.852	0.781	0.800	0.743	0.835	0.753
1038	0.817	0.847	0.848	0.857	0.797	0.819	0.828	0.831
1039	0.871	0.884	0.883	0.871	0.856	0.859	0.868	0.843
1040	0.844	0.859	0.865	0.854	0.826	0.829	0.848	0.824
1041	0.871	0.818	0.883	0.805	0.856	0.794	0.868	0.780
1042	0.795	0.753	0.805	0.716	0.773	0.715	0.782	0.674
1043	0.844	0.795	0.865	0.790	0.826	0.767	0.848	0.762
1044	0.770	0.732	0.789	0.702	0.746	0.690	0.764	0.658
1045	0.895	0.797	0.893	0.794	0.878	0.765	0.875	0.761
1046	0.946	0.862	0.943	0.859	0.939	0.849	0.935	0.844
1047	0.946	0.932	0.943	0.929	0.939	0.917	0.935	0.912
1048	0.947	0.934	0.946	0.932	0.940	0.920	0.938	0.917
1049	0.947	0.941	0.946	0.940	0.940	0.929	0.938	0.927
1050	0.895	0.814	0.894	0.813	0.879	0.787	0.878	0.786
1051	0.895	0.880	0.894	0.879	0.879	0.851	0.878	0.849
1052	0.895	0.798	0.894	0.797	0.879	0.766	0.878	0.764
1053	0.895	0.862	0.893	0.859	0.878	0.827	0.875	0.822
1054	0.749	0.738	0.775	0.691	0.724	0.694	0.749	0.644
1055	0.820	0.800	0.849	0.777	0.801	0.770	0.831	0.746
1056	0.820	0.864	0.849	0.840	0.801	0.832	0.831	0.807
1057	0.822	0.865	0.854	0.846	0.804	0.835	0.838	0.816
1058	0.865	0.895	0.880	0.867	0.851	0.870	0.865	0.840
1059	0.867	0.896	0.884	0.874	0.854	0.872	0.871	0.849
1060	0.749	0.798	0.775	0.747	0.724	0.750	0.749	0.696
1061	0.792	0.764	0.807	0.719	0.772	0.727	0.785	0.679
1062	0.751	0.738	0.779	0.696	0.727	0.696	0.755	0.651
1063	0.791	0.763	0.803	0.714	0.769	0.725	0.780	0.671
1064	0.797	0.767	0.807	0.717	0.776	0.730	0.784	0.675
1065	0.773	0.752	0.791	0.704	0.750	0.712	0.767	0.659
1066	0.797	0.829	0.807	0.775	0.776	0.789	0.784	0.730
1067	0.872	0.832	0.884	0.806	0.859	0.810	0.870	0.781
1068	0.898	0.847	0.905	0.825	0.888	0.830	0.894	0.806
1069	0.882	0.838	0.894	0.817	0.871	0.818	0.882	0.795
1070	0.746	0.693	0.775	0.691	0.719	0.645	0.749	0.644
1071	0.818	0.779	0.849	0.777	0.798	0.747	0.831	0.746
1072	0.818	0.842	0.849	0.840	0.798	0.808	0.831	0.807



CASE CODE	Climate Zone 13				Climate Zone 14			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.820	0.845	0.854	0.846	0.801	0.812	0.838	0.816
1074	0.864	0.871	0.880	0.867	0.849	0.845	0.865	0.840
1075	0.866	0.875	0.884	0.874	0.852	0.849	0.871	0.849
1076	0.746	0.749	0.775	0.747	0.719	0.698	0.749	0.696
1077	0.790	0.720	0.807	0.719	0.768	0.679	0.785	0.679
1078	0.788	0.717	0.803	0.714	0.765	0.676	0.780	0.671
1079	0.748	0.695	0.779	0.696	0.722	0.649	0.755	0.651
1080	0.794	0.721	0.807	0.717	0.772	0.680	0.784	0.675
1081	0.770	0.707	0.791	0.704	0.745	0.663	0.767	0.659
1082	0.794	0.779	0.807	0.775	0.772	0.735	0.784	0.730
1083	0.870	0.810	0.884	0.806	0.856	0.786	0.870	0.781
1084	0.897	0.827	0.905	0.825	0.886	0.809	0.894	0.806
1085	0.881	0.818	0.894	0.817	0.869	0.797	0.882	0.795
1086	0.897	0.842	0.980	0.907	0.882	0.813	0.980	0.907
1087	0.947	0.882	0.980	0.907	0.940	0.869	0.980	0.907
1088	0.948	0.882	0.980	0.907	0.942	0.871	0.980	0.907
1089	0.947	0.953	0.980	0.980	0.940	0.940	0.980	0.980
1090	0.948	0.954	0.980	0.980	0.942	0.941	0.980	0.980
1091	0.897	0.910	0.980	0.980	0.882	0.879	0.980	0.980
1092	0.897	0.911	0.980	0.980	0.883	0.880	0.980	0.980
1093	0.897	0.842	0.980	0.907	0.883	0.814	0.980	0.907
1094	0.813	0.814	0.840	0.824	0.804	0.812	0.832	0.823
1095	0.844	0.823	0.860	0.830	0.836	0.822	0.853	0.829
1096	0.866	0.859	0.893	0.868	0.860	0.857	0.888	0.866
1097	0.866	0.929	0.893	0.938	0.860	0.926	0.888	0.936
1098	0.899	0.938	0.916	0.944	0.895	0.937	0.912	0.943
1099	0.813	0.880	0.840	0.891	0.804	0.878	0.832	0.890
1100	0.847	0.824	0.862	0.830	0.840	0.823	0.855	0.830
1101	0.903	0.869	0.917	0.874	0.899	0.868	0.913	0.874
1102	0.922	0.869	0.924	0.872	0.917	0.869	0.918	0.872
1103	0.958	0.893	0.958	0.894	0.955	0.893	0.955	0.894
1104	0.958	0.965	0.958	0.966	0.955	0.965	0.955	0.966
1105	0.958	0.965	0.959	0.966	0.956	0.965	0.956	0.966
1106	0.958	0.893	0.959	0.894	0.956	0.893	0.956	0.894
1107	0.922	0.940	0.925	0.942	0.917	0.940	0.919	0.942
1108	0.922	0.940	0.924	0.942	0.917	0.940	0.918	0.942



CASE CODE	Climate Zone 15				Climate Zone 16			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1001	0.750	0.596	0.779	0.622	0.693	0.730	0.725	0.755
1002	0.791	0.640	0.806	0.651	0.743	0.763	0.759	0.777
1003	0.751	0.600	0.782	0.630	0.696	0.731	0.732	0.756
1004	0.820	0.703	0.852	0.731	0.778	0.786	0.813	0.813
1005	0.866	0.753	0.882	0.765	0.834	0.821	0.851	0.836
1006	0.822	0.708	0.856	0.741	0.782	0.786	0.821	0.814
1007	0.820	0.760	0.852	0.791	0.778	0.850	0.813	0.879
1008	0.820	0.793	0.852	0.819	0.778	0.856	0.813	0.886
1009	0.868	0.842	0.886	0.858	0.838	0.894	0.859	0.911
1010	0.750	0.637	0.779	0.660	0.693	0.740	0.725	0.766
1011	0.793	0.645	0.810	0.660	0.747	0.763	0.766	0.778
1012	0.750	0.644	0.779	0.672	0.693	0.789	0.725	0.816
1013	0.868	0.758	0.886	0.775	0.838	0.822	0.859	0.837
1014	0.866	0.753	0.882	0.765	0.834	0.821	0.851	0.836
1015	0.822	0.708	0.856	0.741	0.782	0.786	0.821	0.814
1016	0.820	0.793	0.852	0.819	0.778	0.856	0.813	0.886
1017	0.872	0.822	0.887	0.832	0.842	0.893	0.856	0.908
1018	0.846	0.791	0.869	0.811	0.810	0.871	0.835	0.893
1019	0.872	0.760	0.887	0.769	0.842	0.826	0.856	0.840
1020	0.797	0.647	0.811	0.655	0.751	0.767	0.764	0.780
1021	0.846	0.731	0.869	0.750	0.810	0.806	0.835	0.826
1022	0.773	0.621	0.795	0.639	0.721	0.749	0.744	0.767
1023	0.752	0.646	0.779	0.622	0.699	0.741	0.725	0.755
1024	0.793	0.692	0.806	0.651	0.749	0.774	0.759	0.777
1025	0.754	0.649	0.782	0.630	0.702	0.741	0.732	0.756
1026	0.822	0.727	0.852	0.731	0.782	0.792	0.813	0.813
1027	0.867	0.777	0.882	0.765	0.837	0.827	0.851	0.836
1028	0.824	0.729	0.856	0.741	0.785	0.792	0.821	0.814
1029	0.822	0.786	0.852	0.791	0.782	0.856	0.813	0.879
1030	0.822	0.807	0.852	0.819	0.782	0.858	0.813	0.886
1031	0.869	0.855	0.886	0.858	0.841	0.895	0.859	0.911
1032	0.752	0.665	0.779	0.660	0.699	0.743	0.725	0.766
1033	0.795	0.694	0.810	0.660	0.753	0.774	0.766	0.778
1034	0.752	0.699	0.779	0.672	0.699	0.801	0.725	0.816
1035	0.869	0.780	0.886	0.775	0.841	0.827	0.859	0.837
1036	0.867	0.777	0.882	0.765	0.837	0.827	0.851	0.836



CASE CODE	Climate Zone 15				Climate Zone 16			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1037	0.824	0.729	0.856	0.741	0.785	0.792	0.821	0.814
1038	0.822	0.807	0.852	0.819	0.782	0.858	0.813	0.886
1039	0.874	0.848	0.887	0.832	0.846	0.899	0.856	0.908
1040	0.847	0.817	0.869	0.811	0.813	0.877	0.835	0.893
1041	0.874	0.784	0.887	0.769	0.846	0.832	0.856	0.840
1042	0.799	0.699	0.811	0.655	0.757	0.778	0.764	0.780
1043	0.847	0.755	0.869	0.750	0.813	0.811	0.835	0.826
1044	0.776	0.672	0.795	0.639	0.728	0.760	0.744	0.767
1045	0.898	0.751	0.896	0.746	0.865	0.852	0.861	0.852
1046	0.948	0.843	0.945	0.837	0.933	0.886	0.928	0.885
1047	0.948	0.911	0.945	0.905	0.933	0.958	0.928	0.957
1048	0.949	0.914	0.947	0.910	0.935	0.958	0.932	0.958
1049	0.949	0.924	0.947	0.921	0.935	0.962	0.932	0.962
1050	0.899	0.776	0.898	0.774	0.867	0.861	0.865	0.861
1051	0.899	0.839	0.898	0.837	0.867	0.930	0.865	0.930
1052	0.899	0.753	0.898	0.750	0.867	0.852	0.865	0.852
1053	0.898	0.812	0.896	0.807	0.865	0.921	0.861	0.921
1054	0.755	0.675	0.781	0.624	0.705	0.771	0.729	0.757
1055	0.824	0.757	0.853	0.733	0.787	0.823	0.817	0.814
1056	0.824	0.819	0.853	0.792	0.787	0.890	0.817	0.880
1057	0.826	0.821	0.857	0.803	0.790	0.890	0.825	0.881
1058	0.868	0.859	0.883	0.828	0.840	0.914	0.853	0.905
1059	0.870	0.862	0.887	0.839	0.844	0.914	0.861	0.906
1060	0.755	0.730	0.781	0.674	0.705	0.834	0.729	0.818
1061	0.797	0.711	0.812	0.661	0.756	0.791	0.769	0.779
1062	0.757	0.678	0.784	0.632	0.708	0.771	0.736	0.758
1063	0.795	0.709	0.808	0.653	0.753	0.791	0.762	0.778
1064	0.801	0.714	0.812	0.657	0.760	0.794	0.766	0.781
1065	0.778	0.695	0.796	0.640	0.732	0.783	0.748	0.769
1066	0.801	0.772	0.812	0.710	0.760	0.859	0.766	0.844
1067	0.875	0.800	0.888	0.770	0.848	0.848	0.858	0.840
1068	0.900	0.822	0.907	0.797	0.880	0.860	0.885	0.854
1069	0.885	0.810	0.897	0.786	0.862	0.852	0.873	0.846
1070	0.752	0.625	0.781	0.624	0.698	0.761	0.729	0.757
1071	0.822	0.734	0.853	0.733	0.783	0.818	0.817	0.814
1072	0.822	0.793	0.853	0.792	0.783	0.884	0.817	0.880



CASE CODE	Climate Zone 15				Climate Zone 16			
	1 Story		2 Story		1 Story		2 Story	
	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%	Heating,%	Cooling,%
1073	0.824	0.798	0.857	0.803	0.787	0.885	0.825	0.881
1074	0.867	0.833	0.883	0.828	0.837	0.908	0.853	0.905
1075	0.869	0.839	0.887	0.839	0.841	0.909	0.861	0.906
1076	0.752	0.676	0.781	0.674	0.698	0.822	0.729	0.818
1077	0.795	0.662	0.812	0.661	0.750	0.781	0.769	0.779
1078	0.793	0.658	0.808	0.653	0.747	0.781	0.762	0.778
1079	0.754	0.629	0.784	0.632	0.702	0.761	0.736	0.758
1080	0.799	0.662	0.812	0.657	0.754	0.784	0.766	0.781
1081	0.775	0.644	0.796	0.640	0.726	0.772	0.748	0.769
1082	0.799	0.716	0.812	0.710	0.754	0.847	0.766	0.844
1083	0.874	0.776	0.888	0.770	0.845	0.843	0.858	0.840
1084	0.899	0.800	0.907	0.797	0.878	0.855	0.885	0.854
1085	0.884	0.788	0.897	0.786	0.859	0.848	0.873	0.846
1086	0.900	0.801	0.980	0.907	0.870	0.863	0.980	0.907
1087	0.948	0.864	0.980	0.907	0.935	0.891	0.980	0.907
1088	0.949	0.866	0.980	0.907	0.937	0.891	0.980	0.907
1089	0.948	0.934	0.980	0.980	0.935	0.963	0.980	0.980
1090	0.949	0.936	0.980	0.980	0.937	0.963	0.980	0.980
1091	0.900	0.866	0.980	0.980	0.870	0.933	0.980	0.980
1092	0.901	0.867	0.980	0.980	0.872	0.933	0.980	0.980
1093	0.901	0.802	0.980	0.907	0.872	0.863	0.980	0.907
1094	0.827	0.800	0.853	0.815	0.772	0.845	0.801	0.844
1095	0.855	0.815	0.872	0.824	0.809	0.841	0.827	0.841
1096	0.876	0.843	0.902	0.858	0.837	0.892	0.867	0.889
1097	0.876	0.912	0.902	0.927	0.837	0.964	0.867	0.961
1098	0.907	0.929	0.922	0.938	0.878	0.959	0.896	0.957
1099	0.827	0.865	0.853	0.881	0.772	0.914	0.801	0.912
1100	0.859	0.817	0.874	0.826	0.812	0.840	0.827	0.840
1101	0.911	0.861	0.924	0.869	0.882	0.886	0.896	0.885
1102	0.931	0.869	0.934	0.872	0.896	0.869	0.897	0.872
1103	0.962	0.893	0.962	0.894	0.946	0.893	0.945	0.894
1104	0.962	0.965	0.962	0.966	0.946	0.965	0.945	0.966
1105	0.962	0.965	0.963	0.966	0.947	0.965	0.947	0.966
1106	0.962	0.893	0.963	0.894	0.947	0.893	0.947	0.894
1107	0.931	0.940	0.934	0.942	0.896	0.940	0.898	0.942
1108	0.931	0.940	0.934	0.942	0.896	0.940	0.897	0.942







